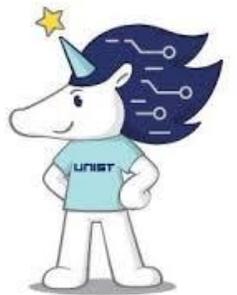


# Monitoring Buildability of 3DPC Using Ultrasonic Guided Wave

Geetanjali Chandam<sup>1</sup>, John S Popovics<sup>\*2</sup>, Myoungsu Shin<sup>\*1</sup>

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UNIST



울산과학기술원  
ULSAN NATIONAL INSTITUTE OF  
SCIENCE AND TECHNOLOGY

## Introduction

1. **Overview of the Study: Monitoring 3DPC (Early Printing Stage)**
2. **Introducing Guided Waves**

## Test Methodology

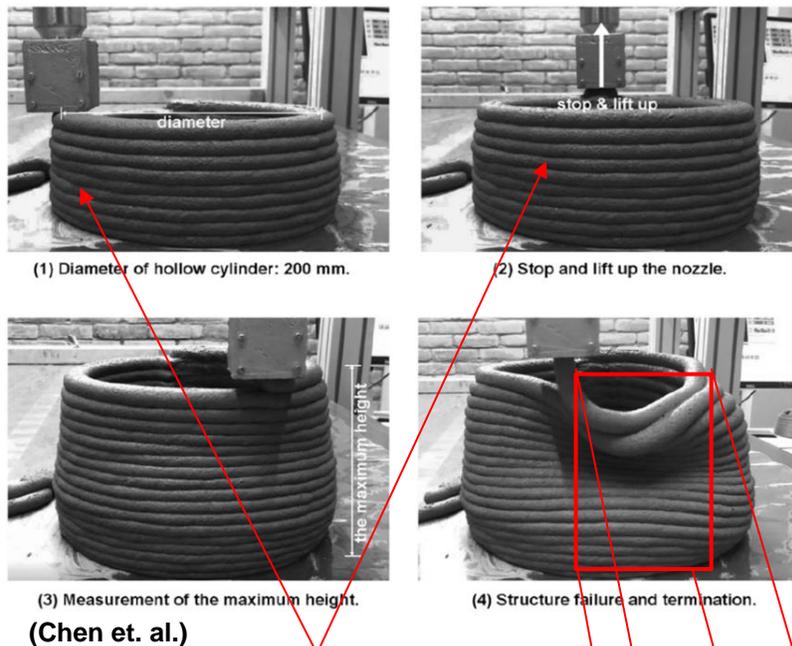
3. **Materials and Mix Design**
4. **Early-age Material Properties**
5. **Printability of the Mix Design**
  
6. **Ultrasonic Test Setup**  
Chosen Waveguide  
Chosen Center Frequencies
7. **Green Strength Test**

## Test Results

8. **Attenuation (dB)**
9. **Green Strength (kPa)**
10. **Buildable Layer Prediction**
11. **Correlations**

# Monitoring 3DPC: Early Printing Stage

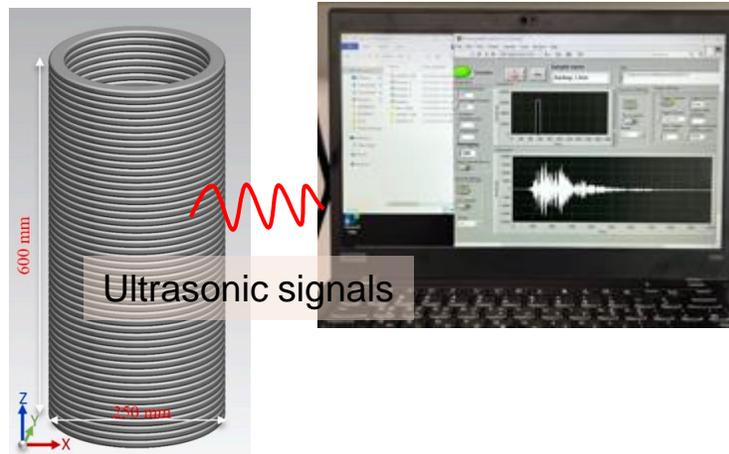
## Process of 3D printing



Build layer by layer

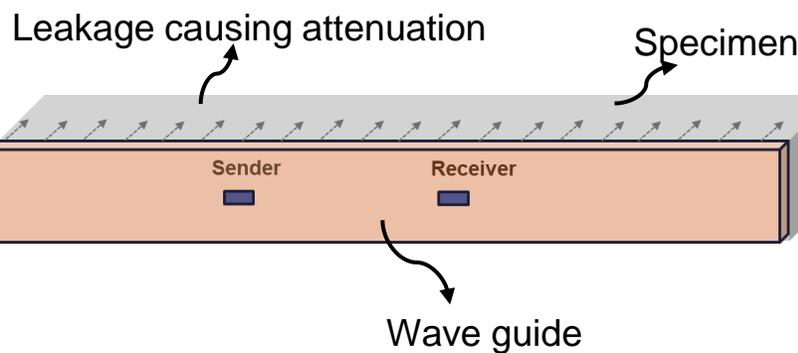
The printed layers must be able to resist successive layer's weight. The resistance of deposited wet material to deformation under load is known as **buildability**

## Application of ultrasonic guided wave



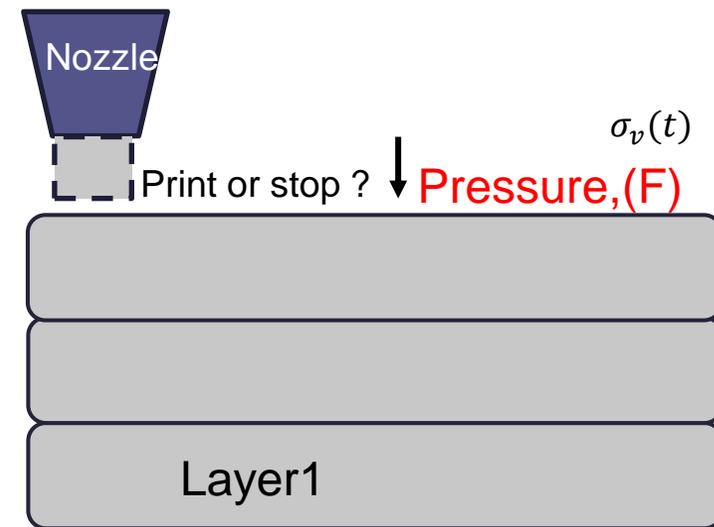
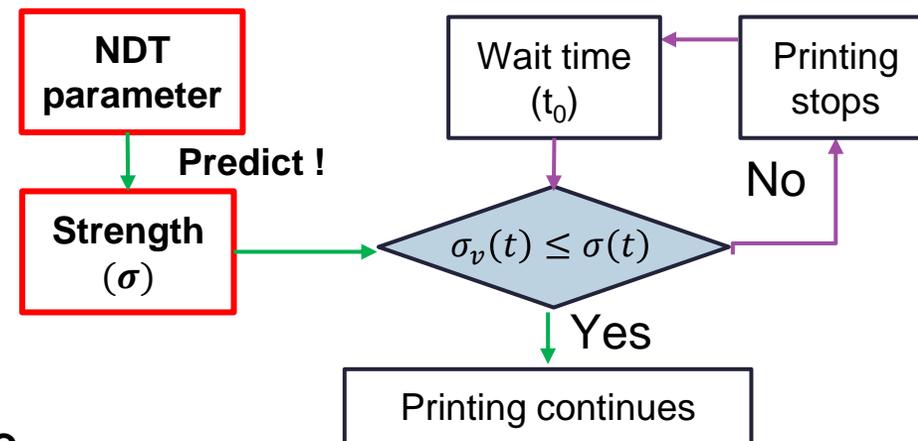
## Non-destructive technique to monitor 3DPC

Maybe guided wave will work !

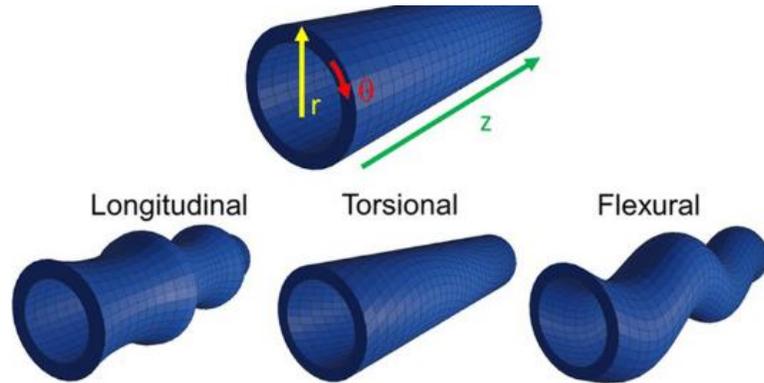


Wave propagates in the wave guide (i.e. plate)

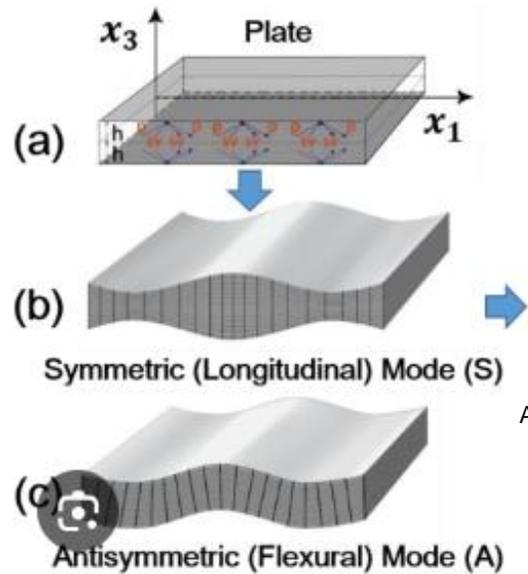
## Determine green strength to predict printability



# What are Guided Waves

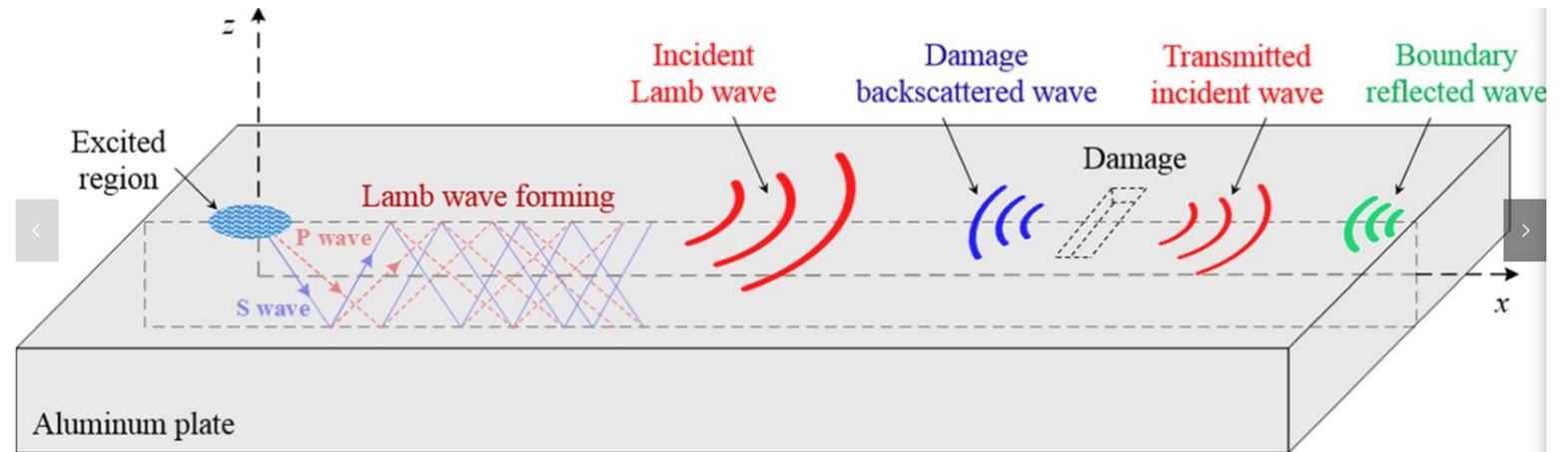


Adopted [1]



Adopted [2]

- Waves propagating in a finite boundary (Plate or cylindrical)
- Guided waves in cylindrical shapes: longitudinal, torsional and flexural modes
- Guide waves in plate structure: Lamb waves
- Lamb waves: **Symmetric** and **Anti-symmetric** modes
- **Wave modes are decomposed due to the superposition of P- and S-waves**



Adopted [3]

The interaction of wave and the surface causes constructive and destructive interference, leading to specific wave modes, highly dependent on **wavelength** of the waves and the **thickness** of the plate structure

[1] Troelstra, Marian Amber, et al. "Shear wave cardiovascular MR elastography using intrinsic cardiac motion for transducer-free non-invasive evaluation of myocardial shear wave velocity." *Scientific Reports* 11.1 (2021): 1403.

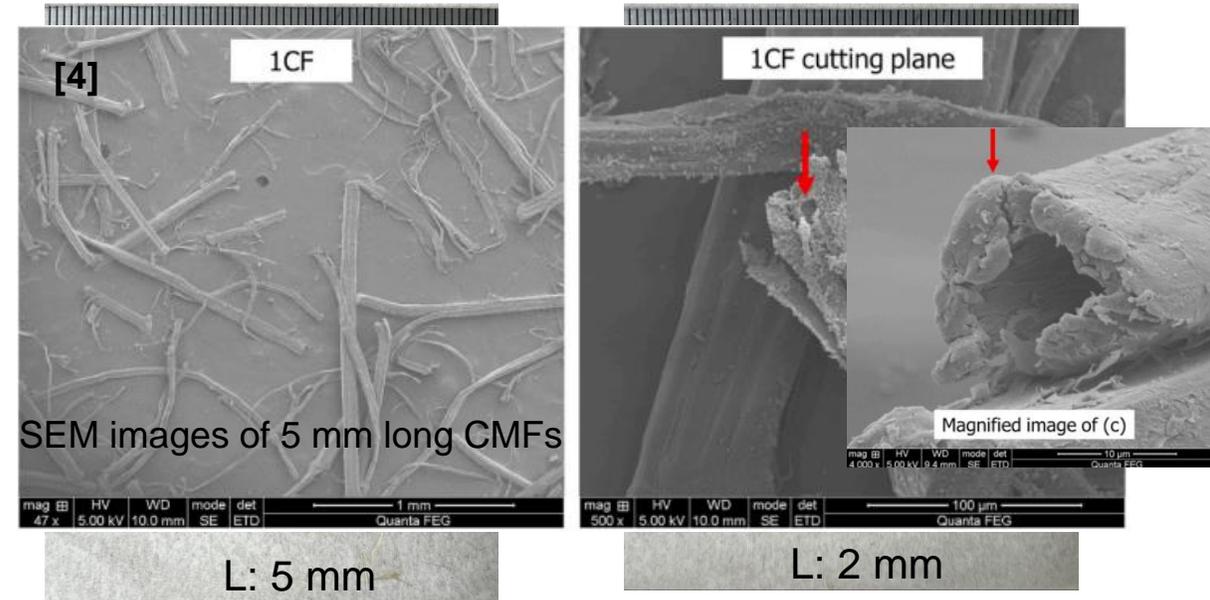
[2] Sun, Xiaoqiang, et al. "Interaction of Lamb wave modes with weak material nonlinearity: Generation of symmetric zero-frequency mode." *Sensors* 18.8 (2018): 2451.

[3] Harb, Mohammad Said, and Fuh-Gwo Yuan. "Damage imaging using non-contact air-coupled transducer/laser Doppler vibrometer system." *Structural Health Monitoring* 15.2 (2016): 193-203.

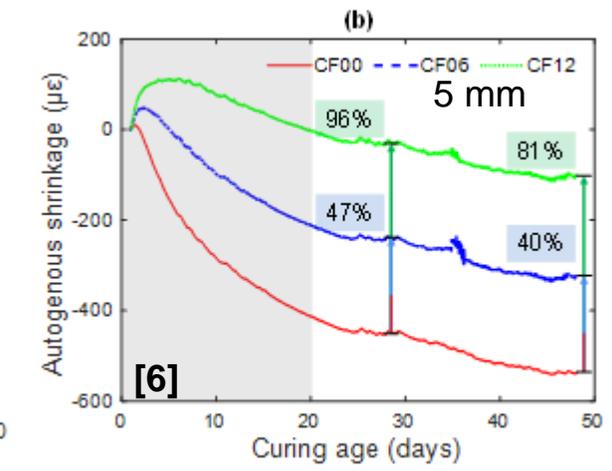
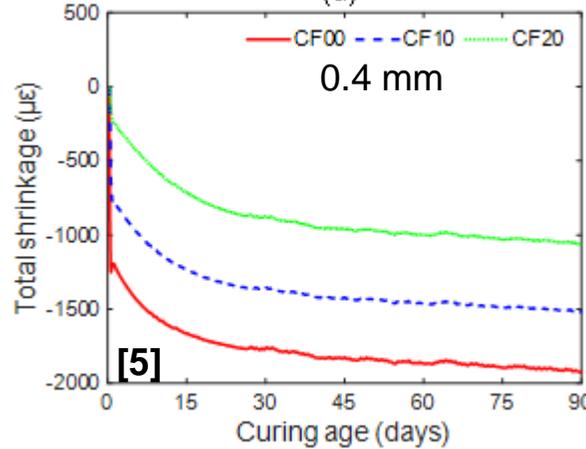
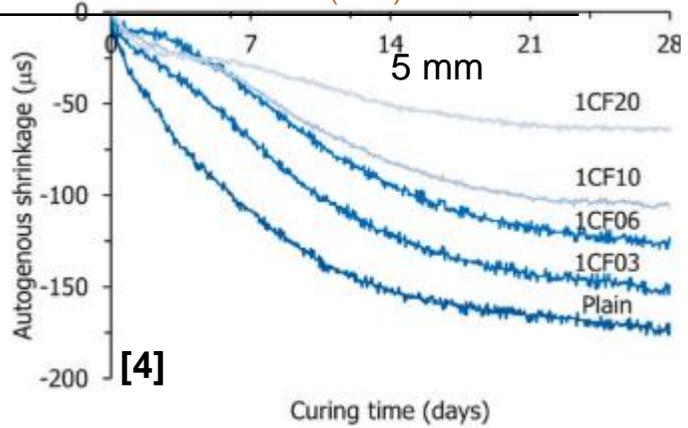
# Materials and Mix Design

(kg/m<sup>3</sup>)

Name	W/B	OPC	Fly Ash	Silica fume	Sand	SP	CMFs	Add. water
CF00	349	764	218	109	1091	11	0	0
2CF10							11 (1 %)	32
2CF20							22 (2 %)	65
5CF10							11 (1 %)	47
5CF20							22 (2 %)	94

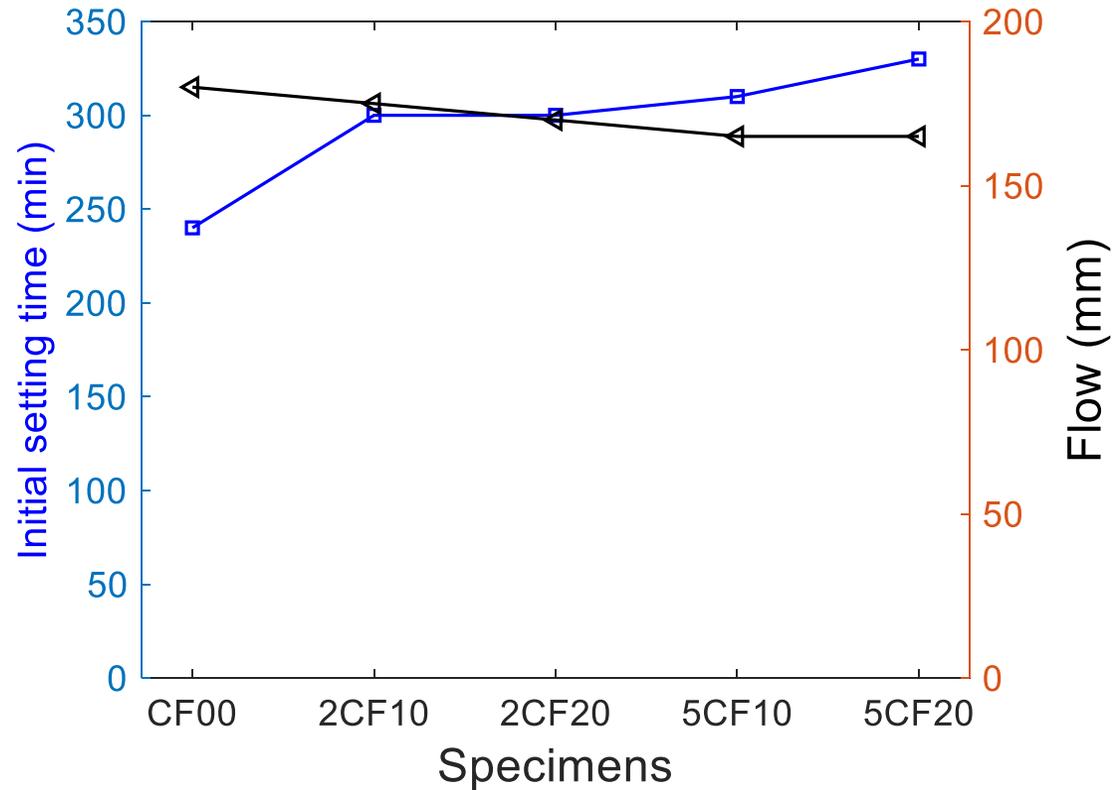


CMFs: Cellulose microfibers  
 2CF10: 2 mm fiber length added 1 %  
 5CF10: 5 mm fiber length added 1 %  
 High water absorbing capacity  
 (internal curing agent)  
 Tensile strength 330 ± 29.4 MPa  
 Average pore diameter 3.4 μm



[4] S. Gwon, Y.C. Choi, **M. Shin**, Internal curing of cement composites using kenaf cellulose microfibers, J Build Eng 47 (2022)  
 [5] E. Cho, **G. Chandam**, S. Gwon, **M. Shin**, Effect of Cellulose Microfibers on Shrinkage: Application of Ultrasonic Non-Destructive Testing  
 [6] **G. Chandam**, Y.Oinam, E. Cho, J.S. Popovics, S. Pyo **M. Shin**, Effectiveness of Wave Interferometry in Monitoring Autogenous Shrinkage and Mitigation Role of Cellulose Microfibers

# Early-age Material Properties



ASTM C191 using Vicat  
needle test apparatus

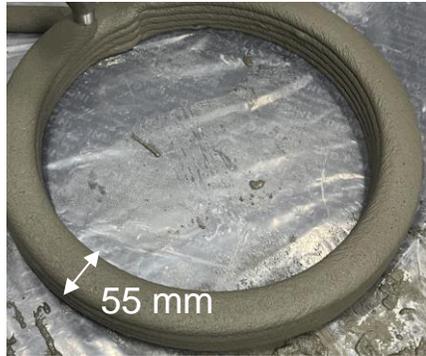
ASTM C230 mini flow table  
tests



- Initial setting time increases with increase of fiber content and fiber length
- Flow decreases with increase in fiber content and fiber length

# Printability of the Mix Design

CF00: No fibers



2CF10: 2mm 1 %



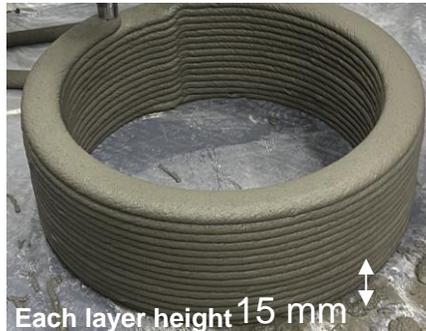
2CF20: 2mm 2 %



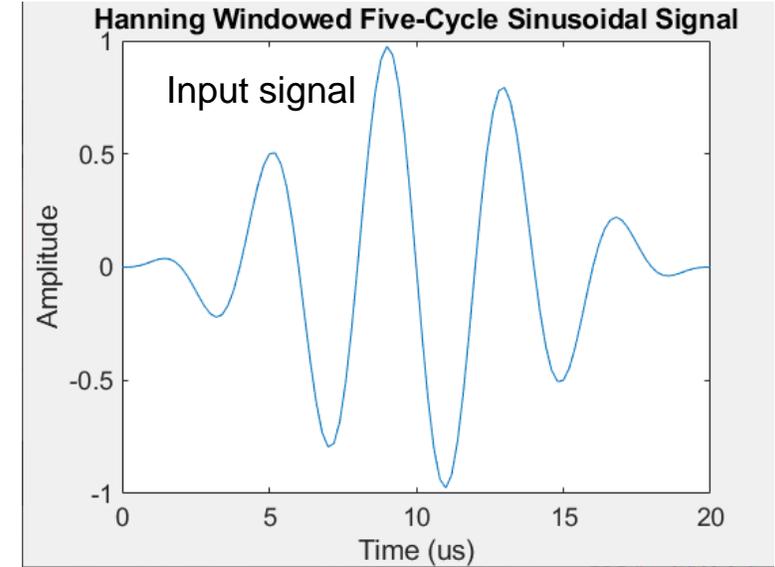
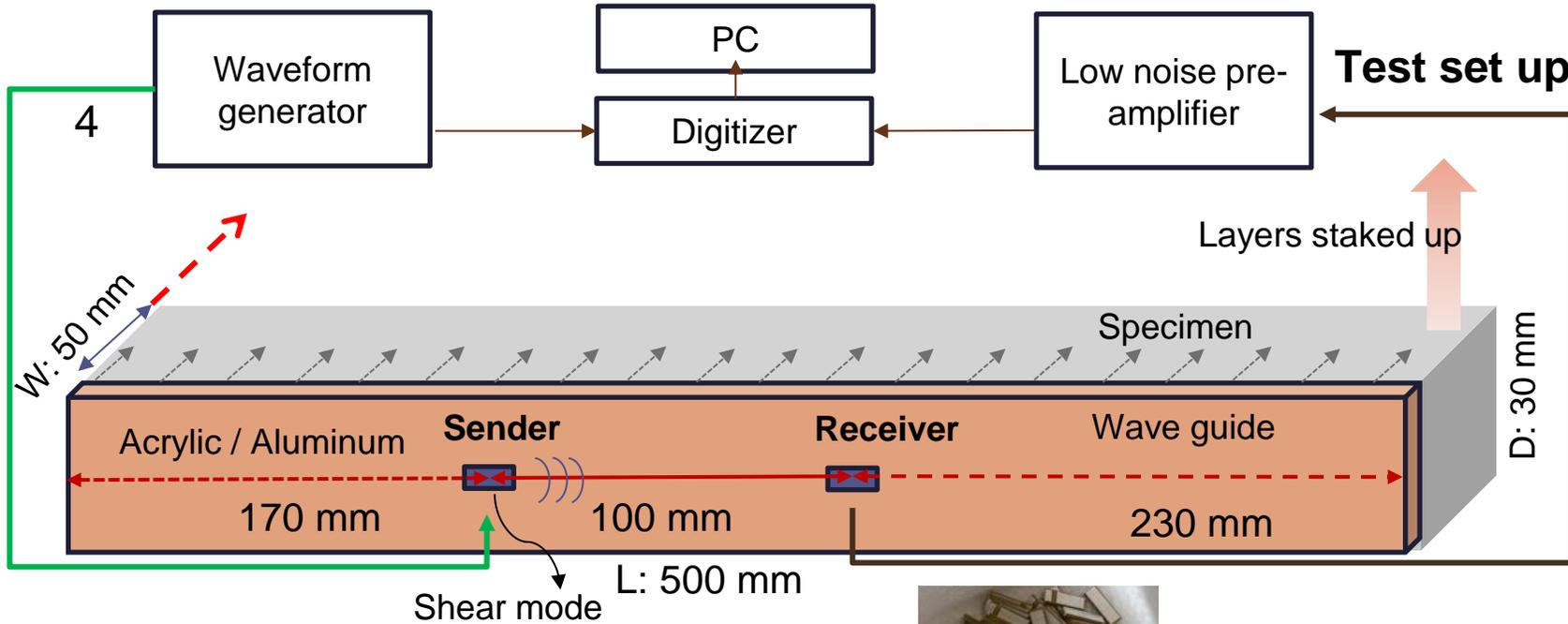
5CF10: 5mm 1 %



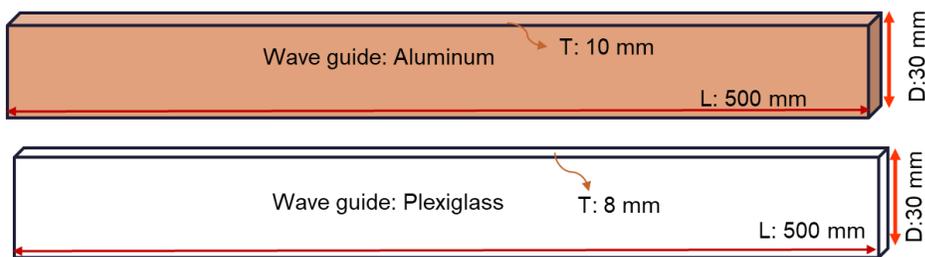
5CF20: 5mm 2 %



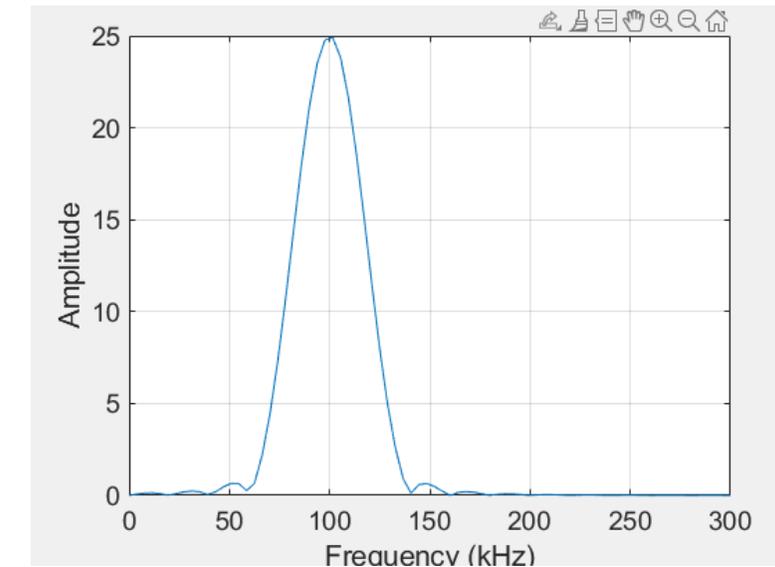
# Experimental Setup



PZT sensors (15 x 5 x 1) mm<sup>3</sup>

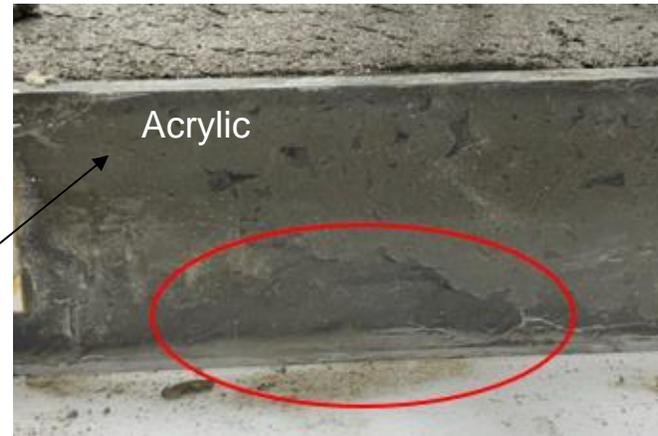
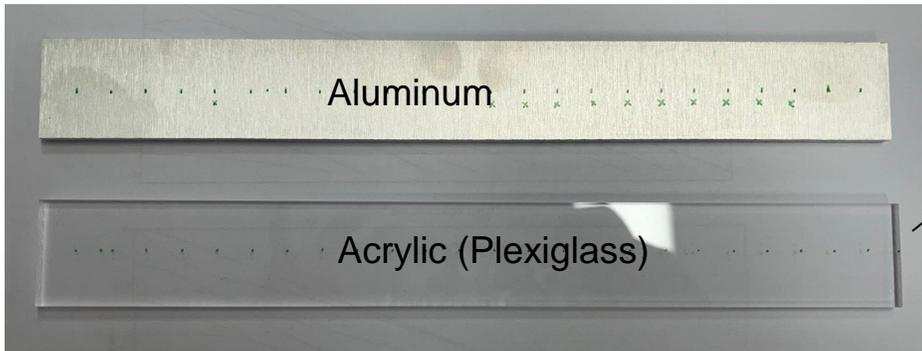


Dominated by symmetric mode (in plane motion) in the plate, which excites leaky shear waves in surrounding material



**Tests were conducted on cast specimens**  
**The specimens were tested for 2 hours right after casting**

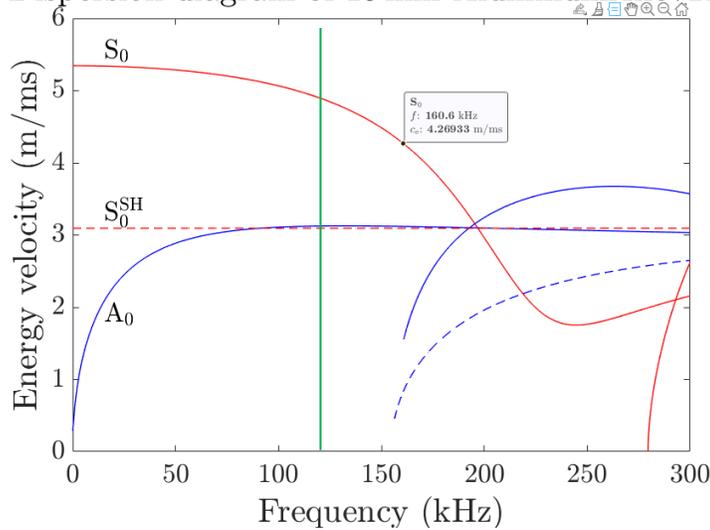
# Waveguides



Material properties

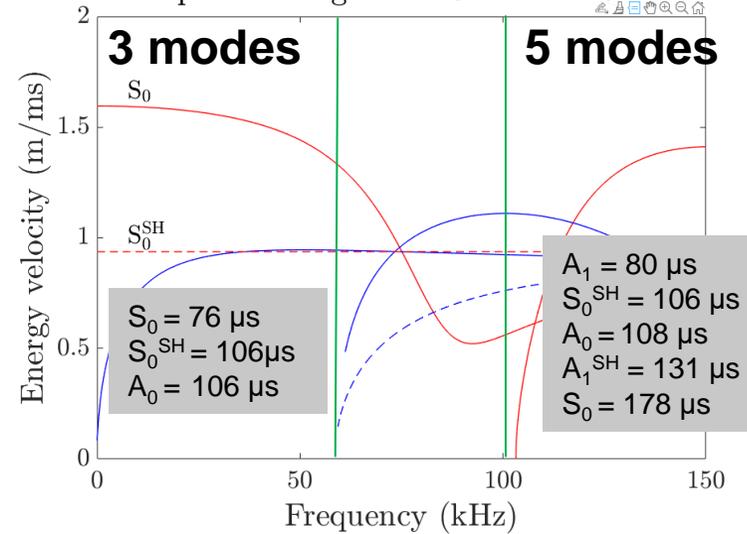
Name	Density ( $\rho$ ) kg/m <sup>3</sup>	$E$ (Gpa)
Aluminum	2710	69
Acrylic (Plexiglass)	1190	2.75

Dispersion diagram of 15 mm Aluminum Alloy 1100



Aluminum wave guide  
thickness 15 mm  
Frequency: 130 kHz and  
150 kHz

Dispersion diagram of 8 mm Plexiglass



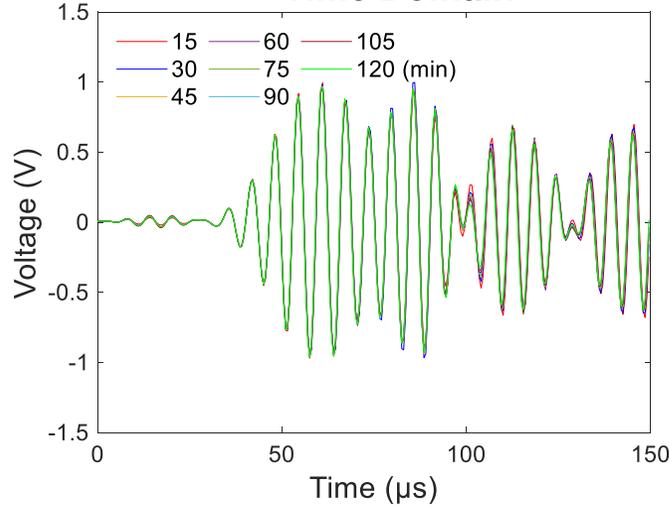
Acrylic wave guide  
thickness 8 mm  
Frequency: 60 kHz and  
100 kHz

DC Dispersion Calculator v2.4

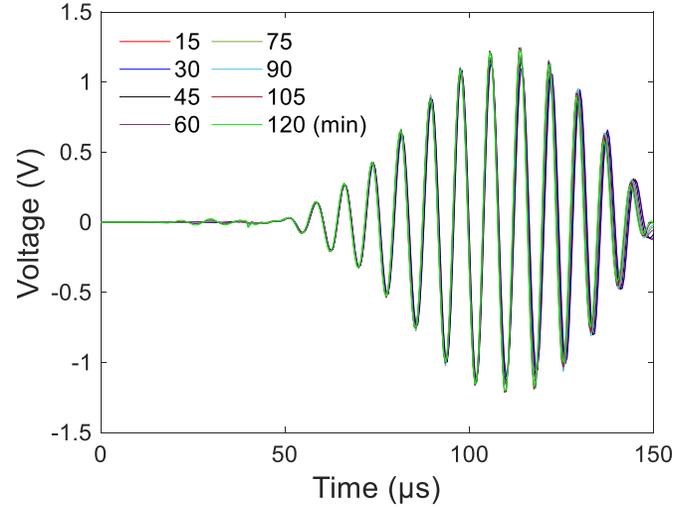
DC Dispersion Calculator v2.4

# Aluminum Waveguide

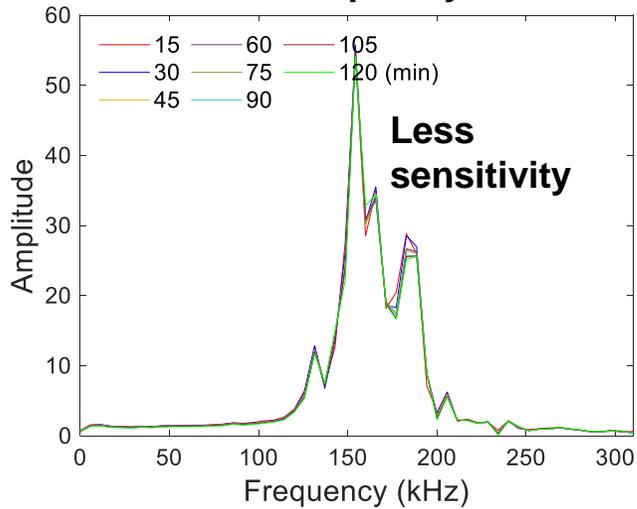
Time Domain



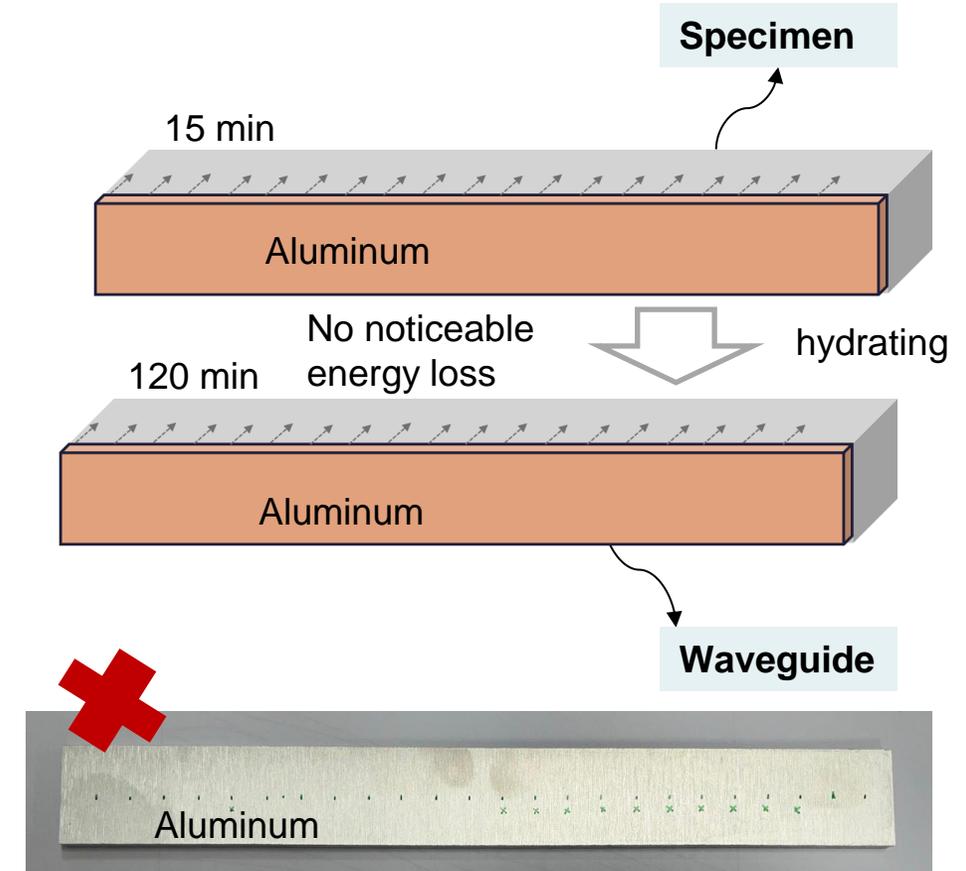
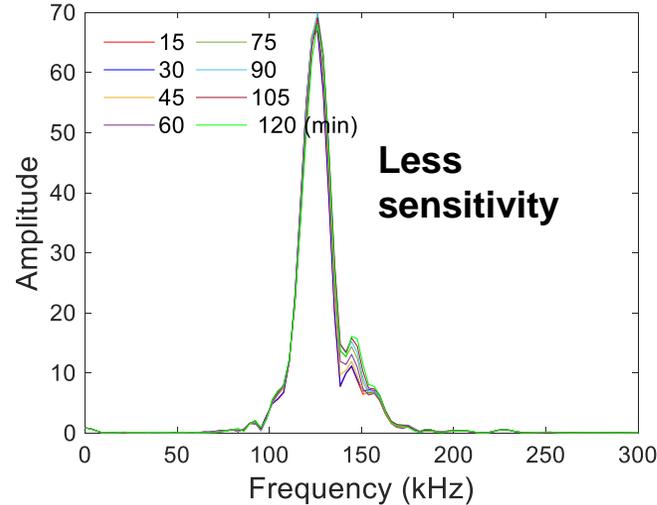
Time Domain



FFT to Frequency domain

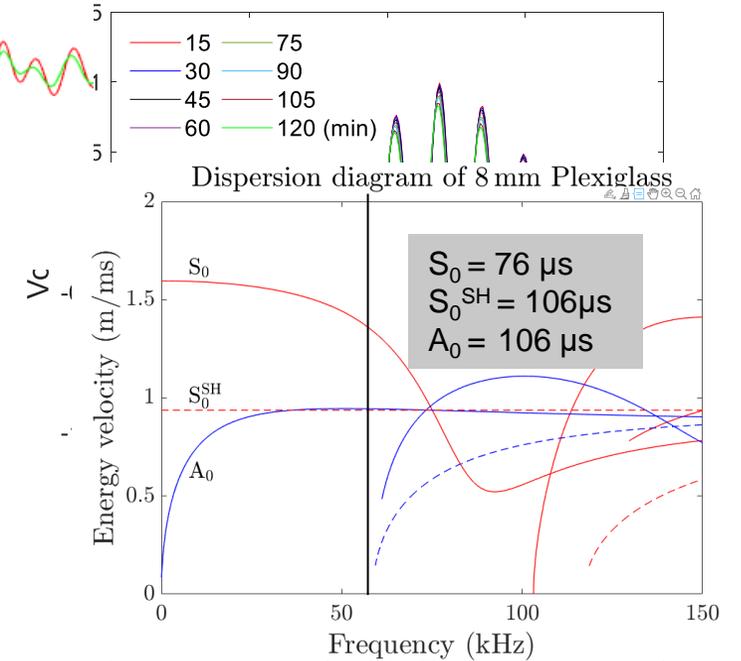
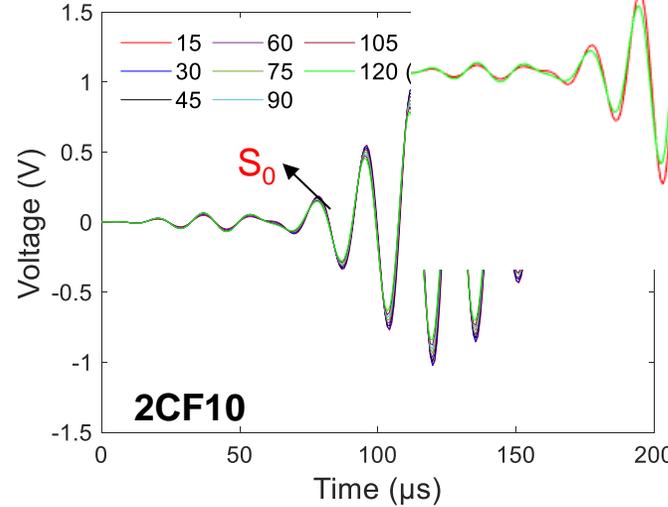
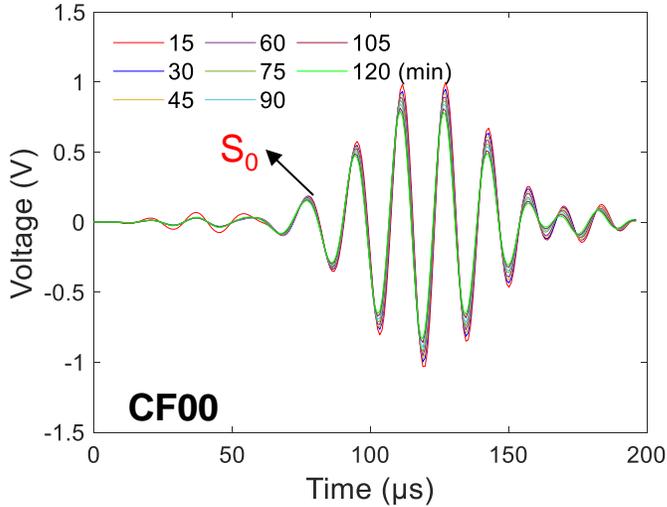


FFT to Frequency domain

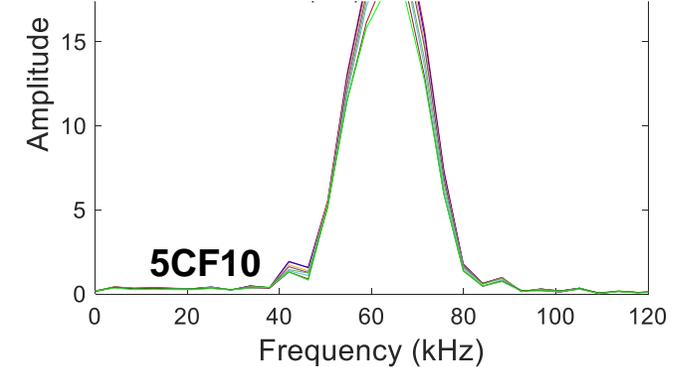
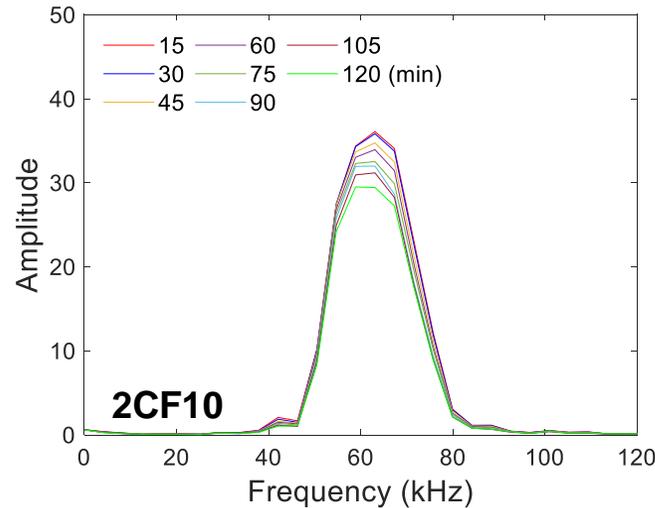
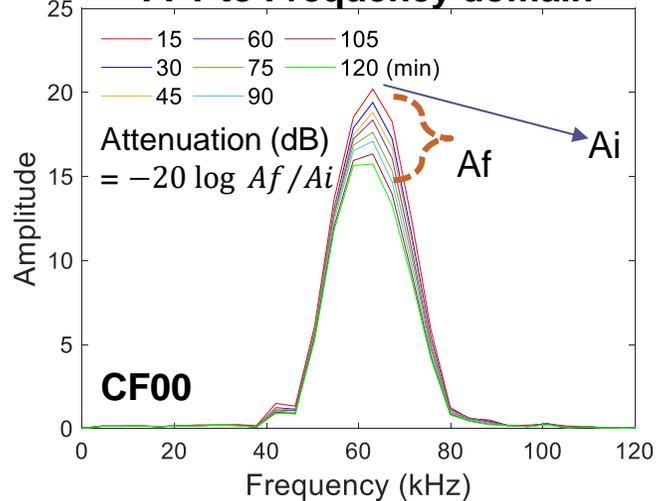


# Acrylic Waveguide: Center Frequency 60 kHz

Time Domain



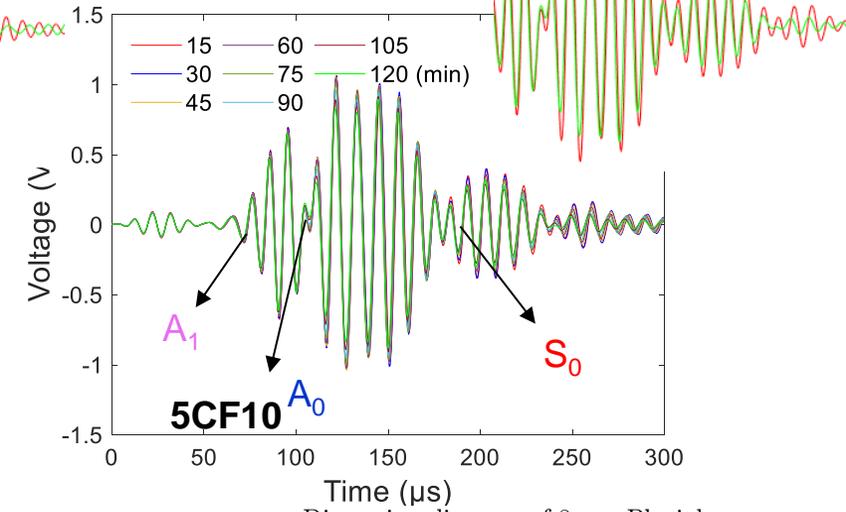
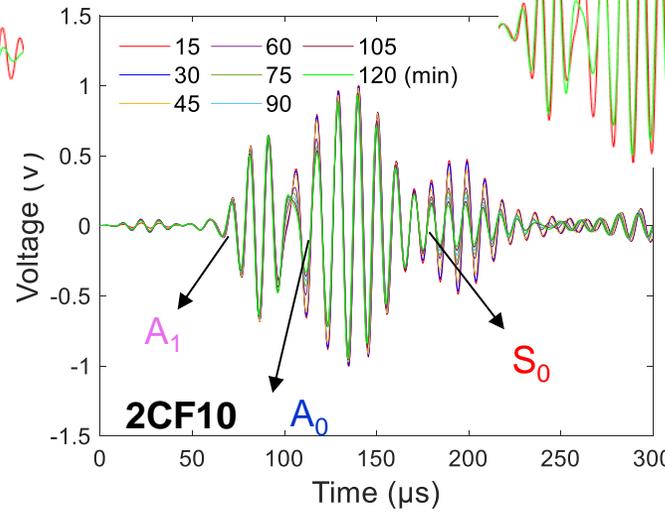
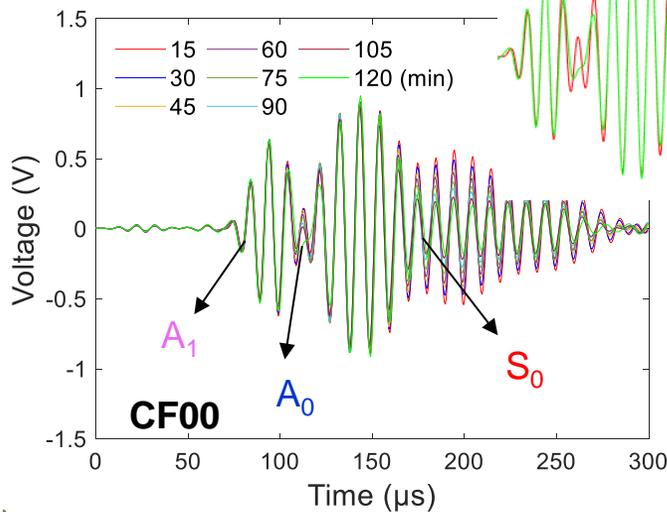
FFT to Frequency domain



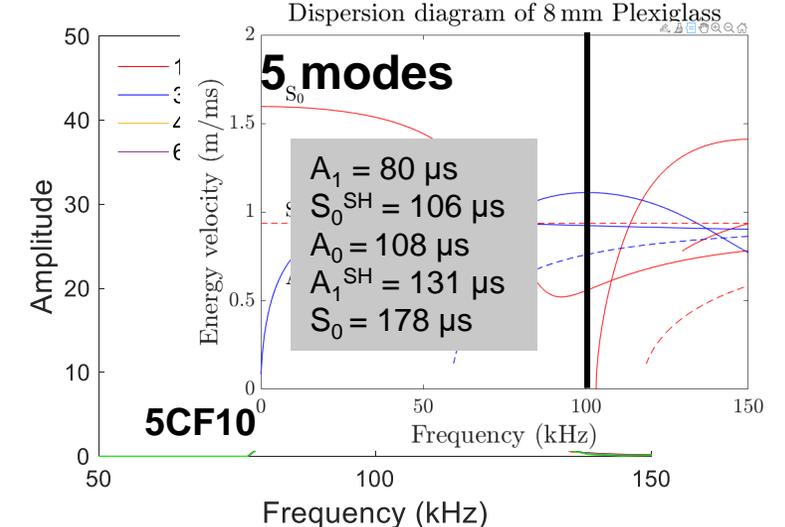
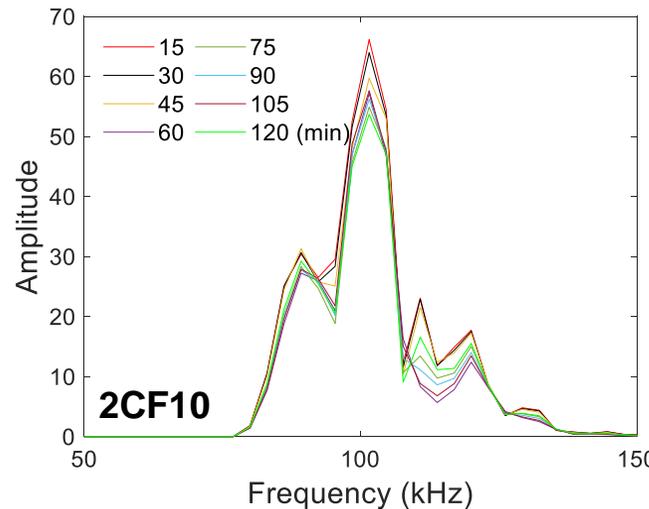
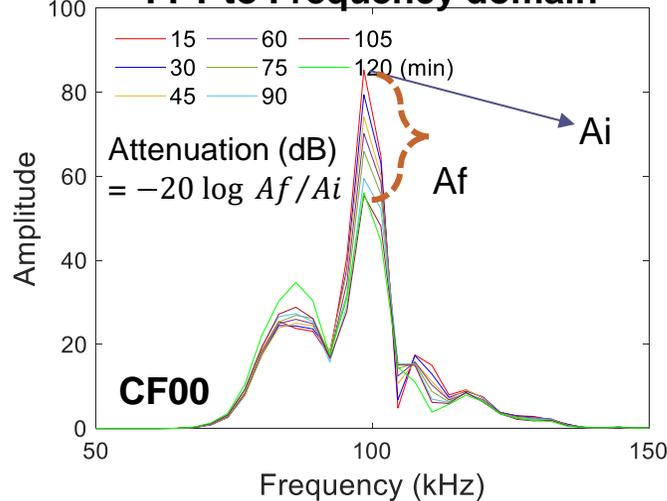
Attenuation (dB) =  $-20 \log Af / Ai$   
 $Ai$  = Initial Amplitude (15 min)  
 $Af$  = Amplitude afterwards

# Acrylic Waveguide: Center Frequency 100 kHz

**Time Domain**

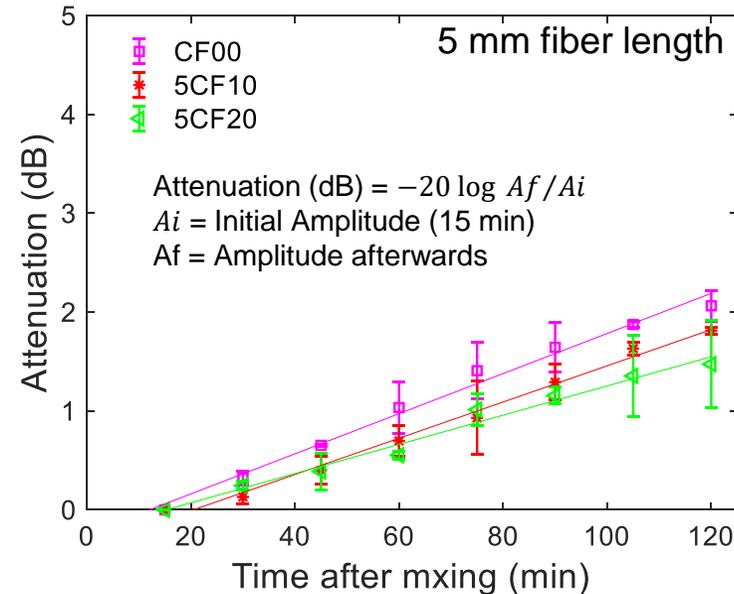
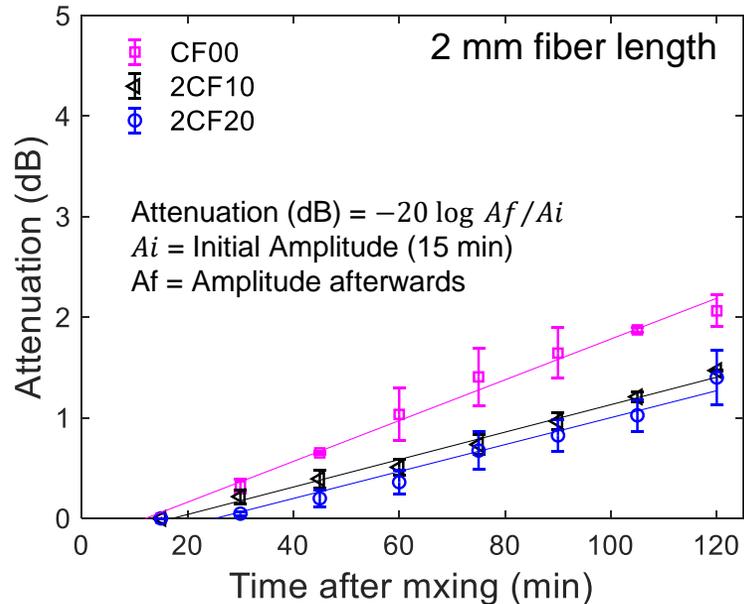


**FFT to Frequency domain**

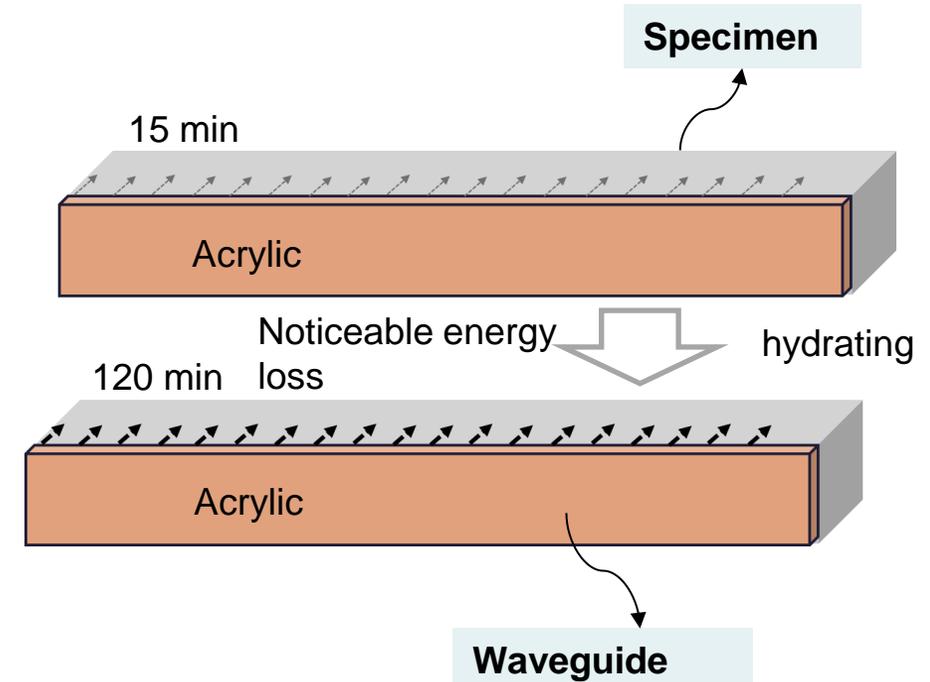


Attenuation (dB) =  $-20 \log Af / Ai$   
 $A_i$  = Initial Amplitude (15 min)  
 $A_f$  = Amplitude afterwards

# Acrylic Waveguide (60 kHz)

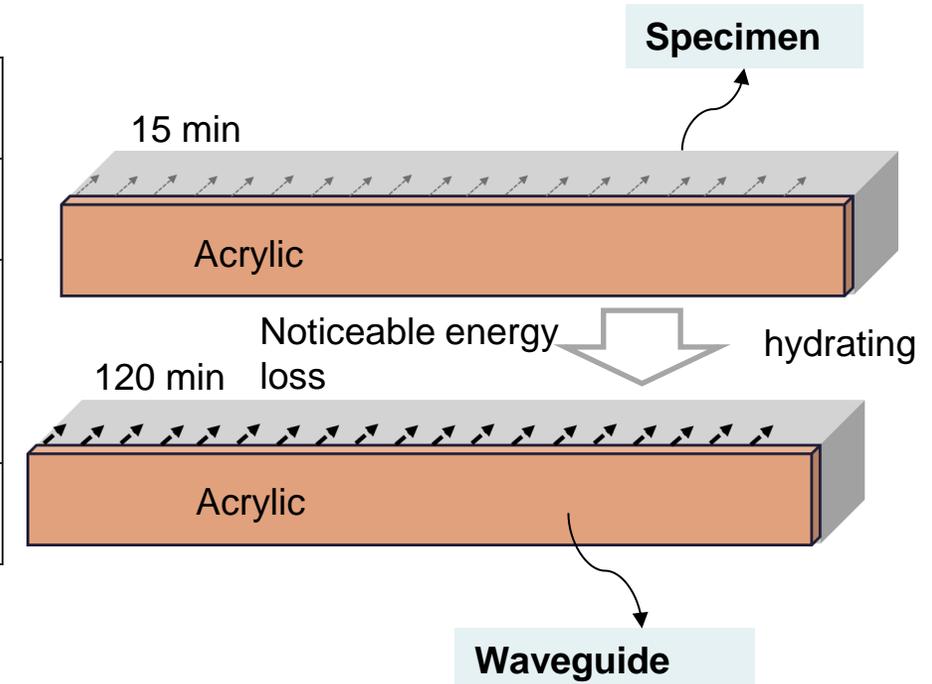
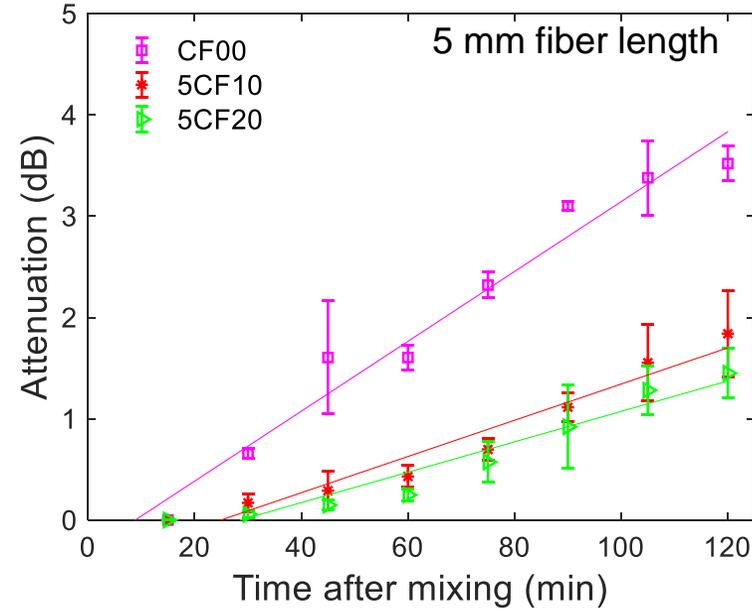
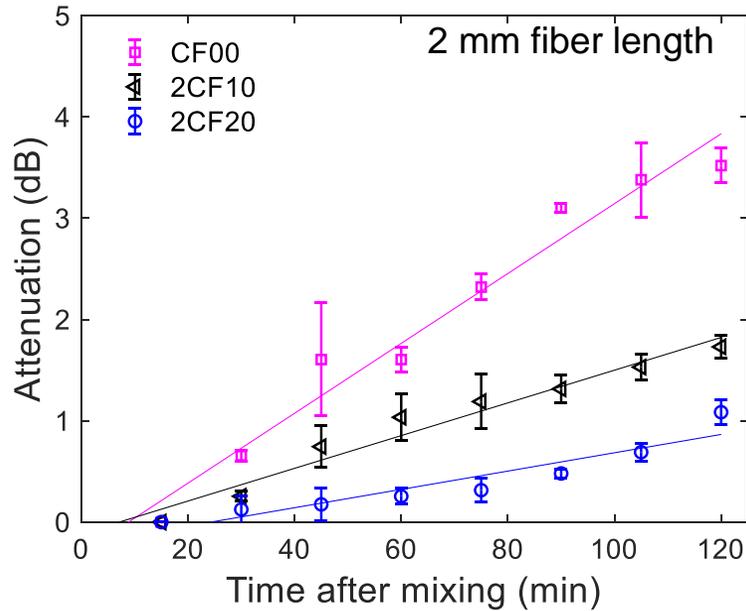


- Regardless of test variables, attenuation increases with increasing curing time
- CF00 exhibited higher attenuation when compared to specimens with CMFs
- Attenuation decreases with incorporation of CMFs, 2 % incorporation exhibited lowest increase possibly due to the delayed hydration characteristics from the inclusion of CMFs



As hydration continues in the specimen, impedance ( $\rho.v$ ) difference between the waveguide and specimen decreases leading to increase of energy loss for the propagating guided waves, eventually subjecting to higher attenuation

# Acrylic Waveguide (100 kHz)

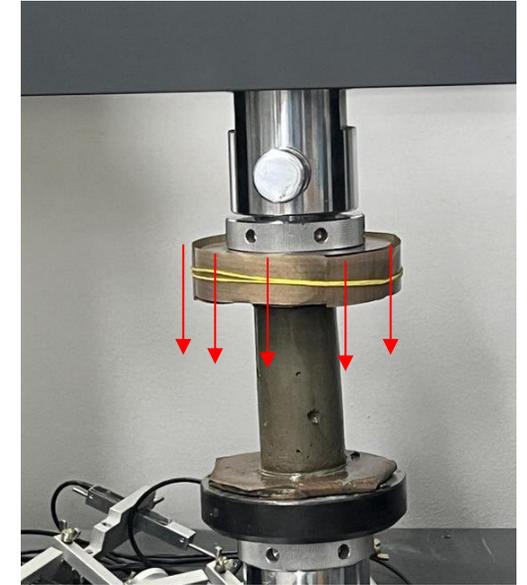
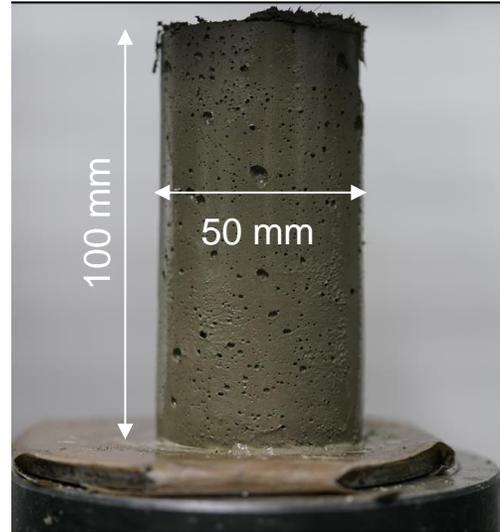


- Similarly, regardless of test variables, attenuation increases with increasing curing time
- CF00 exhibited higher attenuation when compared to specimens with CMFs
- Attenuation decreases with incorporation of CMFs, 2 % incorporation exhibited lowest increase possibly due to the delayed hydration characteristics from the inclusion of CMFs

As hydration continues in the specimen, impedance ( $\rho \cdot v$ ) difference between the wave guide and specimen decreases leading to increase of energy loss for the propagating guided waves, eventually subjecting to higher attenuation

# Green Strength Test

Loading rate: 2 mm/min



Green strength test was conducted with 15 min interval for 2 hours

**3 batches for each mix design were used to determine the green strength**

Name	W/B	OPC	Fly Ash	Silica fume	Sand	SP	CMFs	Add. Water
CF00	349	764	218	109	1091	11	0	0
2CF10	<b>x 3</b>						11 (1 %)	32
2CF20							22 (2 %)	65
5CF10							11 (1 %)	47
5CF20							22 (2 %)	94
								<b>15</b>

# Green Strength

At displacement 20 mm

CF00

15 min

30 min

45 min

60 min

75 min

90 min

105 min

120 min

5CF10

15 min

30 min

45 min

60 min

75 min

90 min

105 min

120 min

5CF20

15 min

30 min

45 min

60 min

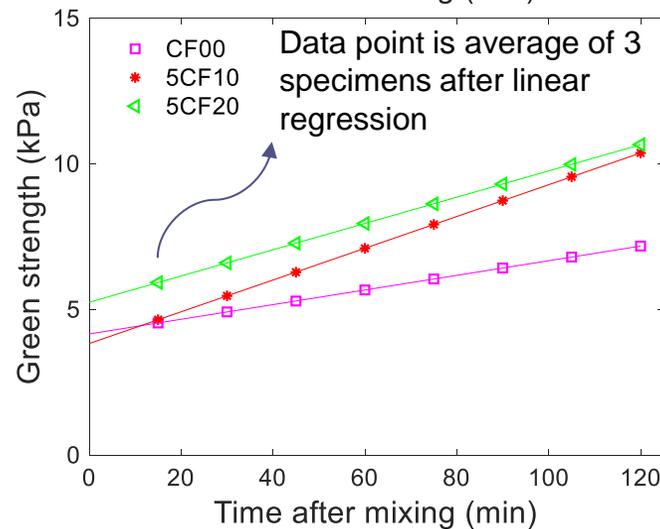
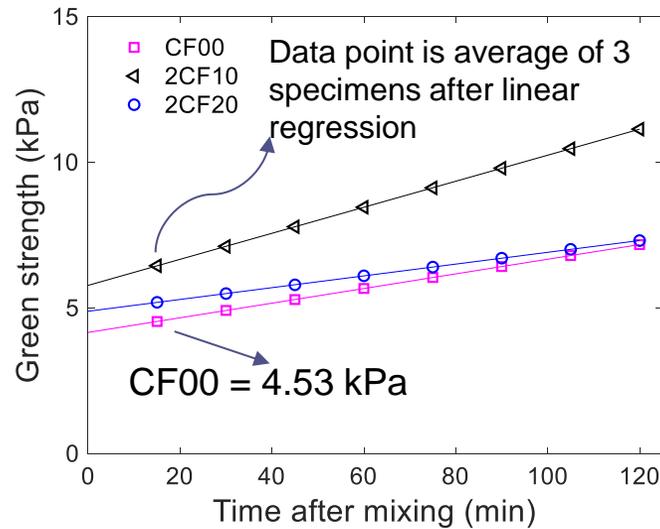
75 min

90 min

105 min

120 min

# Green Strength



# No. of Buildable Layer

$$\sigma_v(t) = \rho gh(t) \text{ [7]}$$

$$\sigma_v(t) = \frac{mg}{bl} \cdot X \text{ [8]}$$

$$X = \frac{\sigma_v(t)b}{\rho Ag}$$

$$X = \left( \frac{4\sigma_v(t)b}{\rho \pi D^2 g} \right)$$

$$X \cdot \left( \frac{\rho \pi D^2 g}{4b} \right) = \sigma_v(t) \leq \sigma(t)$$

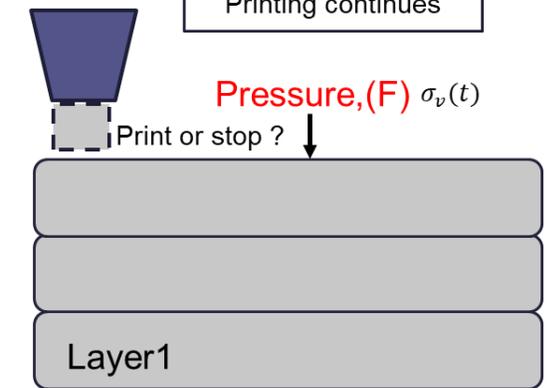
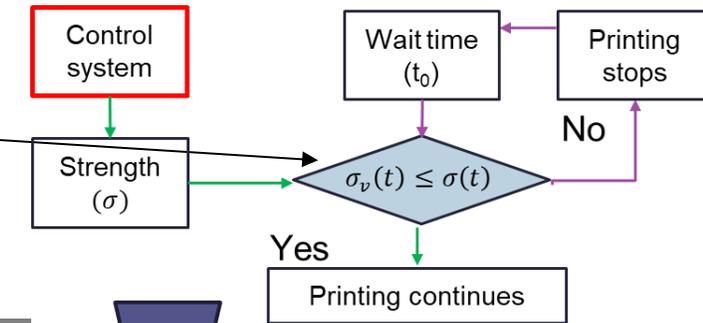
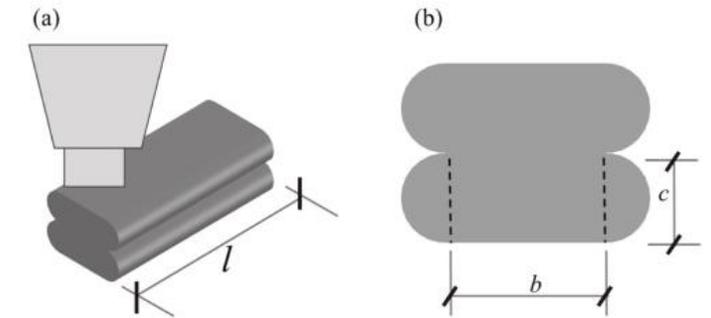
$X = \text{No. of layers}$

$\rho = \text{density of 3DPC}$   
 $g = \text{gravitational acceleration}$   
 $D = \text{nozzle diameter}$   
 $b = \text{width of printed layer}$   
 $c = \text{each layer height}$   
 $H = \text{total layer height}$   
 $\sigma(t) = \text{obtained green strength}$

$$H = (X + 1) \cdot c$$

$$H = \left( \frac{\sigma_v(t)b}{\rho Ag} + 1 \right) \cdot c$$

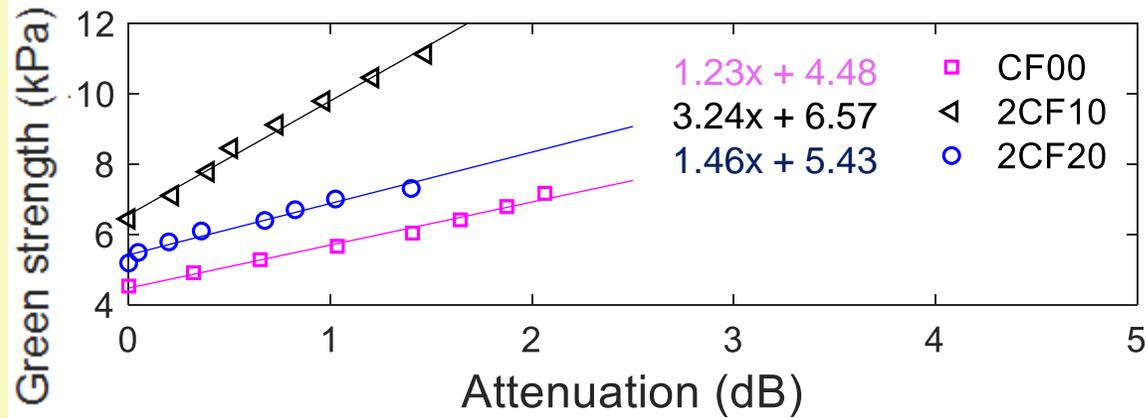
For  $H = 5$   
 1.89 kPa <  $\sigma(t)$   
 Printing continues  
 For  $X = 12$  (critical height)  
 4.53 kPa =  $\sigma(t)$   
 Printing stops



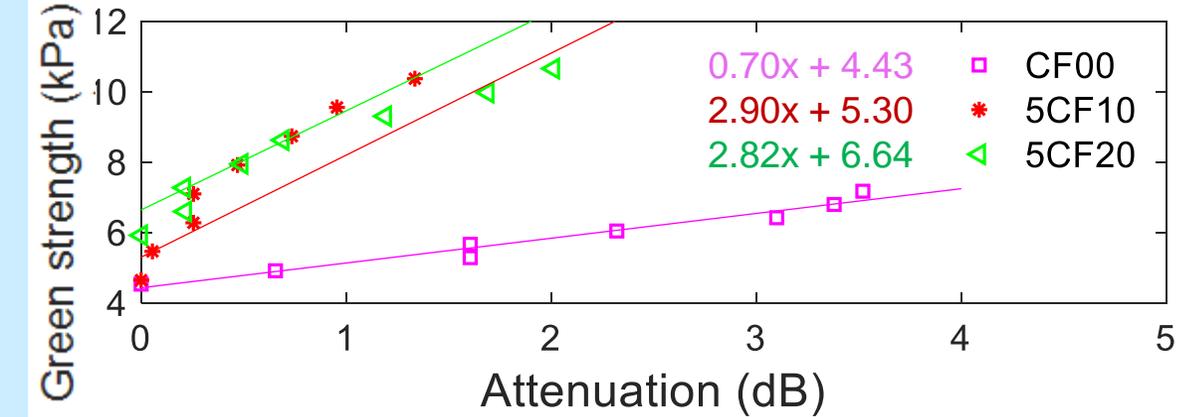
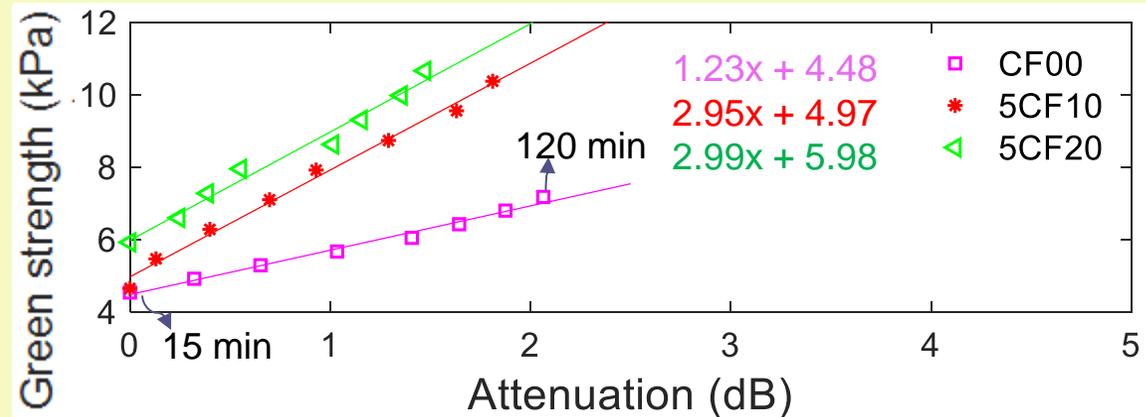
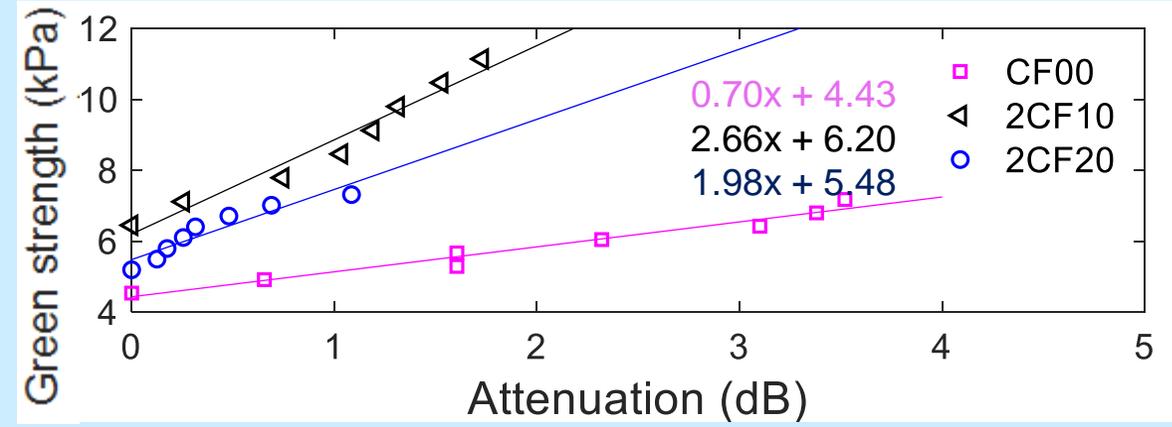
[7] Panda, Biranchi, Jian Hui Lim, and Ming Jen Tan. "Mechanical properties and deformation behaviour of early age concrete in the context of digital construction." *Composites Part B: Engineering* 165 (2019): 563-571.  
 [8] Zhang, Yu, et al. "Study on the predictive model for continuous build height of 3D printed concrete (3DPC) based on printability and early mechanical properties." *Journal of Building Engineering* 99 (2025): 111640.

## Correlations Between Attenuation and Green strength

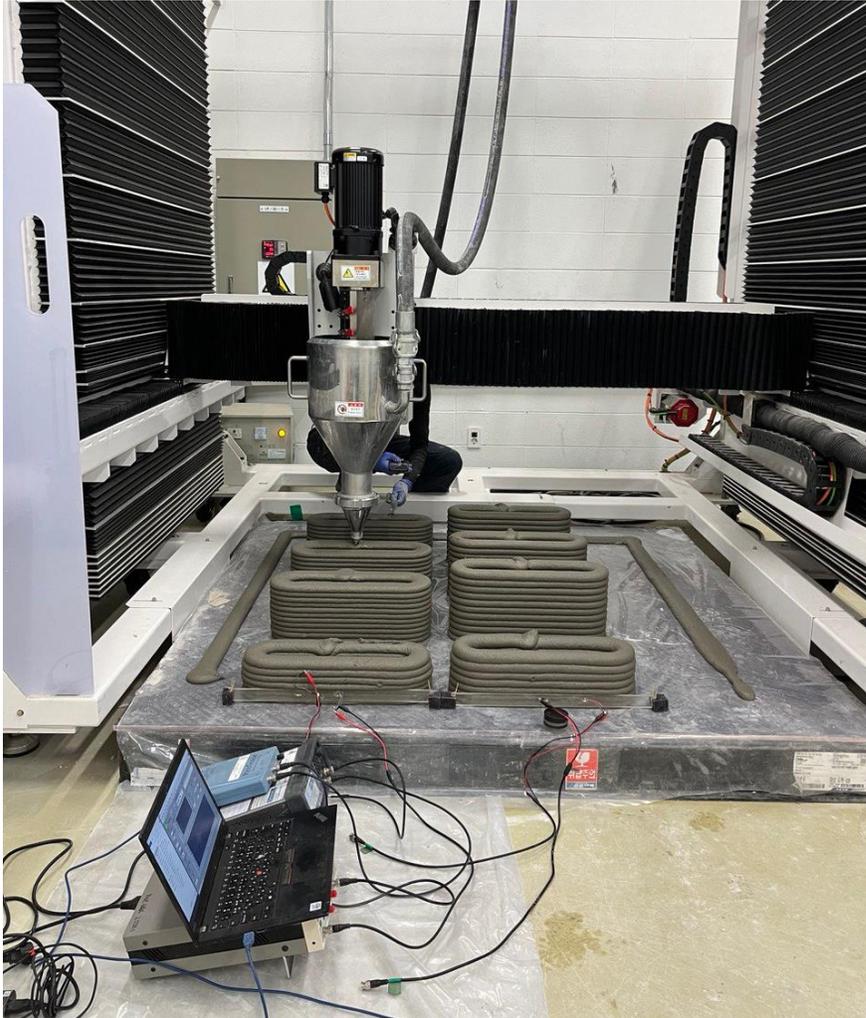
60 kHz



100 kHz

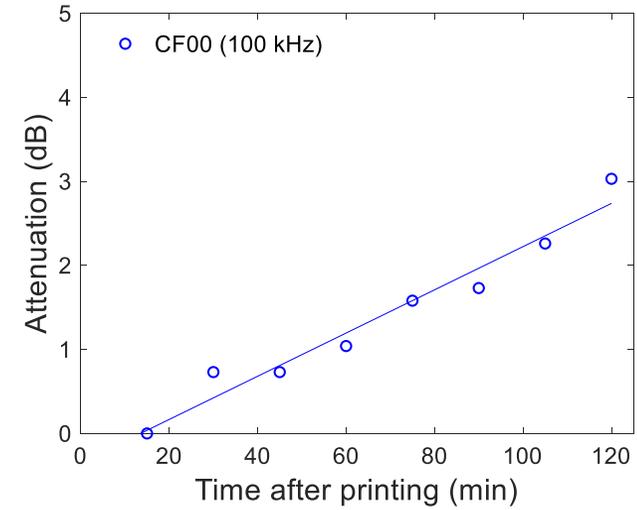
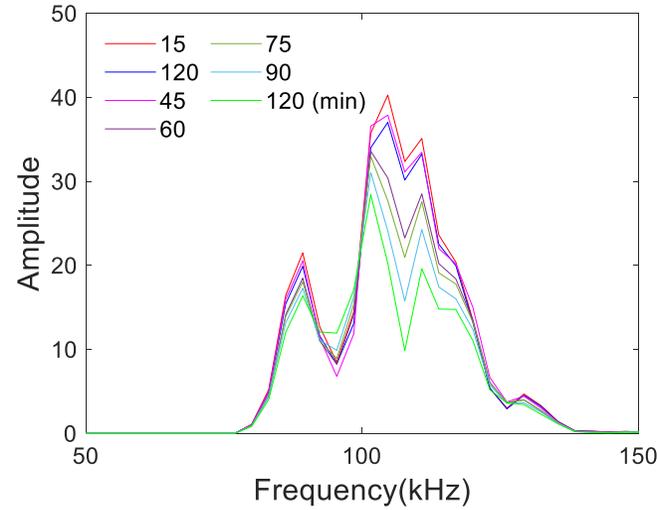
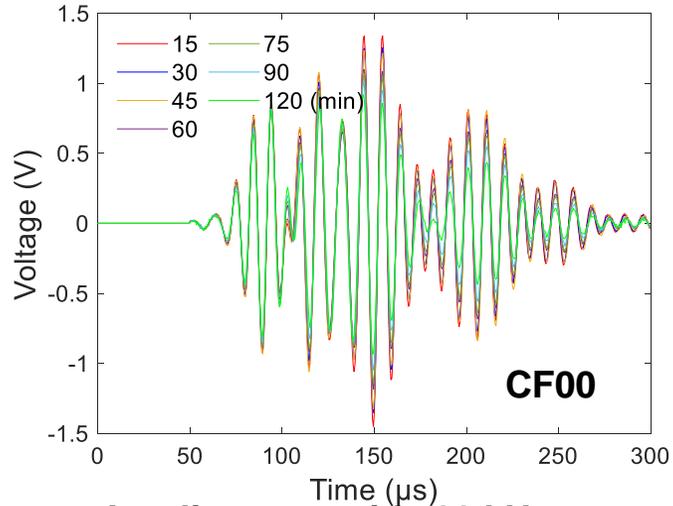


# Inline Application

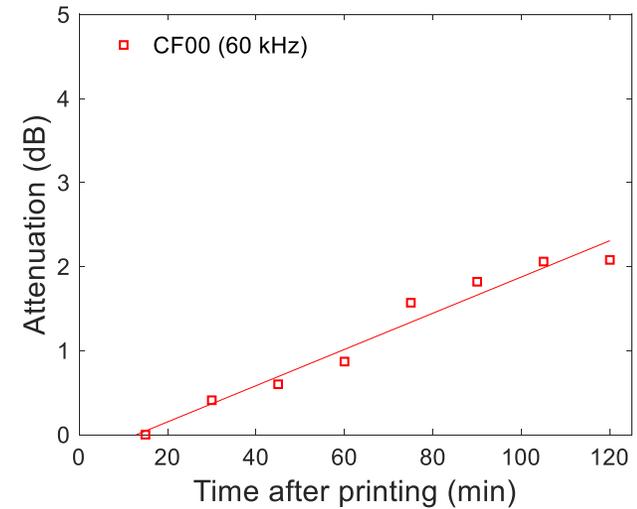
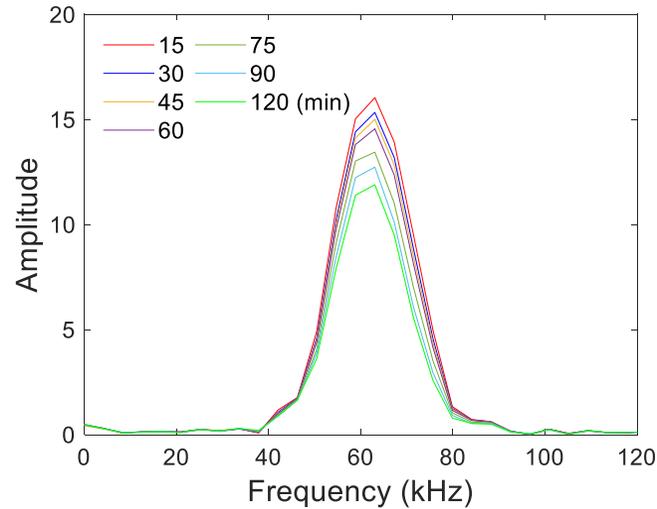
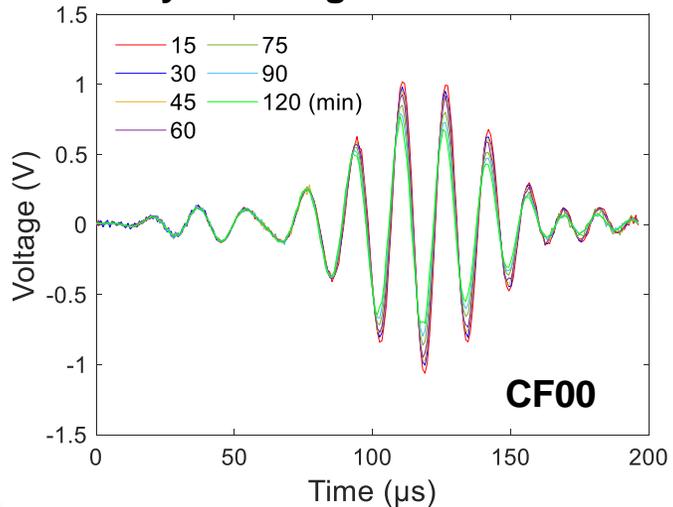


# 3D Printed Specimen

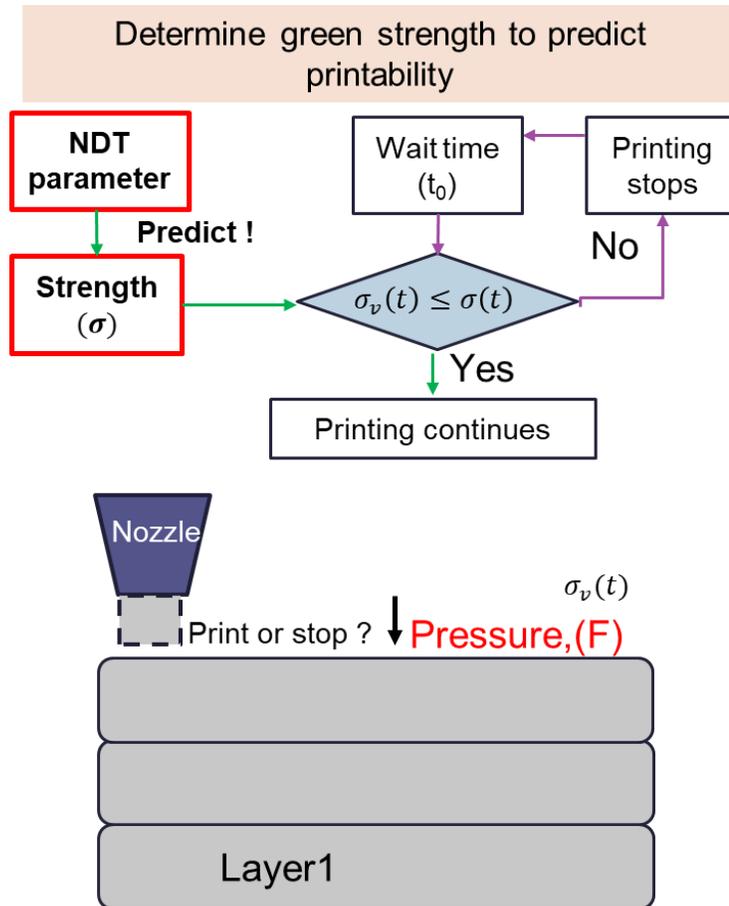
## Acrylic waveguide 100 kHz



## Acrylic waveguide 60 kHz



# Conclusion



1. This study conducted the effectiveness of guided wave to monitor of buildability for 3DPC
2. Acrylic is found to be more effective, given the material property at this stage
3. Correlation between green strength and attenuation was developed
4. No. of buildable layer can be indirectly predicted using guided wave technique



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**Sustainable Structural  
Systems & Materials lab**

**THANK YOU**