Characterization of calcium sulfoaluminate cements exposed to accelerated weathering carbonation conditions

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Introduction



Research background

- Need for new cementitious binder systems^[1,2]
 - \blacktriangleright Reduction of net CO₂ emissions is inevitable in cement industry
 - Demand for cement continues to grow, and Portland cement (PC) is the most commonly used construction material in the world
 - Cement industry is responsible for about 5 8% of worldwide man-made CO₂ emissions

Classification of alternative cementitious binder systems^[2,3]

- PC blended with supplementary cementitious materials
- Alkali-activated cements such as alkali-activated slag, geopolymer and etc.
- Calcium aluminate cement (CAC)
- Calcium sulfoaluminate (CSA) cement and belite-ye'elimite-ferrite (BYF) cement
- Magnesium (or calcium) phosphate cement (MPC) including magnesium (potassium) phosphate binders

Properties of CSA cements

- Typical properties of CSA cements^[4]
 - Fast bond
 - Rapid strength development
 - Shrinkage compensation (expansive cement)
 - Short curing phase
 - Low alkali contents
 - \blacktriangleright Low CO₂ emissions



Weathering carbonation

- Weathering carbonation of cementitious materials (passive, ageing)
 - Weathering carbonation is an inevitable deterioration phenomenon to cementitious materials, slowly affecting the durability of the cementitious materials^[5].
 - The dissolved CO₂ in the pore solution of the cementitious materials reacts either with portlandite or with C-S-H, leading to the reduction of pH level and to the corrosion of embedded rebars^[6].



Richardson, M. G. (1988). "Carbonation of reinforced concrete: its causes and management". C https://civildigital.com/carbonation-concrete-various-failure-mechanisms-concrete/

Possan, E., Thomaz, W.A., Aleandri, G.A., Felix, E.F. and dos Santos, A.C., 2017. CO2 uptake potential due to concrete carbonation: A case study. Case Studies in Construction Materials, 6, pp.147.

Factors affecting carbonation behavior of CSA cements



Zhang et al.^[9] : Water-to-cement ratio

- Zhang et al. (2009)^[9] investigated the carbonation behavior of CSA cement with different w/c ratio ranging 0.33 - 0.49.
- Lower water content decreased the carbonation depth, which signifies the higher carbonation resistance.
- Ettringite, formed under the sufficient w/c ratio conditions, was confirmed to be vulnerable against carbonation.



Hargis et al.^[10] : *m*-values

- Hargis et al. (2017)^[10] investigated the carbonation resistance of the CSA cements with different *m*-values (1.0, 1.4, or 1.8).
- An increase in the *m*-value accelerated the reaction of ye'elimite and densified the microstructure, resulting in an increase in the carbonation resistance.
- Hydration products such as monocarbonate and ettringite were found to be first phases being converted into calcium carbonate upon the carbonation.



Park^[11] : Replacement with SCM

- Park (2020)^[11] theoretically investigated the carbonation resistance of CSA cements blended with supplementary cementitious material (SCM).
- Replacement with SCM lowered the carbonation resistance, leading to the decrease in pH and to the volumetric instability of the matrix.
- Monosulfate acted as an initial carbonation buffer and was transformed into monocarbonate, which became calcium carbonate upon exposure to the high CO₂ concentration.



CSA cements exposed to an accelerated carbonation condition: Role of MgO^[12]



Research objective and methodology^[12]

Objective

To provide the detailed information of the carbonation of CSA cements and role played by MgO upon carbonation

Methodology

[Table] Chemical composition of CSA clinker used in this study (wt.%)



X-ray diffractometry^[12]

- MgO incorporation preferred the formation of monosulfate over ettringite.
- Ettringite and monosulfate still existed after carbonation in the samples with MgO.
- A reduction in calcite peak intensity signified a decrease in the degree of carbonation.



Thermogravimetry^[12]

- MgO incorporation preferred the formation of monosulfate over ettringite and aluminum hydroxide.
- The formation of hydrotalcite became clear in the samples with MgO.
- The amount of calcium carbonates reduced by MgO incorporation (M0 : 13.21%, M20 : 9.54%).



²⁷AI MAS NMR^[12]

- MgO reduced the degree of Al incorporation in C-S-H.
- Upon carbonation, AFm/LDH strongly persisted in the sample with MgO.
- Degree of Al incorporation in C-(A)-S-H of the sample without MgO i ncreased upon carbonation.
- With MgO, tetrahedral Al region was not altered.



SEM/EDS^[12]

- The samples without MgO mainly showed gypsum and aluminum hydroxide after carbonation.
- The samples with MgO mainly consist of AFm phases with C-(A)-S-H after carbonation.
- MgO triggered the formation of hydrotalcite and Mg-rich reaction products with high Si ratios.



Carbonation depth^[12]

- Carbonation depth decreased as the MgO content increased
- Hydrotalcite, which was formed by MgO incorporation, captured CO₂, leading to an enhancement in the carbonation resistance.



[Fig] Carbonation degree of the carbonated MgO-modified CSA cement paste samples

Concluding remarks



Concluding remarks

- Weathering carbonation is an inevitable deterioration phenomenon of cementitious materials which should be taken into account when adopting a new binder system.
- A lower w/c ratio and higher *m*-value of CSA cement can enhance carbonation resistance, while the replacement with supplementary cementitious material can degrade the carbonation resistance of CSA cement.
- Carbonation of CSA cement induced the full carbonation of ettringite and monosulfate.
- Incorporation of MgO in CSA cement led to the formation of AFm phase including hydrotalcite over ettringite and aluminum hydroxide, thereby mitigating the ingress of CO₃²⁻ ions
- The presence of hydrotalcite in the MgO-modified CSA cement can improve the carbonation resistance.



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