

Modeling of entrained air dissolution and long-term saturation:

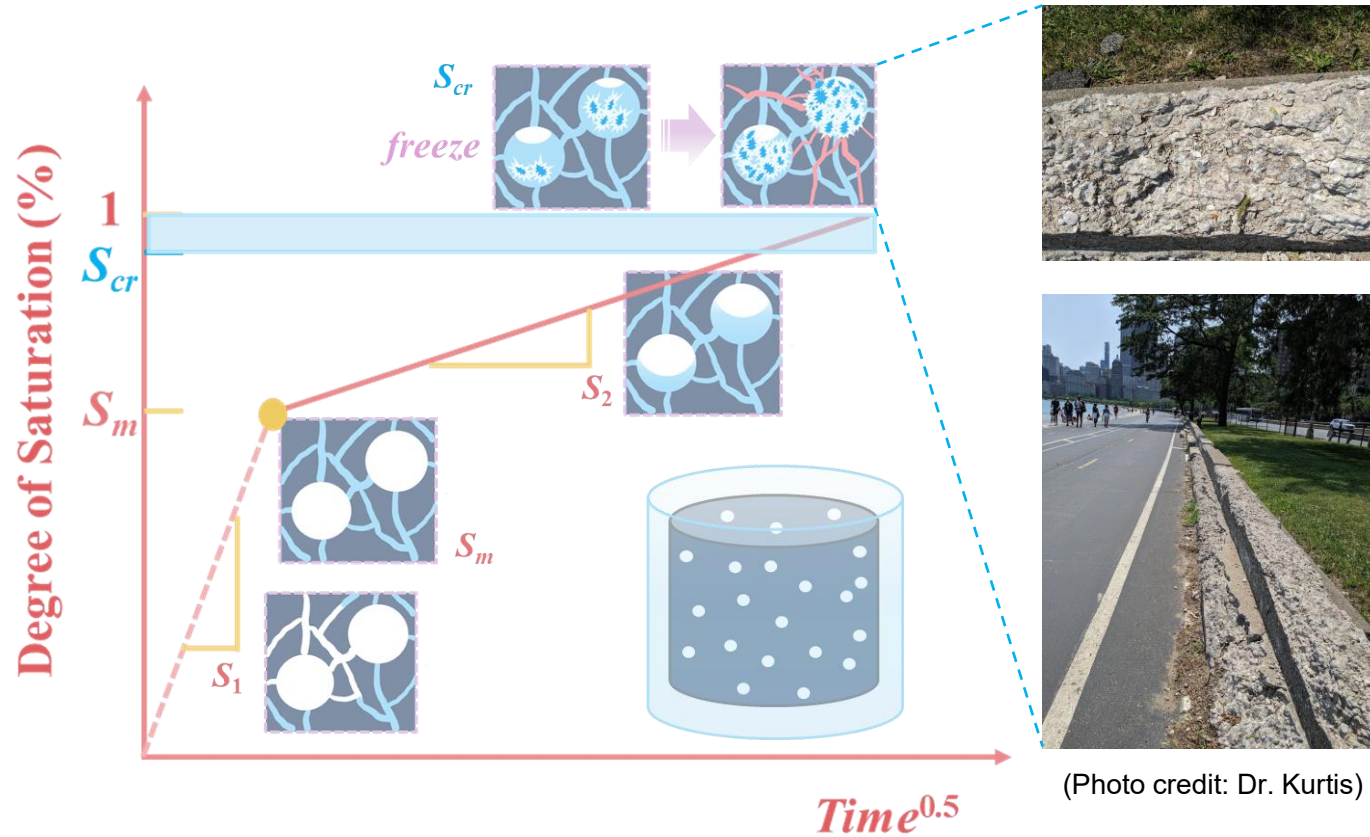
Role of microstructure in emerging cementitious materials

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1. Introduction & motivation



(Photo credit: Dr. Kurtis)

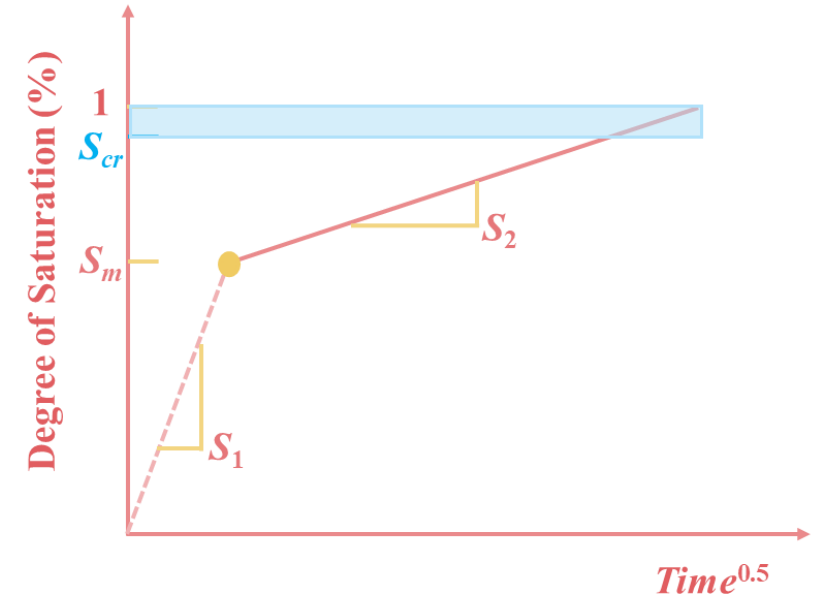
- Background

- Water saturation governs **freeze-thaw resistance** and **long-term durability** in cementitious materials.
- Saturation = Stage 1 (S_1) + Stage 2 (S_2) :
 - S_1 : Rapid capillary suction
 - S_2 : Slow air dissolution → controls S_{cr} (~86%)
- Once $S \geq S_{cr}$, freeze-thaw damage occurs even with enough air content.

Longer S_2 → delayed S_{cr} → higher freeze-thaw durability

1. Introduction & motivation

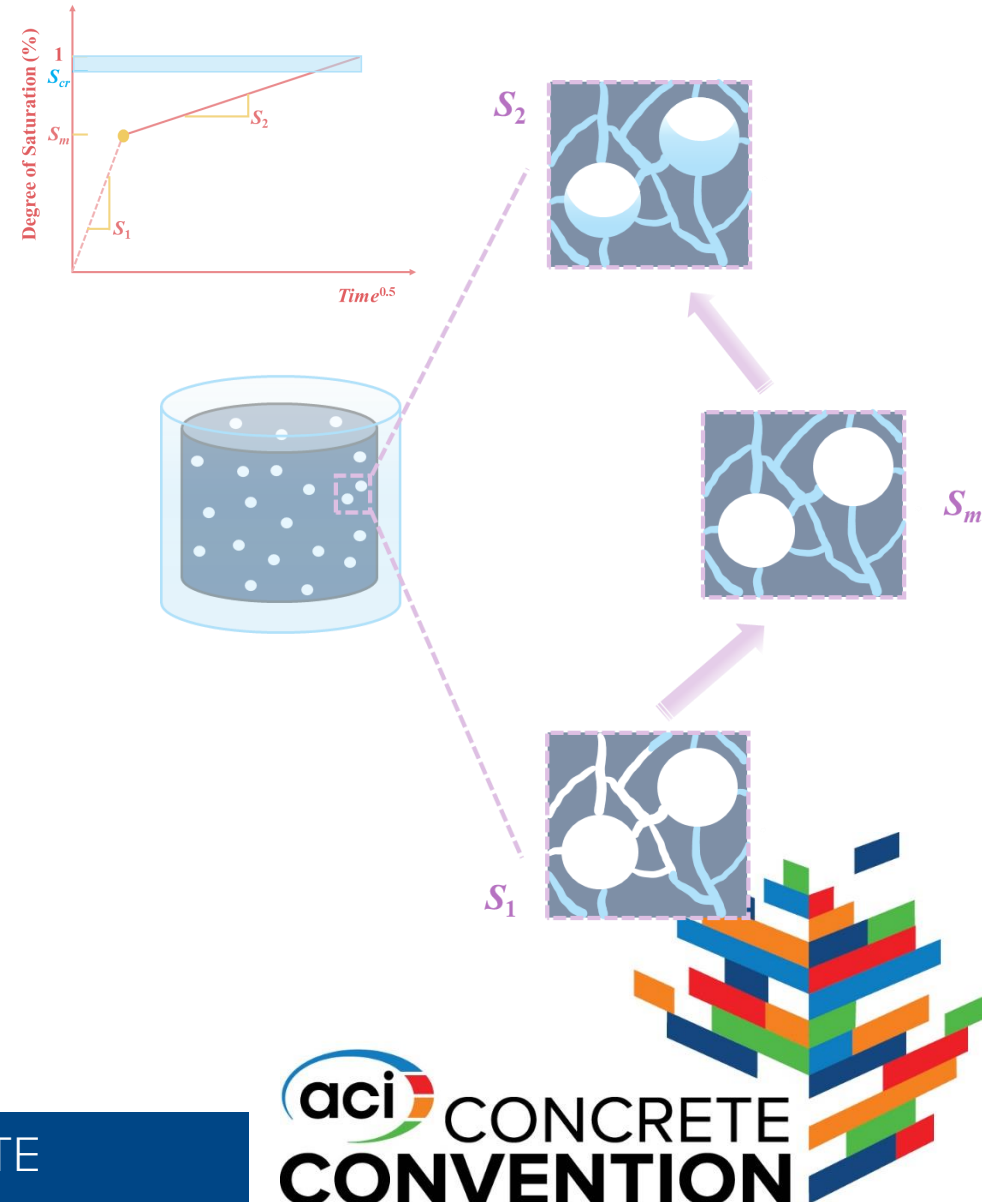
- Knowledge gaps
 - Focus mainly on **OPC** systems.
 - Prior work: **Air-void optimization**, but lacks **long-term saturation kinetics (S_2)**.
 - Research on **emerging cementitious materials** (LC³, CSA, geopolymers) is limited.
- Research gaps
 - No unified framework to **quantify the timescale of S_2** in different cementitious systems.
 - Current models insufficiently capture saturation behavior of **emerging low-carbon cements**.



(Photo credit: Dr. Kurtis)

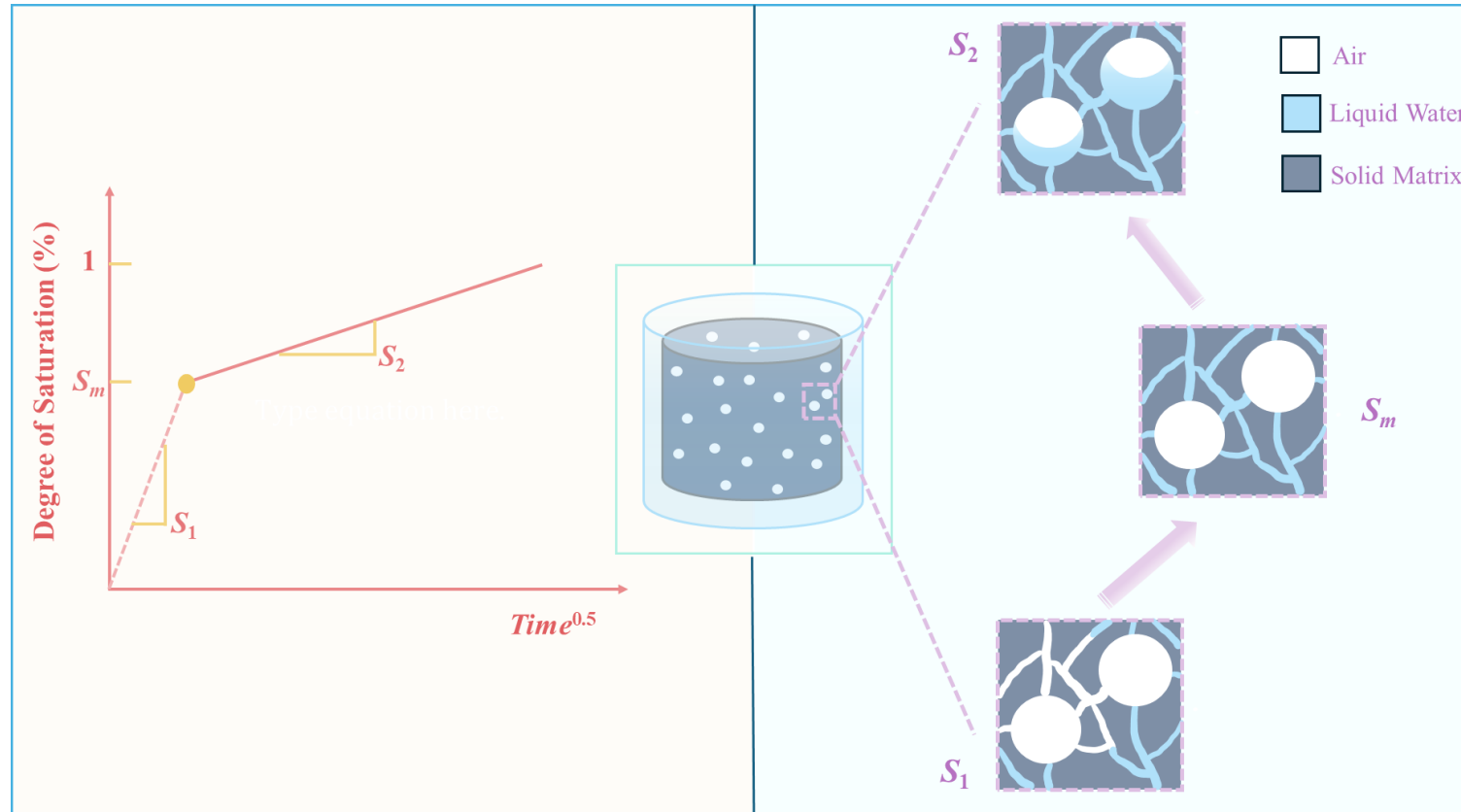
1. Introduction & motivation

- Significance
 - Describe dissolution, diffusion, and advective filling in cementitious materials.
 - Link **microstructural parameters** to **saturation kinetics**.
 - Enable reliable prediction of **freeze-thaw**.
- Objective
 - Provide a **generalizable modeling framework** that applies across OPC and emerging systems.
 - Advance predictive understanding of long-term saturation.
 - Support the design of durable, sustainable cementitious systems.



2. Air dissolution and long-term saturation in cementitious materials

- Air voids and water saturation in cementitious materials



S_1 : Capillary absorption

- Rapid process
- Capillary suction-driven

S_2 : Air dissolution-diffusion

- Slow, long-term process
- Laplace pressure

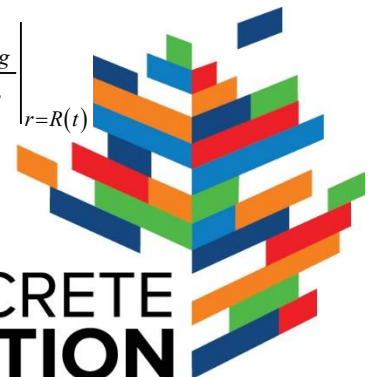
$$P_g = P_0 + \frac{2\sigma}{R}$$

- Henry's Law

$$C_g = P_g \cdot k_H$$

- Diffusion flux

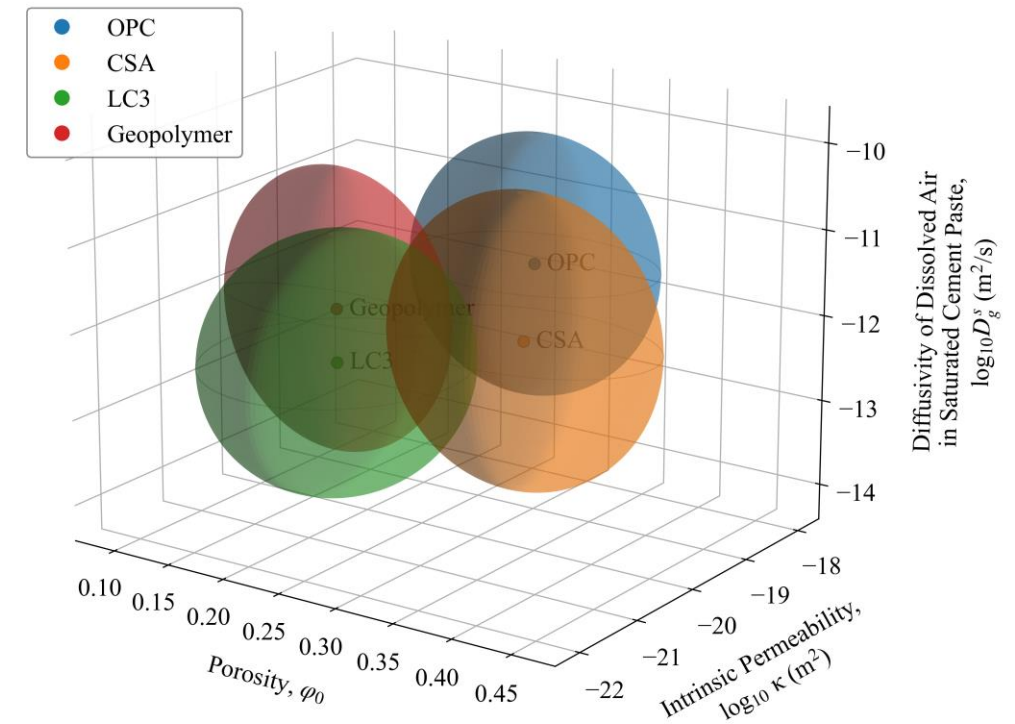
$$J(R, t) = -D \frac{\partial C_g}{\partial r} \bigg|_{r=R(t)}$$



2. Air dissolution and long-term saturation in cementitious materials

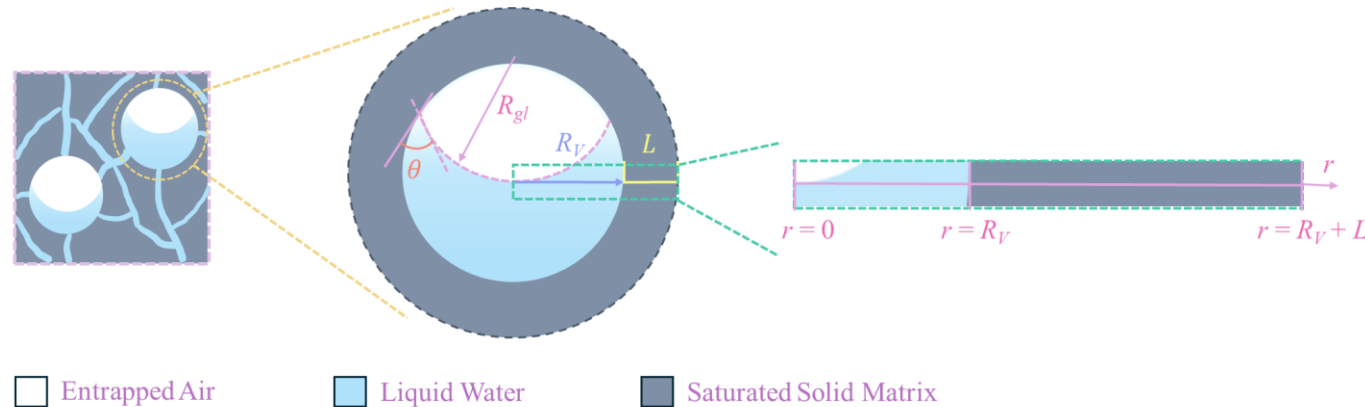
- Variations in physical and microstructural properties across cementitious systems

Parameters	OPC System (Baseline)	CSA Cement System	LC ³ System	Geopolymer System
Bulk porosity, φ_{bulk}	0.2–0.4	~0.23–0.45	~0.1–0.3	0.1–0.3
Intrinsic permeability, κ (m ²)	10 ⁻¹⁸ –10 ⁻²⁰	10 ⁻¹⁹ –10 ⁻²¹	10 ⁻¹⁹ –10 ⁻²²	10 ⁻²⁰ –10 ⁻²¹
Diffusivity of dissolved air in saturated hydrated cement paste, D_g^s (m ² /s)	10 ⁻¹⁰ –10 ⁻¹³	~10 ⁻¹¹ –10 ⁻¹⁴	10 ⁻¹¹ –10 ⁻¹⁴	~10 ⁻¹¹ –10 ⁻¹⁴
Tortuosity, τ	$\tau = \varphi_{eff} \cdot \varphi_{seg}^{-3.15}$	1.5 × OPC	3–4 × OPC	1.2–2 × OPC
Air void-paste ITZ thickness, δ (μm)	~30	~0.65 × OPC	~0.67 × OPC	No distinct porous ITZ observed
ITZ porosity, φ_{ITZ}	~2–3 × bulk paste	~0.8 × OPC	~0.75 × OPC	Comparable to bulk paste



3. Mechanism and modeling of air dissolution and water filling

- Physical description of the process



- Governing equations -- Single void dissolution kinetics (SVDK) model (Smith et al., 2020)

- Gas mass in the spherical void
- Liquid water mass in the spherical void
- The concentration of dissolved gas in the liquid

$$\frac{\partial m_g}{\partial t} = 4\pi R_v^2 \left(\underbrace{D_g^s \frac{\partial C_g}{\partial r}}_{\text{diffusion}} \bigg|_{r=R_v^+} + \underbrace{\frac{\kappa}{\eta} C_g \frac{\partial P_l}{\partial r}}_{\text{advection}} \bigg|_{r=R_v^+} \right)$$

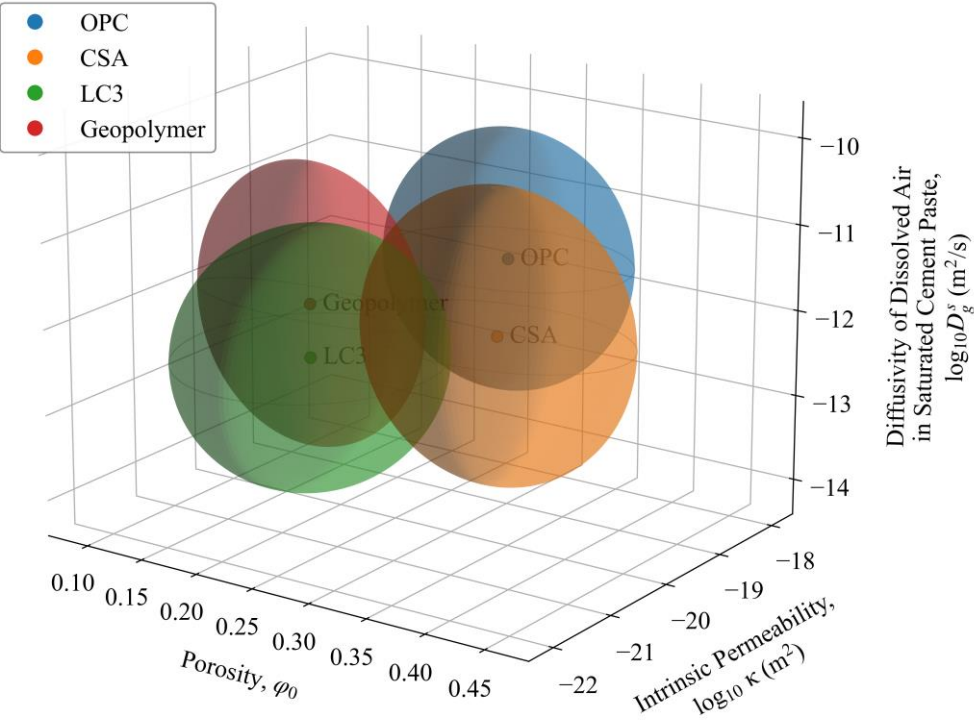
$$\frac{\partial m_l}{\partial t} = 4\pi R_v^2 \left(\underbrace{-D_g^s \frac{\partial C_g}{\partial r}}_{\text{diffusion}} \bigg|_{r=R_v^+} + \underbrace{\frac{\kappa}{\eta} (\rho_l - C_g) \frac{\partial P_l}{\partial r}}_{\text{advection}} \bigg|_{r=R_v^+} \right)$$

$$\frac{\partial C_g}{\partial t} = \underbrace{\frac{D_g^s}{\phi_0} \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C_g}{\partial r} \right)}_{\text{diffusion}} + \underbrace{\frac{\kappa R_v (R_v + L)}{\phi_0 \eta} \frac{[P_l(R_v + L, t) - P_l(R_v, t)]}{r^2 L} \frac{\partial C_g}{\partial r}}_{\text{advection}}$$

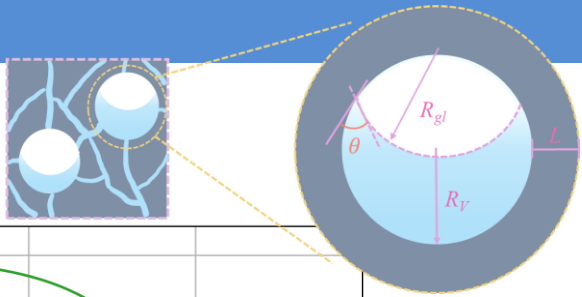
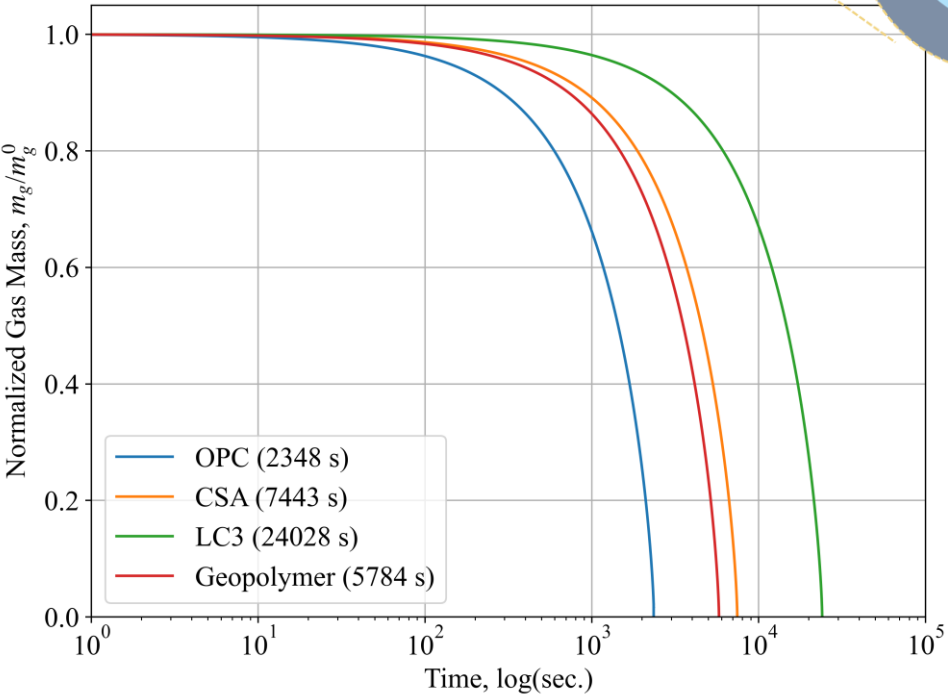


4. Parametric analysis of saturation kinetics

- Comparison across different cementitious systems



Physical Parameters	OPC	CSA	LC ³	Geopolymer
ϕ_0	0.3	0.34	0.2	0.2
κ , (m^2)	1×10^{-19}	1×10^{-20}	3.16×10^{-21}	3.16×10^{-21}
D_g^i , (m^2/s)	3.16×10^{-12}	1×10^{-12}	3.16×10^{-13}	1.34×10^{-12}

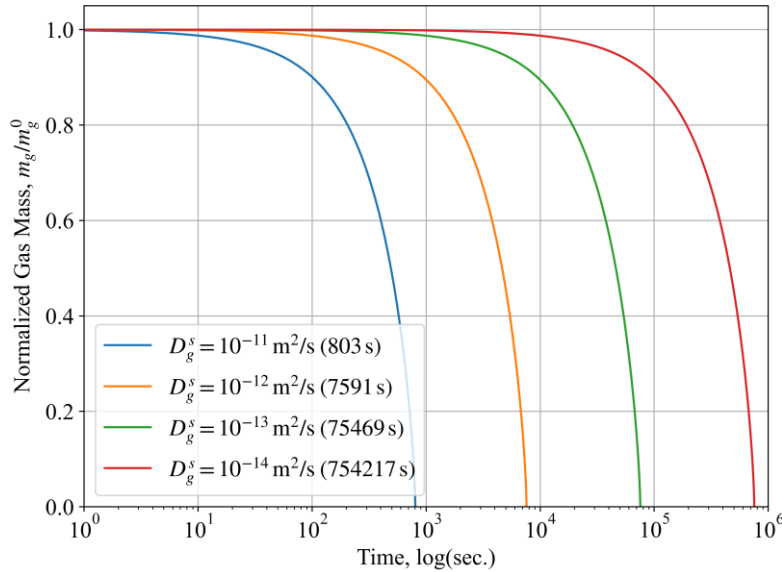
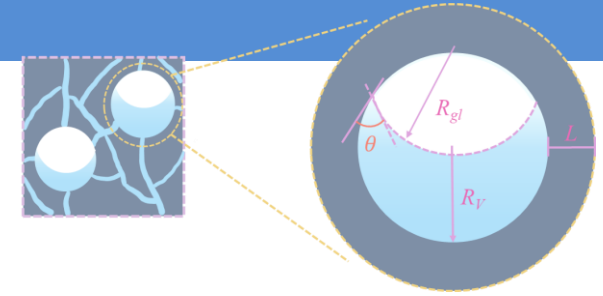


$R_v = 10 \mu m$ $L = 1 mm$
 $\theta = 20^\circ$ $m_t = 0.5$



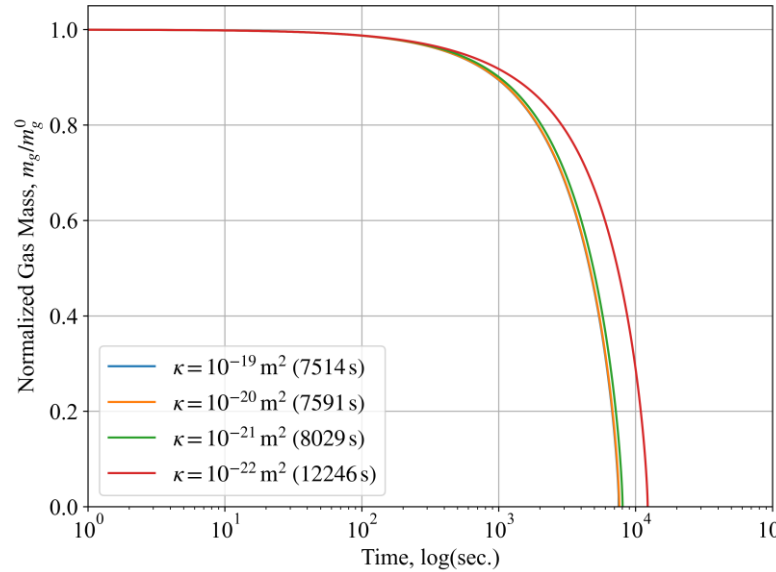
4. Parametric analysis of saturation kinetics

- Transport-related physical properties



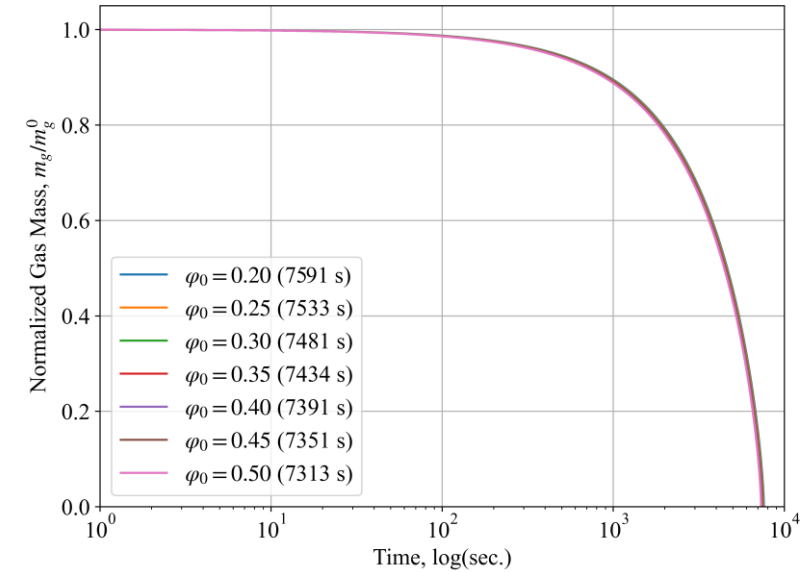
Diffusivity of dissolved air in saturated cement paste, D_g^s

$$\kappa = 1 \times 10^{-20}, \varphi_0 = 0.2, R_v = 10 \text{ } \mu\text{m}, L = 1 \text{ mm}, \theta = 20^\circ$$



Intrinsic permeability of cement paste, κ

$$D_g^s = 1 \times 10^{-12}, \varphi_0 = 0.2, R_v = 10 \text{ } \mu\text{m}, L = 1 \text{ mm}, \theta = 20^\circ$$

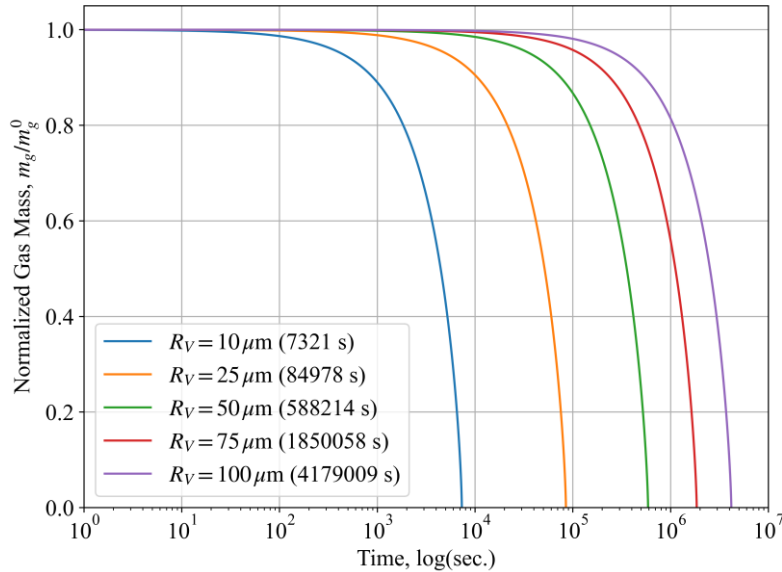
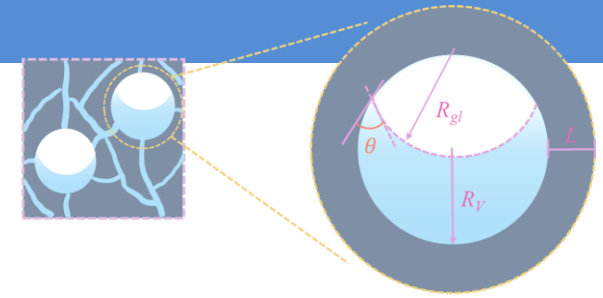


Porosity of cement paste matrix, φ_0

$$D_g^s = 1 \times 10^{-12}, \kappa = 1 \times 10^{-20}, R_v = 10 \text{ } \mu\text{m}, L = 1 \text{ mm}, \theta = 20^\circ$$

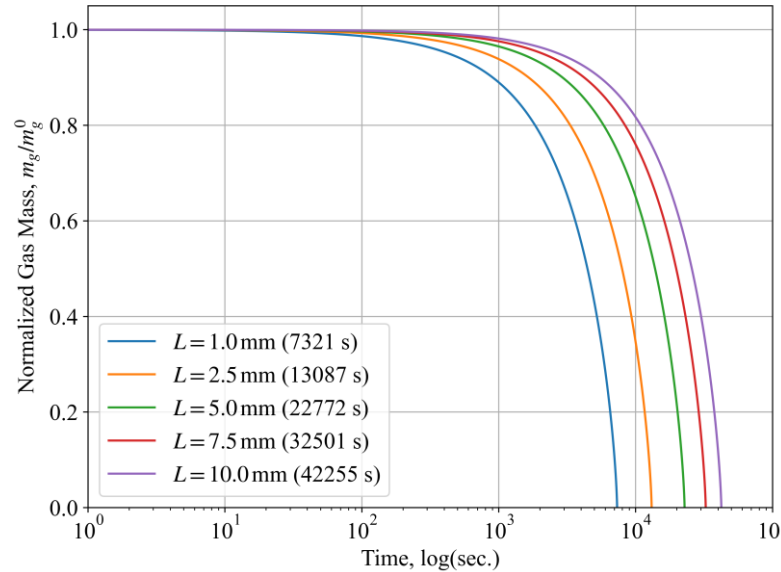
4. Parametric analysis of saturation kinetics

- Microstructure-related geometrical properties



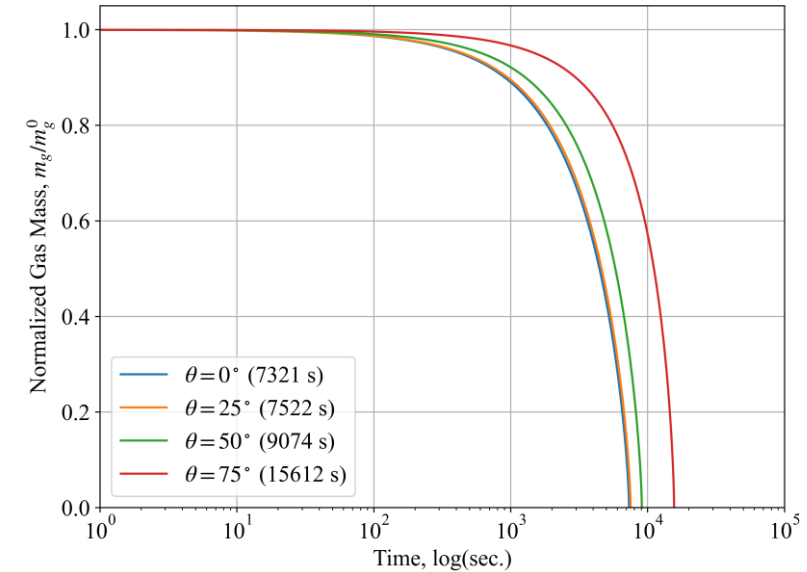
Spherical air void radius, R_V

$L = 1 \text{ mm}$, $\theta = 0^\circ$, $D_g^s = 1 \times 10^{-12}$, $\kappa = 1 \times 10^{-20}$, $\varphi_0 = 0.2$



Saturated cement paste shell thickness, L

$R_V = 10 \mu\text{m}$, $\theta = 0^\circ$, $D_g^s = 1 \times 10^{-12}$, $\kappa = 1 \times 10^{-20}$, $\varphi_0 = 0.2$

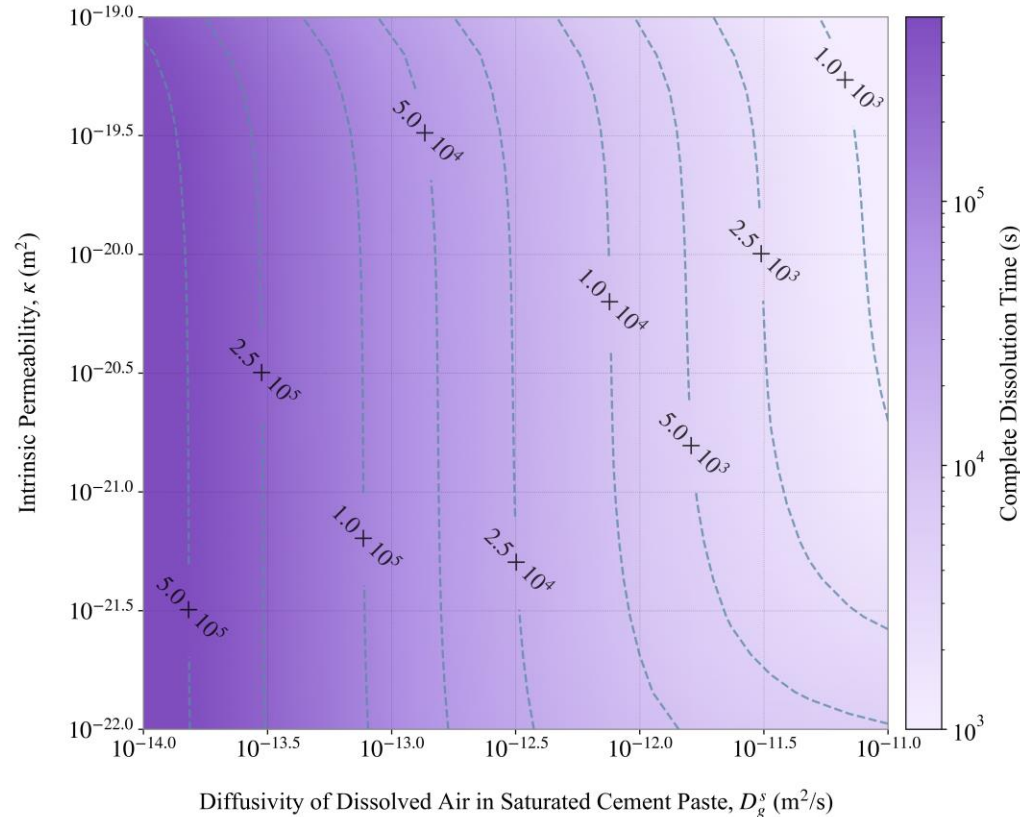


Air-liquid interface contact angle, θ

$R_V = 10 \mu\text{m}$, $L = 1 \text{ mm}$, $D_g^s = 1 \times 10^{-12}$, $\kappa = 1 \times 10^{-20}$, $\varphi_0 = 0.2$

5. Microstructure-informed optimization for freeze-thaw durability

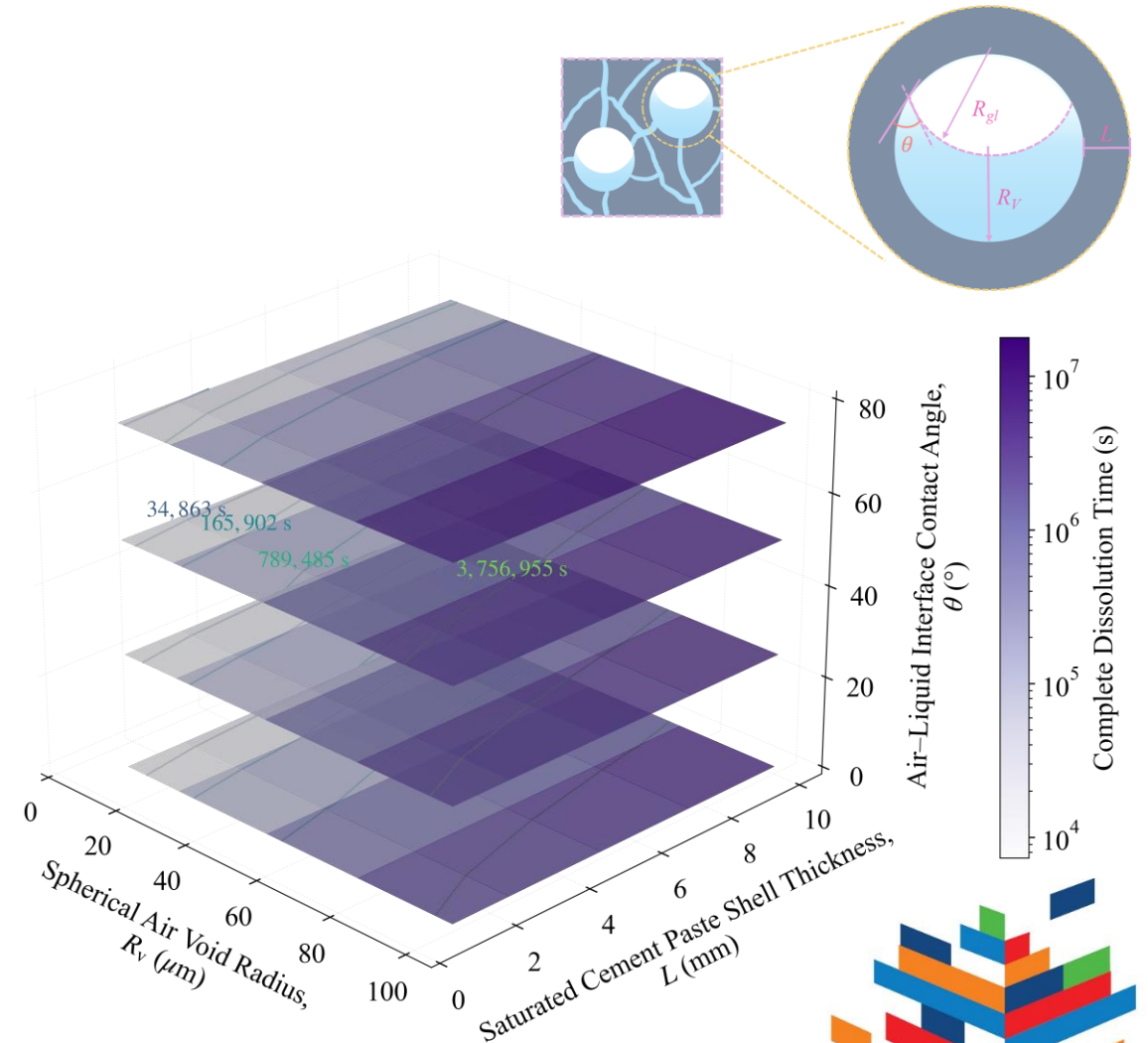
- Transport-related physical properties



- Refining diffusion pathways (e.g., increasing tortuosity, reducing D_g^s) is more effective than altering porosity.
- Combining low D_g^s and low κ yields better long-term air retention and freeze-thaw durability.
- System-specific insights:**
 - OPC requires stronger densification and air control.
 - CSA focuses on cracking and setting control.
 - LC³ should preserve its low-transport dense matrix.
 - Geopolymers need to reduce shrinkage and ensure compatibility with air-entraining agents.

5. Microstructure-informed optimization for freeze-thaw durability

- Microstructure-related geometrical properties
 - Create a controlled amount of stable, larger entrained voids (e.g., $R_v \sim 50\text{--}100\mu\text{m}$) mixed with abundant small voids to keep spacing factor.
 - Increase interfacial hydrophobicity to enlarge contact angle and initial gas volume to slow dissolution.
 - Increase the effective path from void to free surface, e.g., add SCMs to densify paste to raise tortuosity.



6. Summary

- **Comparison across different cementitious systems:**
 - From OPC to emerging systems, the transition from conventional to low-carbon, dense microstructures corresponds to progressively improved freeze-thaw durability.
- **Transport parameters dominate the kinetics of air void saturation:**
 - Diffusivity is the most critical factor, permeability plays a secondary role, and porosity shows limited impact in the typical range of cement paste.
- **Geometrical parameters provide additional ways for durability design:**
 - Air void radius provides the strongest geometrical control, shell thickness increases the diffusion path, and contact angle moderately affects dissolution.

6. Summary

- **Design implications for freeze-thaw durability.**
 - Optimizing void systems through a bi-modal or multi-modal distribution (many small voids for spacing, stable larger ones for air retention).
 - Refining transport pathways by reducing diffusivity and permeability via low w/b, SCMs, densified ITZ, and improved curing.
 - Modifying interfacial chemistry to increase contact angle and delay void dissolution.
 - **System-specific insights:** OPC needs densification and air stability; CSA should control cracking and setting; LC³ should maintain its dense, low-transport microstructure; and geopolymers should limit shrinkage and ensure AEA compatibility.



Thank you! & Questions?



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