An Experimental Study on Evaluation of Compressive Strength in Cement Mortar Using Averaged Electromagnetic Properties

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Abstract: A non-destructive testing (NDT) method for evaluating physical properties of concrete including the compressive strength is highly desirable. This paper presents such an NDT method based on measurements of electromagnetic (EM) properties of the material. Experiments are carried out on cement mortar with different water/cement (W/C) ratios. Their EM properties including the conductivity and the dielectric constant are measured at different exposure conditions and curing periods over a wide frequency range of the EM wave. The compressive strength of these specimens is also tested. It is found that both the conductivity and the dielectric constant increase as the W/C ratio decreases and the curing period increases, which leads strength development in the specimens. A linear correlation is observed between the averaged EM properties over the 5 to 20 GHz frequency range and the measured compressive strength, demonstrating the effectiveness of the EM property-based NDT method in evaluating strength of OPC mortar.

Keywords: NDT, electromagnetic, cement mortar, conductivity, dielectric constant.

1. Introduction

An NDT technique is highly desirable for evaluating strength and condition of cement-based construction materials. Among the potential techniques, EM property-based NDT methods have been studied for these materials. 1-4 The pore and saturation in a porous media such as concrete and cement mortar are considered as major parameters affecting their EM properties. The saturation of concrete is reported to have the most significant contribution toward the complex dielectric permittivity of the overall mixture. 2-4 In addition, the pores in the cement matrix also play an important role in the electrical conductivity spectra. 3,5 The pore and saturation are major parameters affecting not only the EM properties, but also physical properties in cement-based materials. During the hydration process in cement particles, pores occur in the concrete and the amount of pore (porosity) is in close relationship with structural performance like strength 6-8 and durability performance like diffusion 9,10 and water permeation. 11

Many studies have been performed on concrete utilizing the EM properties. Characterization of EM properties in cement-based materials has been studied and documented. 3-5,12-14 Some of these studies are focused on permeability and diffusion coefficient for material durability research. 15-17 Others are for the characterization of EM properties in concrete using mineral admixtures such as FA (fly ash) and GGBS (ground granulated blast-furnace slag) considering concrete curing stage. 18-21 In addition, EM properties are applied for monitoring and condition assessment of reinforced concrete structures. They include monitoring of deteriorated concrete 13,22-24 and modeling of EM properties in porous concrete or cement-based system. 22,25-25 Recently, EM properties are used to assess condition of FRP-wrapped concrete structures. 26-30

Despite these research activities, very limited investigations have been performed on relationships between the EM properties and physical properties (such as compressive strength) of cement-based construction materials. The ultimate goal of this study is to investigate the relationship between the EM properties and the compressive strength of concrete. In order to avoid the effect of coarse aggregates, OPC mortar is first studied. OPC mortar specimens are prepared with five different W/C ratios (40%, 45%, 50%, 55%, and 60%) and the compressive strength is measured at the age of 1, 2, and 4 weeks curing. Meanwhile the EM properties of these specimens including the conductivity and the dielectric constant are measured using EM waves over a wide frequency range from 0.2 through 20 GHz. Furthermore, the specimens are tested not only in room conditions but also in saturated conditions in order to study the effect of the saturation on EM properties. Based on the experimental study, the relationship between the EM properties and physical characteristics of OPC mortar is obtained and discussed.
2. Conductivity and dielectric constant

Every material has a unique set of EM properties. Dielectric materials such as concrete can be characterized by two independent electromagnetic properties: the complex permittivity ($\varepsilon'$) and the complex permeability ($\mu'$). In general, four independent measurements are necessary to obtain the real and imaginary parts of $\varepsilon'$ and $\mu'$. However, most common dielectric materials including concrete are nonmagnetic, making the permeability $\mu'$ close to the permeability of free space ($\mu_0 = 4\pi \times 10^{-7}$ Henry/meter). Thus, the focus of the discussion is on the complex permittivity $\varepsilon'^*$ which is defined in references.\(^{2,29}\)

$$\varepsilon'^* = \varepsilon' - j\varepsilon''$$  \hspace{1cm} (1)

where, $\varepsilon'$ and $\varepsilon''$ are the real and imaginary parts of the complex permittivity with $j = \sqrt{-1}$.

Dividing Eq. (1) by the permittivity in free space $\varepsilon_0$ (8.854 × 10\(^{-12}\) Farad/m), Eq. (2) and furthermore Eq. (3) can be derived:\(^{3,29}\)

$$\frac{\varepsilon'^*}{\varepsilon_0} = \frac{\varepsilon'_r - j\varepsilon'_i}{\varepsilon_0}$$  \hspace{1cm} (2)

$$\varepsilon'_r = \varepsilon' - j\varepsilon''$$  \hspace{1cm} (3)

where, $\varepsilon'^*$ is the relative complex permittivity, and $\varepsilon'_r$ and $\varepsilon'_i$ are its real and imaginary parts, respectively. The real part of the relative complex permittivity, so-called dielectric constant ($\varepsilon'_r > 1$), means how much energy from an external electric field is stored in a material. The imaginary part of the relative complex permittivity, ($\varepsilon'_i > 0$), shows how dissipative the material is to an external electric field, which is simply referred to as the loss factor.\(^{3,22}\) The equivalent conductivity can be expressed in terms of the imaginary part of the complex permittivity ($\varepsilon''$) as shown in Eq. (4).

$$\sigma = \varepsilon''\omega = (\varepsilon'_r\varepsilon_0\tan\delta)2\pi f$$  \hspace{1cm} (4)

where, $\sigma$ is conductivity (mhos/m), $\omega$ is the EM wave frequency (rad/sec), $\tan\delta$ is loss tangent (the ratio of energy loss to energy stored in a material) and $f$ is frequency in (Hz). These EM properties are not constant and dependent upon frequency, temperature, moisture content, chloride content, and concrete mix constituents.\(^{3-4}\) In this study, two EM properties of the OPC mortar, the dielectric constant and the conductivity are measured in a given EM wave frequency.

3. Test of EM properties and compressive strength in OPC mortar

OPC motor specimens with different W/C ratios are made and their strengths are tested at different curing periods and exposure conditions. Meanwhile, their EM properties are also measured.

3.1 Test specimens

The specimens were made with OPC mortar under five W/C ratios (40%, 45%, 50%, 55%, and 60%). Each specimen was kept in an air-curing condition for 3 days after mixing and then in submerged condition (20°C) for four weeks. The mix proportions and physical properties of aggregate are listed in Table 1.

The cylindrical specimens (100 mm × 200 mm) are made for the compressive strength tests and rectangular ones (80 mm × 150 mm × 40 mm) are also made for measurement of EM properties. The depth of the specimens for EM measurement is determined to be 40 mm, which is considered sufficient to prevent the wave penetrating through the specimen and reflected from the outer boundary. This is based on a previous study that EM measurement of concrete specimens with a depth of 5 mm suffered slight interference of reflected microwave.\(^{14}\)

3.2 EM measurement setup and calibration

Measurement setup consists of a dielectric probe kit including the analyzing software and an open ended coaxial probe, a network analyzer, and a laptop computer, as shown in Fig. 1. The probe is a cut-off section of transmission line and the EM properties of the material are measured by placing the probe in contact with a flat face of a solid material or immersing into a liquid. The network analyzer is connected with the laptop computer and communicated with and controlled by the laptop computer.\(^{29}\) The network analyzer sends and receives the microwave through the probe over a frequency range from 0.2 GHz to 20 GHz at an interval of 0.4 GHz. The measured reflection signals are then analyzed by the software at the laptop computer for obtaining the EM properties (i.e., the dielectric constant and the conductivity). Fig. 1(a), (b), and (c) show schematic diagram, picture of measurement setup, and photo measurement, respectively.

Generally for the calibration of the experimental system using the open-ended coaxial probe, well-known properties are needed over the measuring frequency range.\(^{31}\) In this study, calibration was performed on air and water in 25°C temperature prior to the measurement. The calibration results, in terms of the dielectric constant and the conductivity, are shown in Fig. 2, well agreeing with those reported in literature.\(^{2,29}\)

3.3 Tests for compressive strength and EM properties

Three cylindrical OPC mortar specimens are prepared for each compressive strength test. The compressive tests of the specimens with five different W/C ratios are performed at the age of one, two, and four weeks, based on the testing standard.\(^{32}\) The specimens for EM properties are kept in the same conditions as those for compressive strength tests. Grinding with 3–5 mm depth is performed for removal of bleeding portion and

Table 1 Mixture proportions and properties of sand for specimens.

<table>
<thead>
<tr>
<th>W/C ratio (%)</th>
<th>Cement (kg/25liter)</th>
<th>Sand (kg/25liter)</th>
<th>Water (kg/25liter)</th>
</tr>
</thead>
<tbody>
<tr>
<td>40</td>
<td>8.50</td>
<td>25.00</td>
<td>3.40</td>
</tr>
<tr>
<td>45</td>
<td>8.50</td>
<td>25.00</td>
<td>3.83</td>
</tr>
<tr>
<td>50</td>
<td>8.50</td>
<td>25.00</td>
<td>4.25</td>
</tr>
<tr>
<td>55</td>
<td>8.50</td>
<td>25.00</td>
<td>4.68</td>
</tr>
<tr>
<td>60</td>
<td>8.50</td>
<td>25.00</td>
<td>5.10</td>
</tr>
</tbody>
</table>

- Cement : Sand = 1 : 3.125 (weight ratio)
- Physical properties of aggregate
  Specific gravity (= 2.60 g/cm³), Absorption (= 0.95%), F.M. (= 2.64)
unevenness of the surface. For using the averaged value within the range of 0.2~20 GHz, EM properties are measured 10 times for each specimen. Before measurement of the EM properties, some of the specimens are exposed to room condition (temperature: 20~22°C; relative humidity: 55~62%) for 36 hours, while the others are immediately tested after bring them out of water in order to evaluate the changed EM properties due to saturation. The test plan and exposure conditions are summarized in Table 2.

4. Measured strengths and EM properties

4.1 Compressive strengths with different W/C ratios

The results of the compressive test show the traditional trend of strength development that the strength increases with reduced W/C ratios and extended curing periods. Through extension of the curing period in early age (within 28 days) and decrease in W/C ratio, cement-based material has less porosity and more hydrates due to the sufficient hydration process, which is in close relation with the compressive strength. The results of
compressive strength measured from the compressive testing of the cylindrical samples are shown in Fig. 3, in which (a) shows the compressive strength increases as the curing period extends for different W/C ratios and (b) the strength decreases as the W/C ratio increases for different curing periods.

### 4.2 EM properties with different W/C ratios and curing periods

#### 4.2.1 EM properties with different W/C ratios

The conductivity and dielectric constant measured after four weeks of curing under different exposure conditions are plotted in Fig. 4 over a large range of EM wave frequencies. From Fig. 4, the conductivity increases and the dielectric constant decreases in all the cases with increasing frequency, regardless of W/C ratios. In a given frequency, the conductivity and the dielectric constant measured on the specimens with lower W/C ratios show higher values. This trend is based on characteristics of

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**Fig. 3** Test results of compressive strength in OPC mortar.

**Fig. 4** EM properties measured in different exposure conditions.

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<table>
<thead>
<tr>
<th>Table 2 Test plan and exposure conditions.</th>
</tr>
</thead>
<tbody>
<tr>
<td>W/C (%)</td>
</tr>
<tr>
<td>---------</td>
</tr>
<tr>
<td>Room condition</td>
</tr>
<tr>
<td>40</td>
</tr>
<tr>
<td>45</td>
</tr>
<tr>
<td>50</td>
</tr>
<tr>
<td>55</td>
</tr>
<tr>
<td>60</td>
</tr>
</tbody>
</table>

- Room condition: temperature (22~25°C), relative humidity (50~62%)
4.2.2 EM properties with different curing periods

To facilitate a comparison of EM properties with different W/C ratios in a specific curing period, averages are taken respectively for the conductivity and the dielectric constant values measured over the 5–20 GHz frequency range. In Fig. 5, the averaged EM property values normalized to the maximum value (under 40% W/C ratio) are plotted for one, two, and four week-curing periods, respectively. In the given curing period, the averaged dielectric constant and conductivity increase as the W/C ratios reduce.

For the specimens in the room condition, change in the W/C ratio from 0.4 to 0.6 significantly reduces the EM properties. More specifically, the conductivity at the 0.6 W/C ratio is 67–63% of the value at the 0.4 W/C ratio, while dielectric constant is 78–69%. In the saturated condition, however, no significant reduction in the EM properties with increased W/C ratios is observed. More specifically, the conductivity at the 0.6 W/C ratio is 83–93% of the value at 0.4 W/C ratio, while the dielectric constant is 87–81%. This is because water in the fully saturated specimens is a more dominant parameter for the EM properties than the other mix parameters such as the W/C ratio. The change in the conductivity and the dielectric constant is respectively plotted in Figs. 6 and 7 with different W/C ratios and curing periods.

For the comparison among different curing periods and W/C ratios, all the measured EM property values are normalized by the maximum value that is measured at the 0.4 W/C ratio after four week of curing. These normalized EM property values are plotted in Figs. 8 and 9 and summarized in Table 3. The graphs in Figs. 8 and 9 show a more distinct reduction of the EM property values with the increase in the W/C ratio and the decrease in the curing period under the room condition, in comparison to the saturated condition among all the specimens, the minimum EM values are measured in the case of the 0.6 W/C ratio after 1 week of curing, they are 48.73% (conductivity) and 55.01% (dielectric constant) to the maximum value that are measured in the case of the 0.4 W/C ratio after 4 weeks of curing.

4.3 Relationship between compressive strength and measured EM properties

Comparing the compressive testing results in Table 3 with the EM property measurement results under different W/C ratios
and curing periods, a clear correlation is observed. Linear regression analysis is carried out to obtain the relationship between the compressive strength and the averaged EM properties (over the frequency range of 5 GHz through 20 GHz). The regression results, together with the testing results of the compressive strengths and the measured results of the conductivity and the dielectric constant, are shown in Figs. 9 and 10 for the room and the saturated conditions. The linear relationship and correlation factors are expressed in Eqs. (5)–(8).

\[
C = 0.1083 \cdot S + 2.3401, \quad R^2 = 0.7422 \\
C_{\text{room}} = 0.0278 \cdot S + 0.0053, \quad R^2 = 0.9401 \\
D_{\text{sat}} = 0.5502 \cdot S + 7.7156, \quad R^2 = 0.8011 \\
D_{\text{room}} = 0.1074 \cdot S + 0.8932, \quad R^2 = 0.9355
\]

Table 3 Comparison of normalized EM properties.

<table>
<thead>
<tr>
<th>W/C (%)</th>
<th>1 week (%)</th>
<th>2 weeks (%)</th>
<th>4 weeks (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>C/R</td>
<td>C/S</td>
<td>D/R</td>
</tr>
<tr>
<td>40</td>
<td>72.34</td>
<td>82.56</td>
<td>80.28</td>
</tr>
<tr>
<td>45</td>
<td>64.57</td>
<td>78.21</td>
<td>74.88</td>
</tr>
<tr>
<td>50</td>
<td>60.16</td>
<td>76.75</td>
<td>72.15</td>
</tr>
<tr>
<td>55</td>
<td>56.70</td>
<td>71.95</td>
<td>60.80</td>
</tr>
<tr>
<td>60</td>
<td>48.73</td>
<td>68.87</td>
<td>55.01</td>
</tr>
<tr>
<td>60</td>
<td>48.73</td>
<td>68.87</td>
<td>55.01</td>
</tr>
</tbody>
</table>

(Note) C/R : conductivity in room condition, C/S : conductivity in submerged condition, D/R : dielectric constant in room condition, D/S : dielectric constant in submerged condition.
saturated and room conditions under which the specimens are tested. In the saturated condition, the measured EM properties are observed to be less correlated because they unsteadily increase in the position of the sample surface which has the large pores filled with local moisture (water). In this paper, over-saturated samples are used for measurement of EM properties, which means abundant water is still on the surface since they are directly tested after pickup form submerged water. If samples with larger pore are saturated, EM properties increase due to the water in pores. However, the results in saturated condition show opposite trends because of the over-saturated condition. The EM behaviors with different saturation are well analyzed in the previous research\(^{35}\) which indicates that higher EM properties are measured in mortar with higher W/C ratios when they are fully saturated. An increased porosity in mortar with higher W/C ratios can keep more surface water (saturation) which magnifies dielectric constant and conductivities. In the research,\(^{39}\) the surface abundant water on sample is removed before measurement for EM properties so that the trends are opposite to the results from this study in saturated condition. From Figs. 9 and 10, it is clearly observed that the both of the EM properties, the conductivity and the dielectric constant, of the OPC mortar increase linearly with the compressive strength. This demonstrates the feasibility of using the non-destructive EM property measurement for evaluating the compressive strength of OPC mortar, and potentially concrete. It is noted that the correlation factors for specimens measured in the room condition are higher than those in the saturated condition.

5. Conclusions

Through extensive experiments including the compressive strength tests and EM property measurements of a large number of OPC mortar specimens involving five different W/C ratios, three curing periods, and two different exposure conditions (room and saturated), the following conclusions can be made:

1) The measured EM properties, both the conductivity and the dielectric constant, increase with the extension of curing period and reduced W/C ratio. The maximum averaged values in the conductivity and the dielectric constant are measured in the specimens with lowest W/C ratio of 0.4 and the longest curing period of four weeks.

2) The measured EM properties, both the dielectric constant and the conductivity, clearly show a linear relationship with compressive strength of the OPC mortar under both the room and saturated conditions. This demonstrates a significant potential for non-destructive evaluation of the compressive strength of concrete through the measurement of its EM properties.

3) In room condition, the conductivity at the 0.6 W/C ratio is 67–63% of the value at the 0.4 W/C ratio, while dielectric constant is 78–69%. In the saturated condition, however, no significant reduction in the EM properties with increased W/C ratios is observed. The conductivity at the 0.6 W/C ratio is 83–93% of the value at 0.4 W/C ratio, while the dielectric constant is 87–81%.

4) From the results, it is evaluated that dielectric constant in room condition is most efficient to evaluate the strength of cement mortar, showing higher correlation factor. In the future, the authors will extend this study to concrete specimens considering the influence of the coarse aggregates and its transition zone.

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References


