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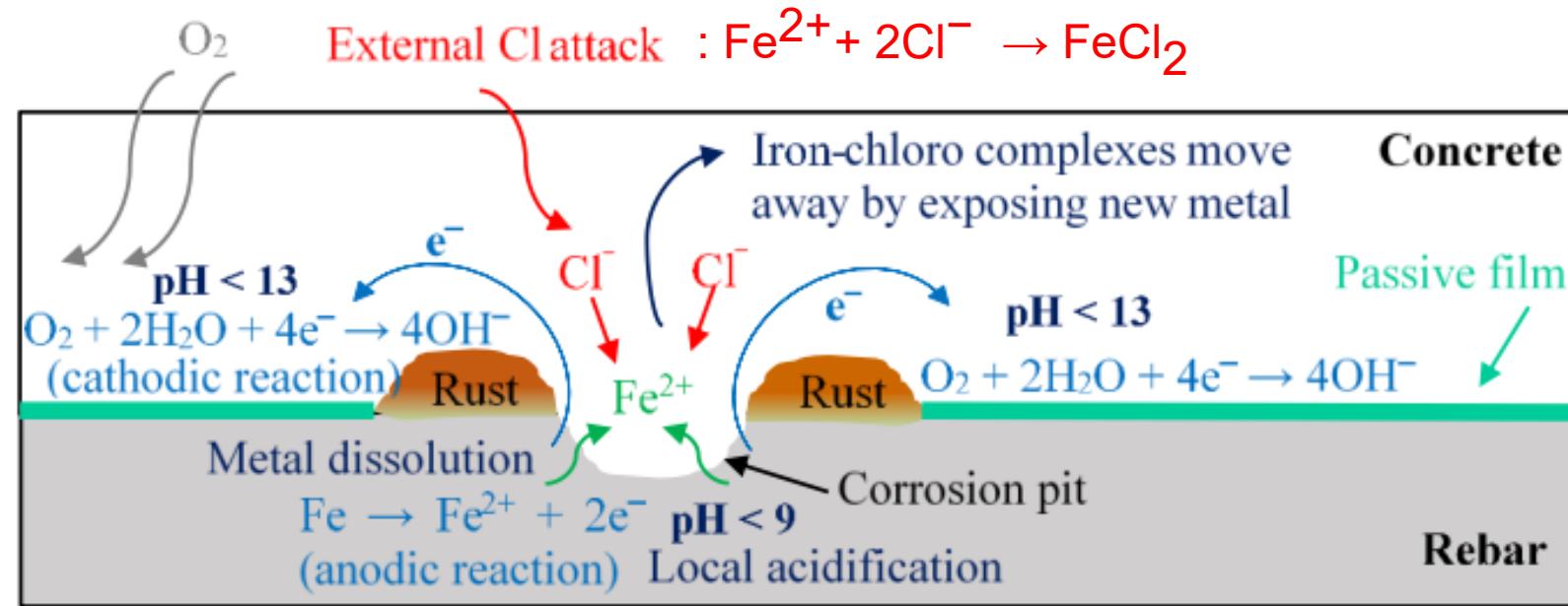
Rational Methods for Evaluating Chloride Penetrability and Corrosion Performance of BCSA Cement Composites

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Chloride-induced corrosion of embedded steel



Materials and mixture proportions

Oxide	BCSA	PC
CaO	51	63
SiO ₂	14	19
Al ₂ O ₃	14	4.6
Fe ₂ O ₃	0.87	3.3
MgO	0.76	2.0
SO ₃	17	4.4
Alkalies	0.61	0.89
LOI	1.6	2.5

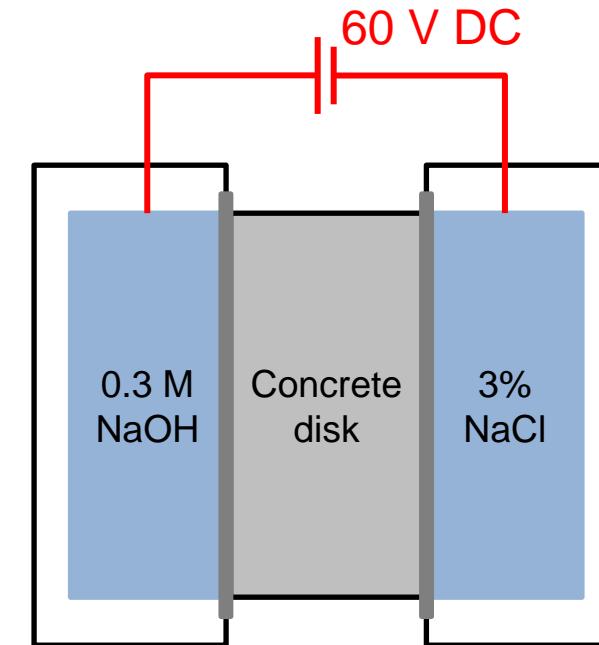
Cement type	w/cm	Cement kg/m ³	Water kg/m ³	Sand kg/m ³	#67 stone kg/m ³	Citric acid % cm
BCSA	0.36	360	130	900	1100	1.00
	0.40	340	136			
	0.45	320	144			
	0.55	280	154			

Rough composition of BCSA
 Belite 44%
 Ye'elite 27%
 Calcium sulfate 24%

Rapid chloride penetrability test – ASTM C1202

Cement	w/cm	Charge passed (C)	Penetrability
PC	0.36	337	Very low
BCSA	0.40	175	Very low
	0.45	268	Very low
	0.55	262	Very low

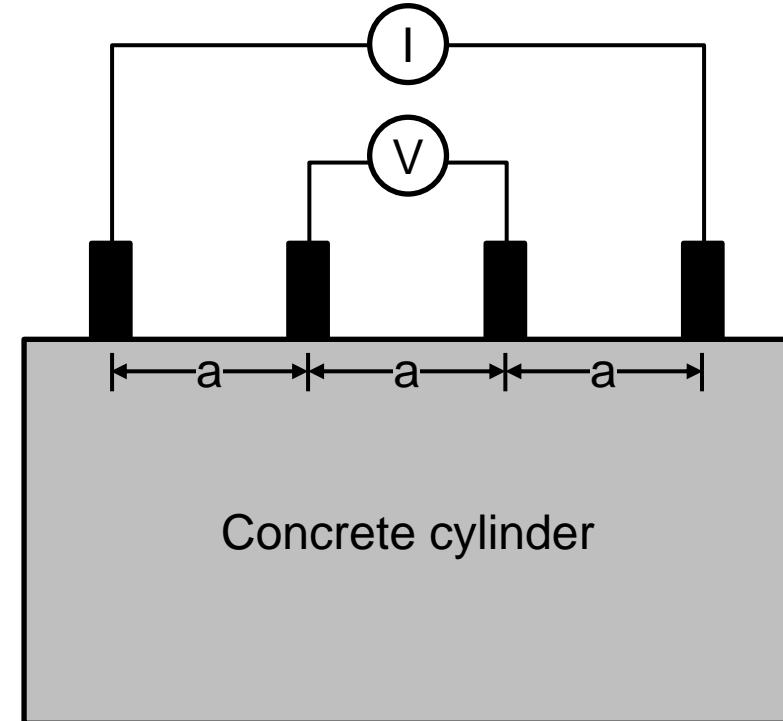
Charge passed (C)	Penetrability
>4,000	High
2,000–4,000	Moderate
1,000–2,000	Low
100–1,000	Very Low
<100	Negligible



Surface resistivity test – AASHTO T 358

Cement	w/cm	Resistivity (kΩ-cm)	Penetrability
PC	0.36	10	High
BCSA	0.40	73	Very low
	0.45	48	Very low
	0.55	34	Low

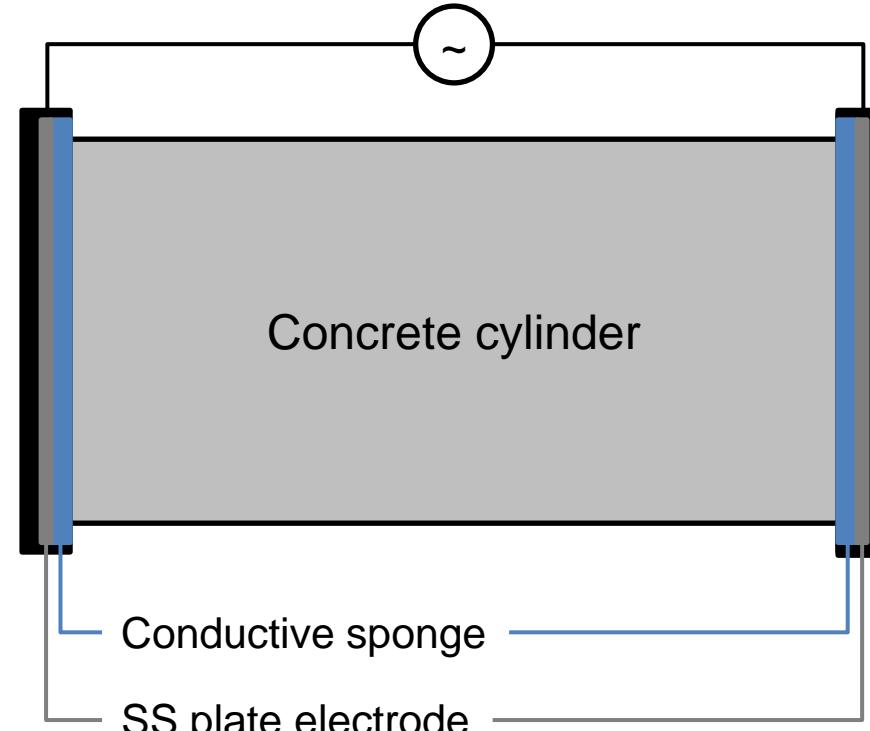
Resistivity (kΩ-cm)	Penetrability
<12	High
12-21	Moderate
21-37	Low
37-254	Very Low
>254	Negligible



Bulk resistivity test – ASTM C1876

Cement	w/cm	Resistivity (kΩ-cm)	Penetrability
PC	0.36	3.84	High
BCSA	0.40	6.77	Moderate
	0.45	6.77	Moderate
	0.55	4.63	High

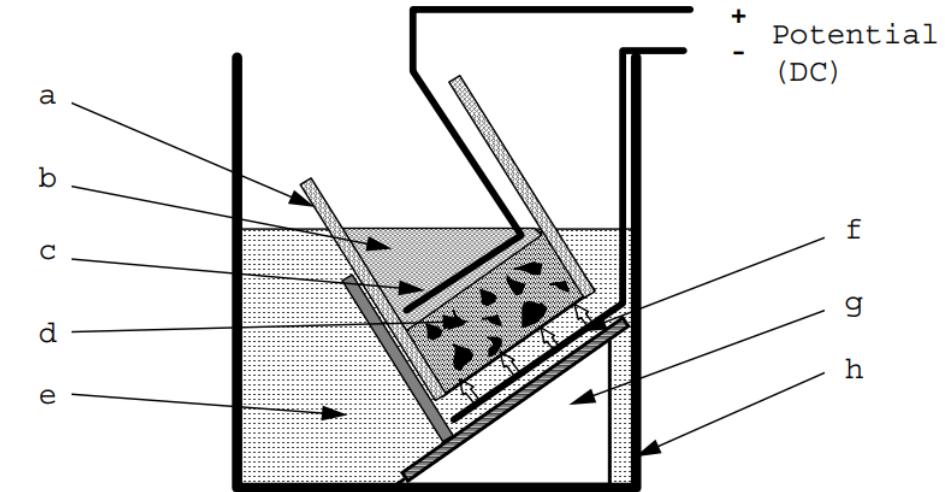
Resistivity (kΩ-cm)	Penetrability
<5	High
5-10	Moderate
10-20	Low
20-200	Very Low
>200	Negligible



Non-steady-state migration test – NT 492

Cement	w/cm	Migration coefficient (m^2/s)	Penetrability
PC	0.36	10.78×10^{-12}	Moderate
BCSA	0.40	2.07×10^{-12}	Low
	0.45	10.39×10^{-12}	Moderate
	0.55	17.59×10^{-12}	High

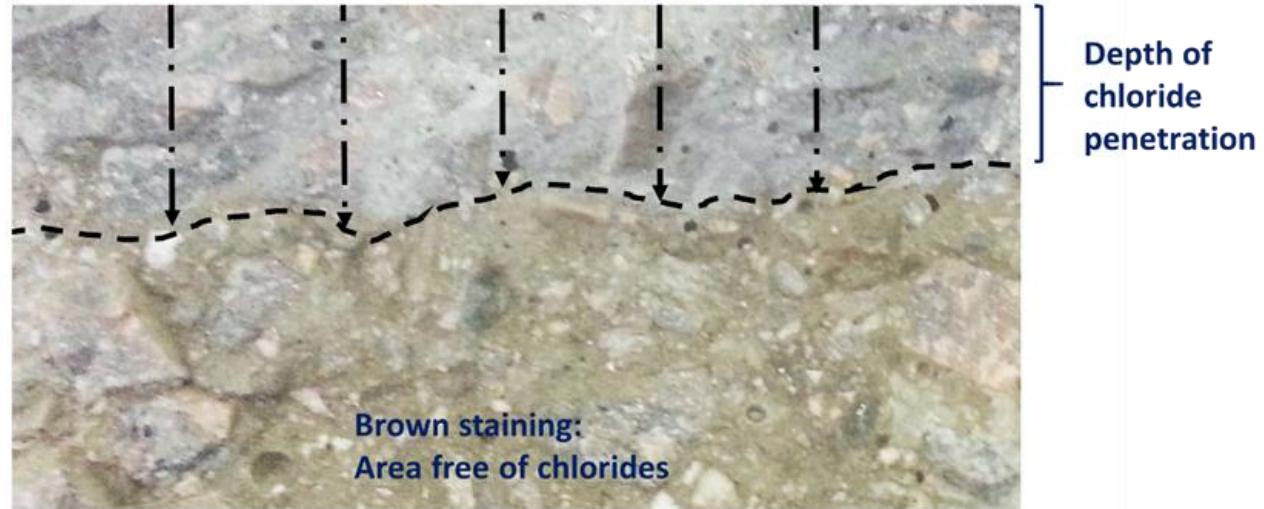
Migration coefficient ($10^{-12} m^2/s$)	Penetrability
> 16	High
8-16	Moderate
2-8	Low
< 2	Very Low



- a. Rubber sleeve
- b. Anolyte
- c. Anode
- d. Specimen
- e. Catholyte
- f. Cathode
- g. Plastic support
- h. Plastic box

Non-steady-state migration test – NT 492

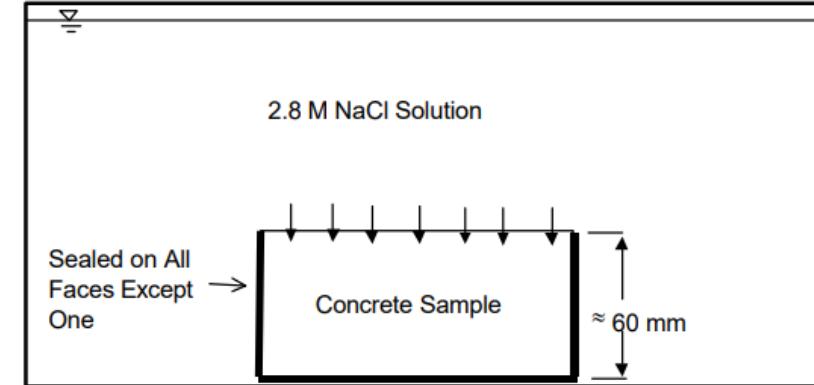
- $D_{NSSM} = \frac{RT}{zFE} \cdot \frac{x_d - \alpha\sqrt{x_d}}{t}$
- $E = 2\sqrt{\frac{U-2}{L}}$
- $\alpha = 2\sqrt{\frac{RT}{zFE}} \cdot \text{erf}^{-1}\left(1 - \frac{2c_d}{c_0}\right)$



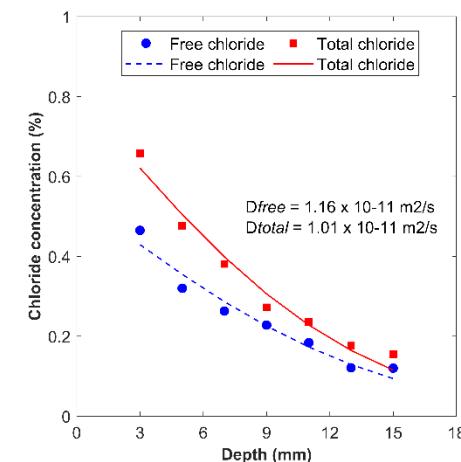
- c_d = chloride concentration threshold for AgNO_3 color change
- $c_d = 0.07 \text{ N}$ for PC concrete
- c_d is unknown for BCSA concrete

Bulk diffusion test (ASTM C1556)

Cement	w/cm	Migration coefficient (m^2/s)	Penetrability
PC	0.36	5.80×10^{-12}	Low
BCSA	0.40	28.3×10^{-12}	High
	0.45	23.9×10^{-12}	High
	0.55	15.9×10^{-12}	High



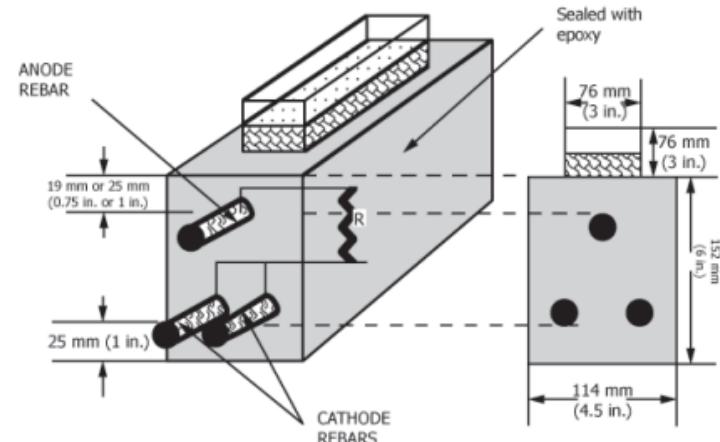
Diffusion coefficient ($10^{-12} m^2/s$)	Penetrability
> 15	High
10-15	Moderate
5-10	Low
2-5	Very Low
< 2	Negligible



Comparison of penetrability classifications

Cement	w/cm	RCPT	Surface resistivity	Bulk resistivity	NSSM	Bulk diffusion
PC	0.36	Very low 337 C	High 10 kΩ-cm	High 4 kΩ-cm	Moderate $D = 11 \times 10^{-12} \text{ m}^2/\text{s}$	Low $D = 6 \times 10^{-12} \text{ m}^2/\text{s}$
BCSA	0.40	Very low 175 C	Very low 73 kΩ-cm	Moderate 7 kΩ-cm	Low $D = 2 \times 10^{-12} \text{ m}^2/\text{s}$	High $D = 28 \times 10^{-12} \text{ m}^2/\text{s}$
	0.45	Very low 268 C	Very low 48 kΩ-cm	Moderate 7 kΩ-cm	Moderate $D = 10 \times 10^{-12} \text{ m}^2/\text{s}$	High $D = 24 \times 10^{-12} \text{ m}^2/\text{s}$
	0.55	Very low 262 C	Low 34 kΩ-cm	High 5 kΩ-cm	High $D = 18 \times 10^{-12} \text{ m}^2/\text{s}$	High $D = 16 \times 10^{-12} \text{ m}^2/\text{s}$

Corrosion performance – ASTM G109

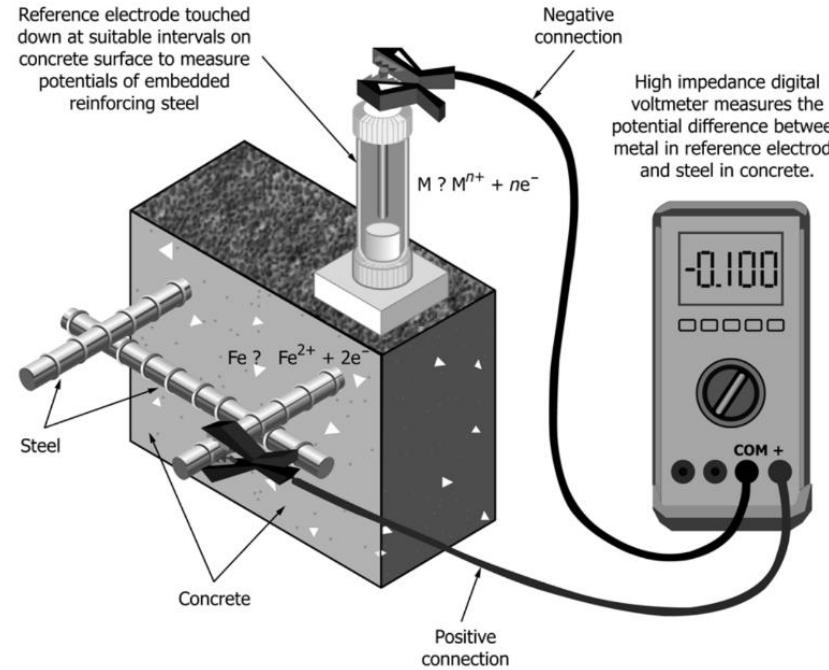


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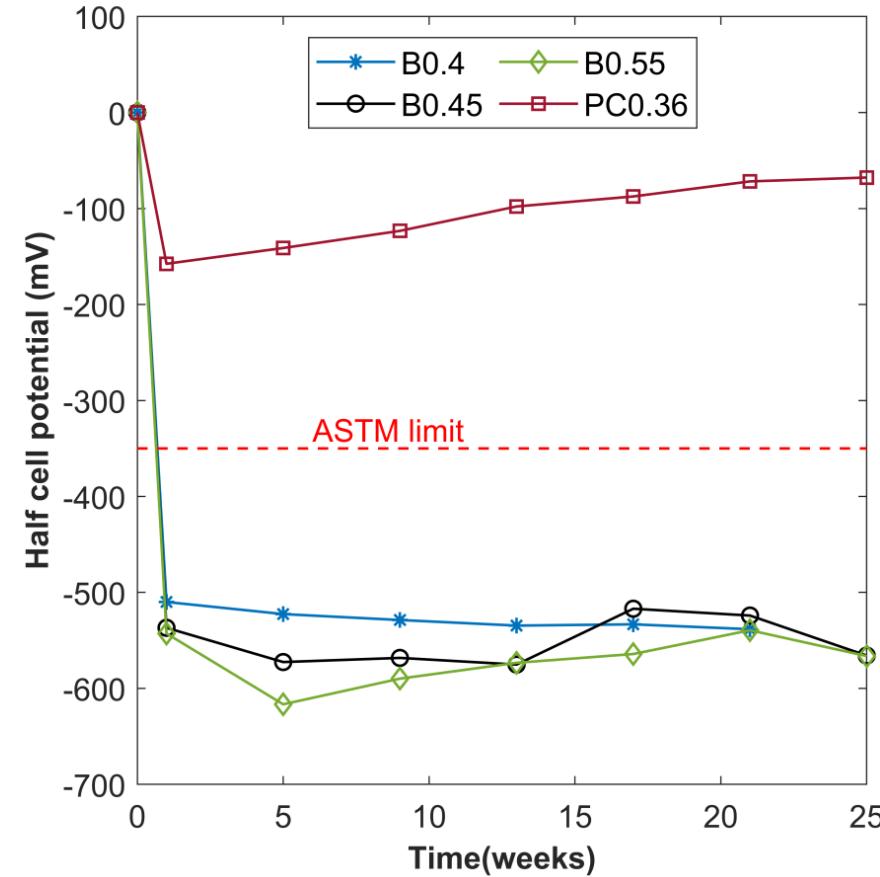
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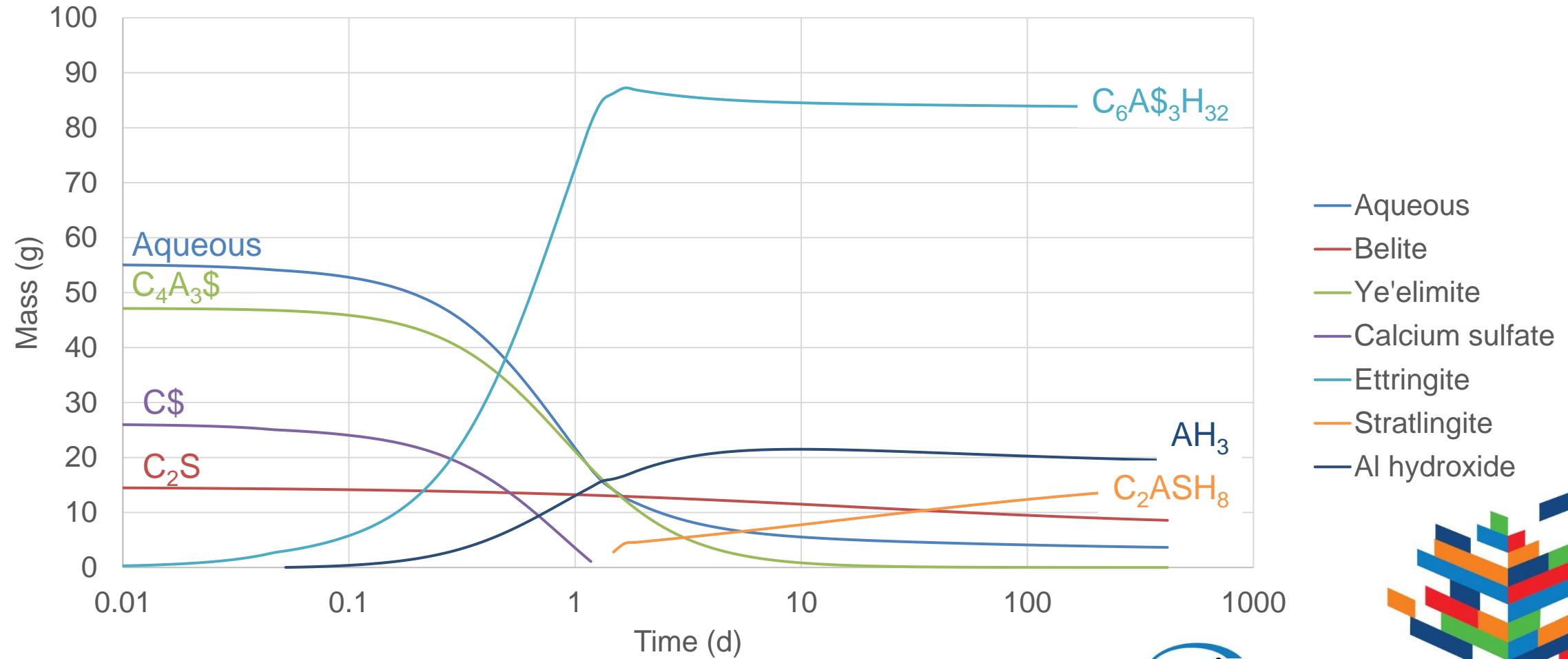
Corrosion performance – ASTM C876



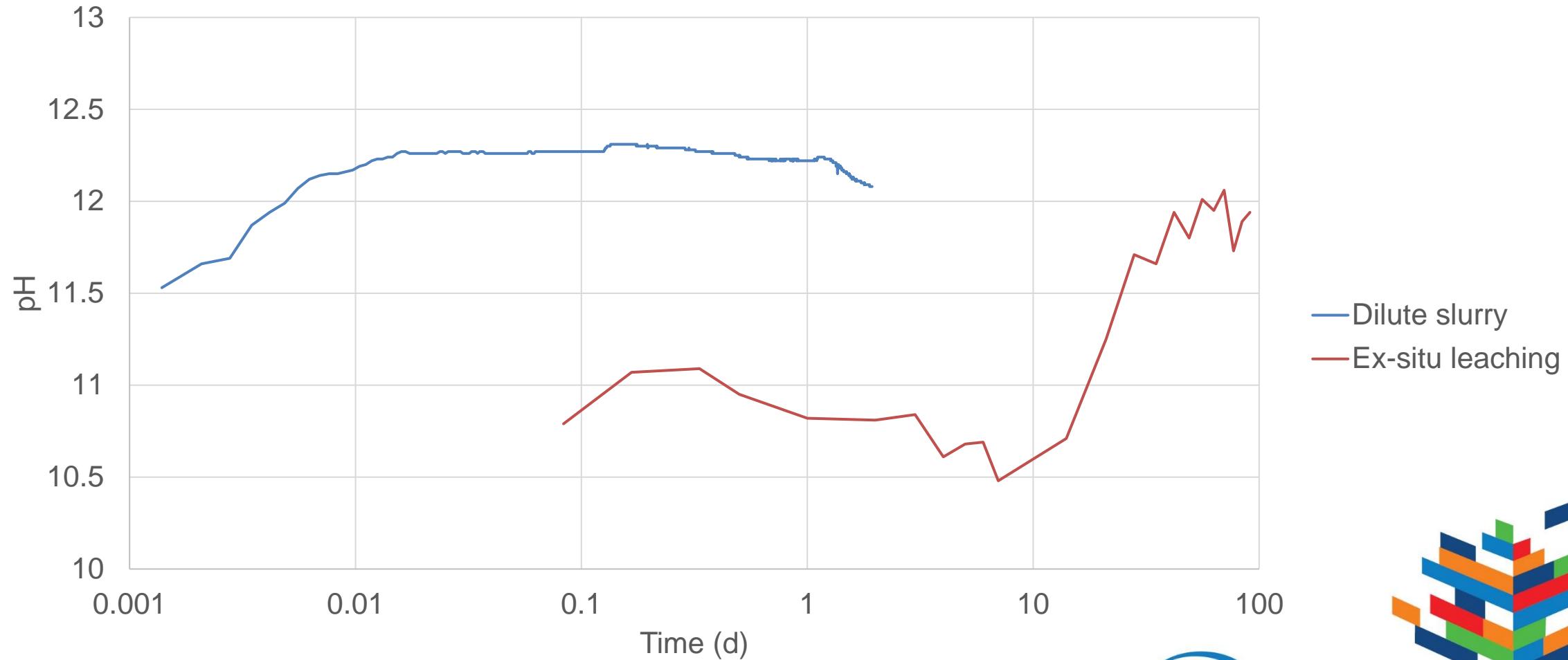
Half cell potential	Corrosion condition
> -200 mV	Unlikely
-200 to -350 mV	Uncertain
< -350 mV	Likely



Hydration modeling - CEMGEMS



Pore solution alkalinity





Remaining questions

1. Does later-age hydration of belite and associated elevation in pH translate to better corrosion resistance under ASTM G109?
2. Do chloride penetrability test results correlate well with later-age corrosion performance?
3. What about formation factor, direct pore solution expression, etc?



Thank you!

Contact information

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