

# Performance of Cracked High-Performance Concrete in a Harsh Marine Environment

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ACI Convention – Salt Lake City

## **1. Mechanical Properties**

## **2. Durability issues to be considered:**

- Alkali-aggregate reaction (AAR)
- Freeze-thaw action
- Salt scaling
- Sulphate attack
- Abrasion
- Delayed ettringite formation
- Chemical attack
- Corrosion of steel

## **3. Minimize Cracking**

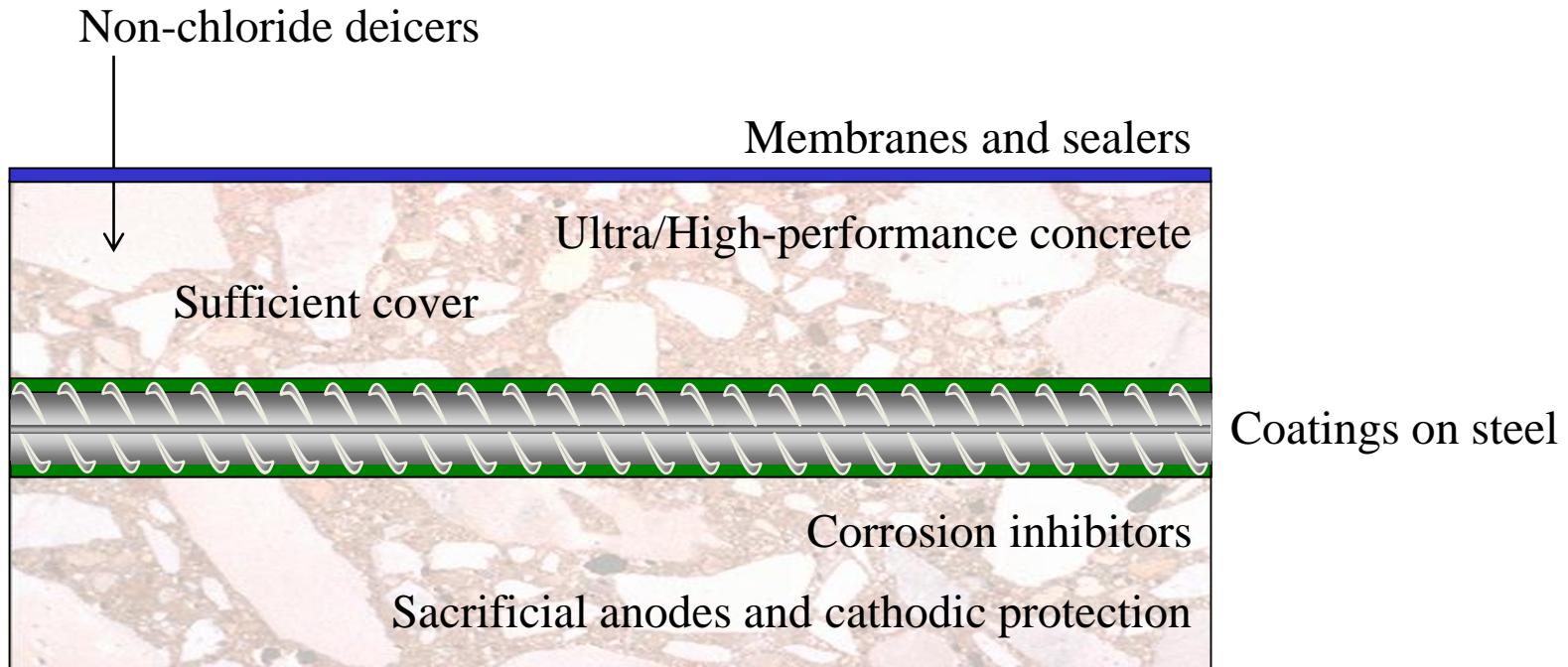
- Thermal cracking
- Shrinkage cracking (autogenous, drying and shrinkage)

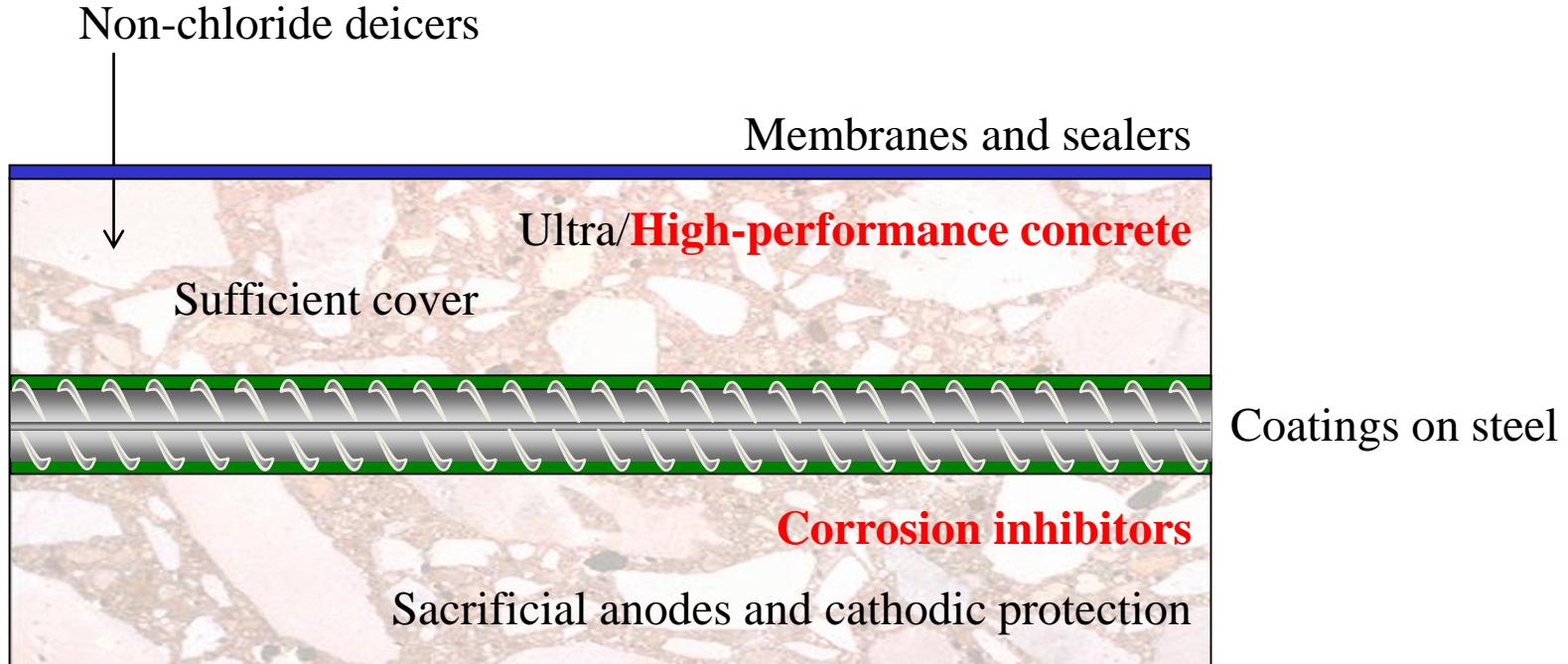


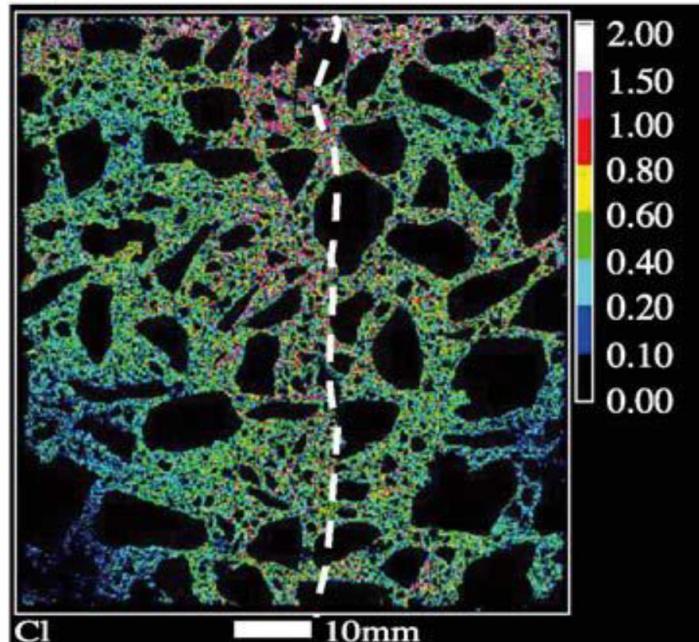
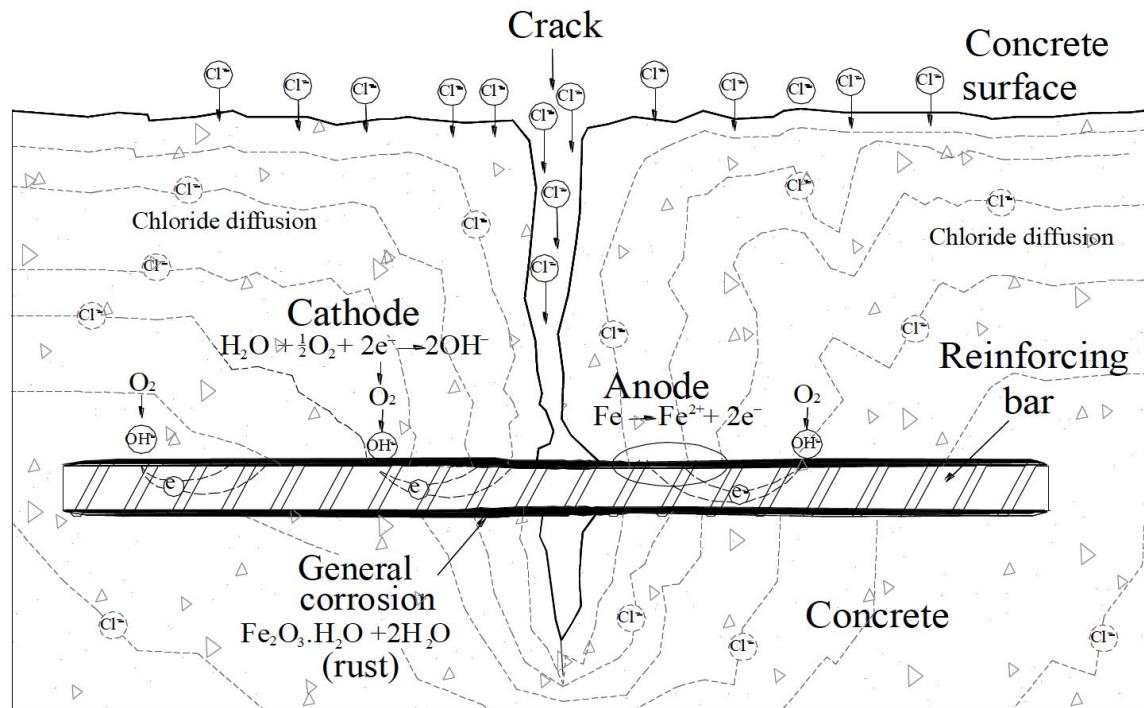


Seawater

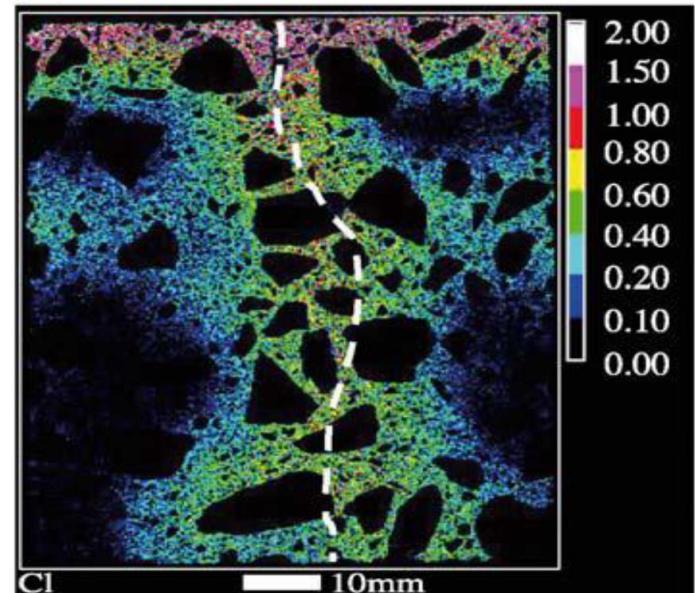
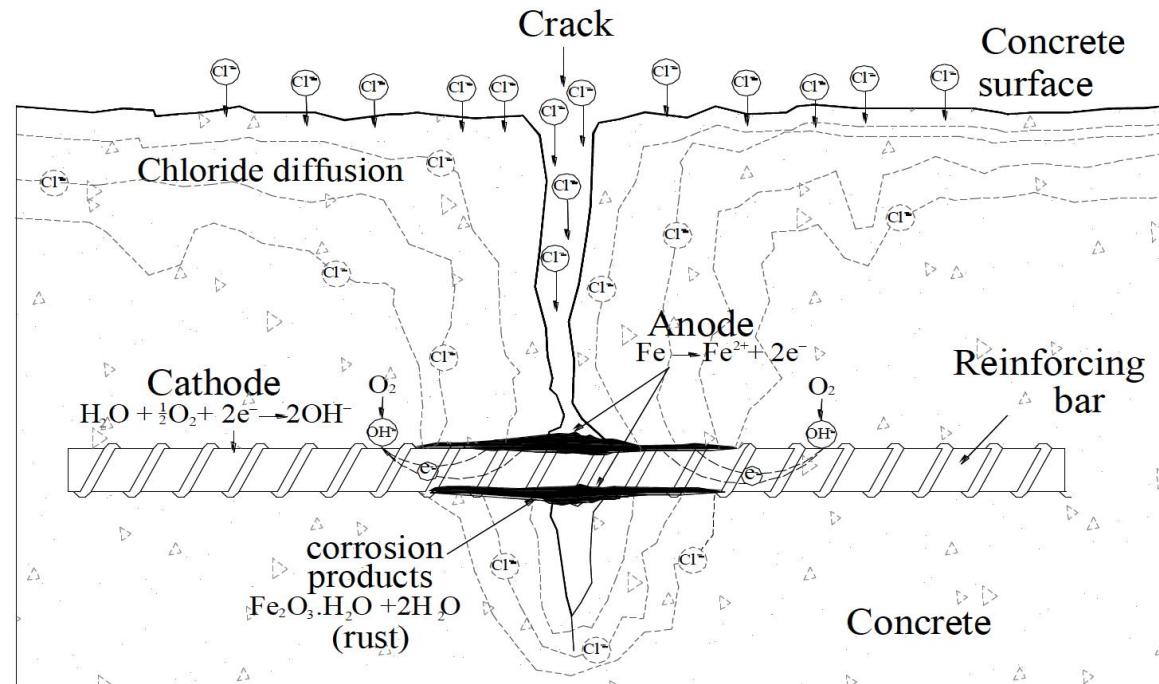
Road salts



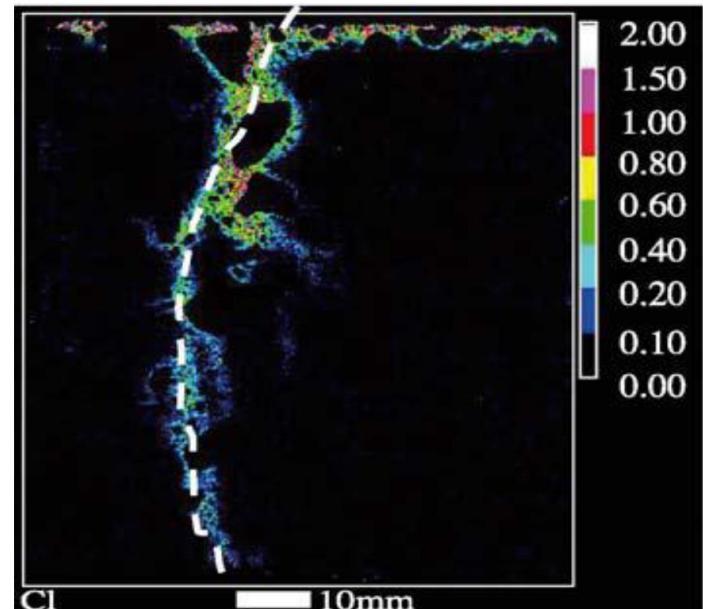
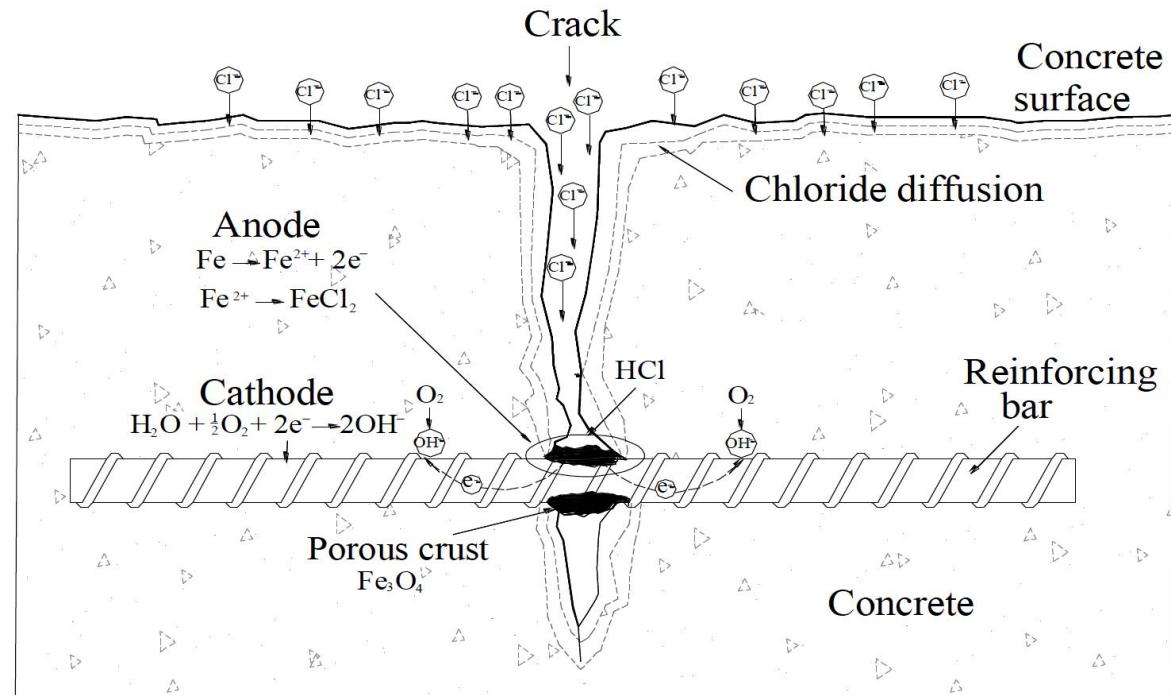




(Win, 2004)



(Win, 2004)



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***High Performance Concrete*** – concrete meeting special combinations of performance and uniformity requirements that cannot always be achieved routinely using conventional constituents and normal mixing, placing, and curing practices.

**ACI Concrete Terminology**

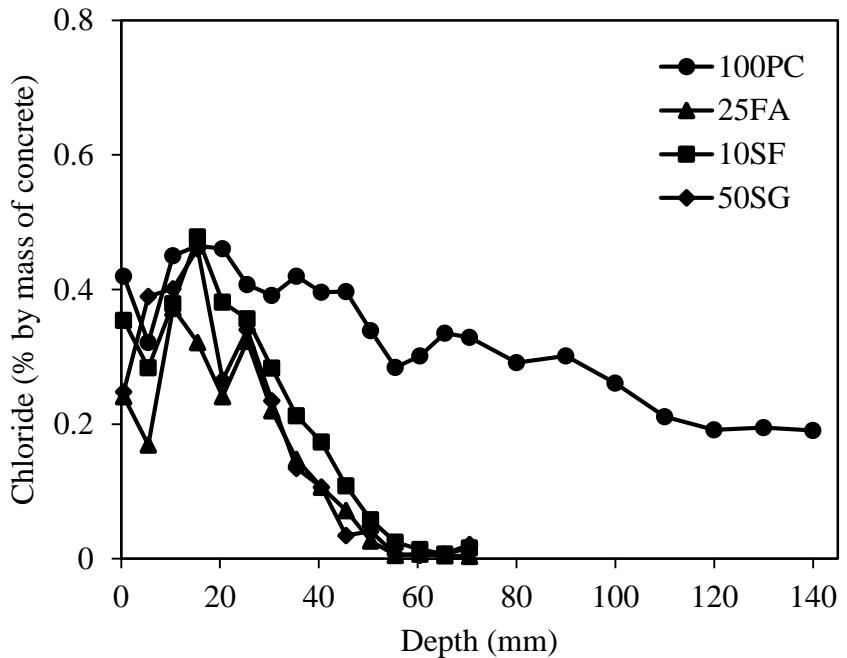
### **Supplementary Cementing Materials (SCMs):**

- Fly Ash
- Silica Fume

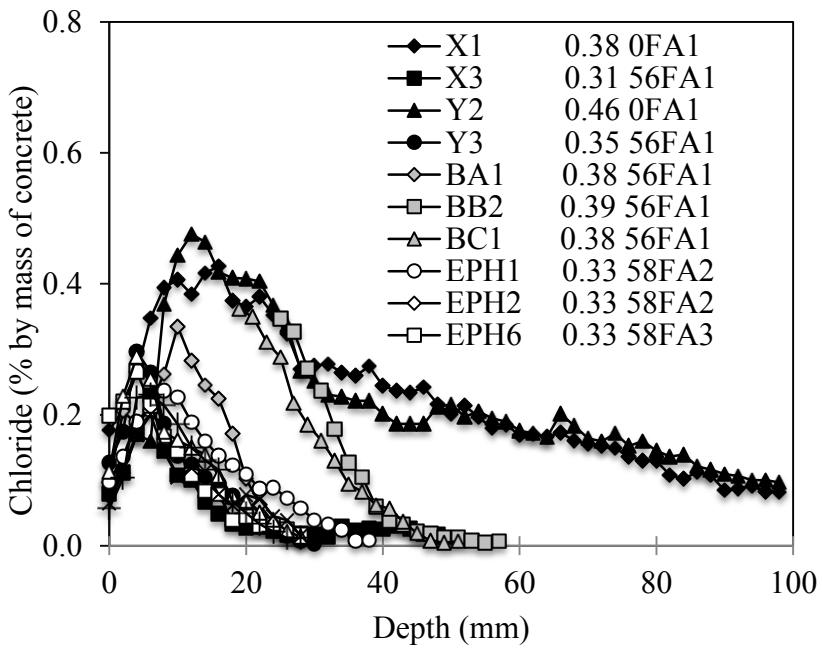
### **Corrosion Inhibitors:**

- Calcium Nitrite inhibitor (CNI)
- Disodium Tetrapropenyl succinate (DTS)

# Performance of SCM Concrete – Treat Island (25 to 27 Years)



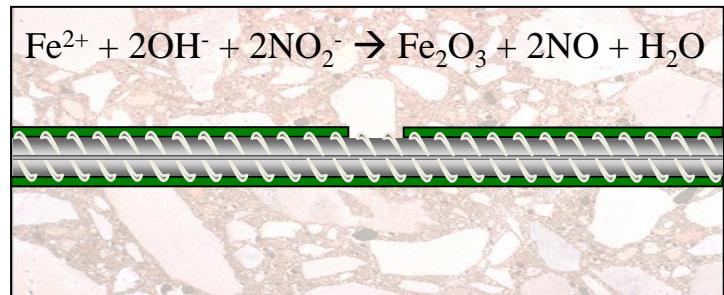
Fahim, A., Moffatt, E.G. and Thomas, M.D.A. (2017). Corrosion Resistance of Concrete Incorporating Supplementary Cementing Materials in a Marine Environment. International Concrete, SP-320-18, pp. 18.1-18.14.



Moffatt, E.G., Thomas, M.D.A., and Fahim, A. (2017). Performance of High-Volume Fly Ash Concrete in Marine Environment. Cement and Concrete Research. 102, pp. 127-135.

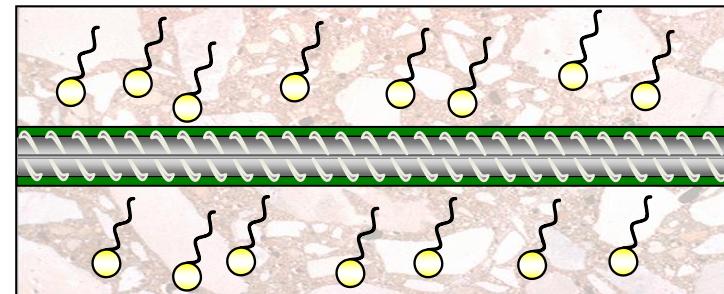
## **Calcium Nitrite Inhibitor (CNI)**

- inorganic corrosion inhibitor
- helps stabilize the passive layer on the steel
- competes with chloride ions for ferrous ions
- acts as an accelerator



## **Disodium Tetrapropenyl Succinate (DTS)**

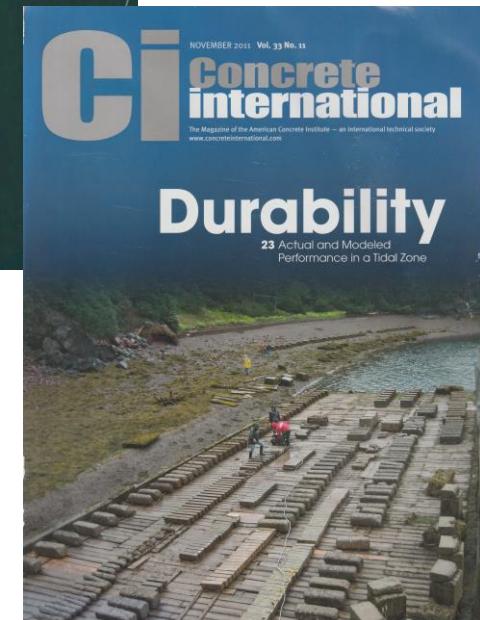
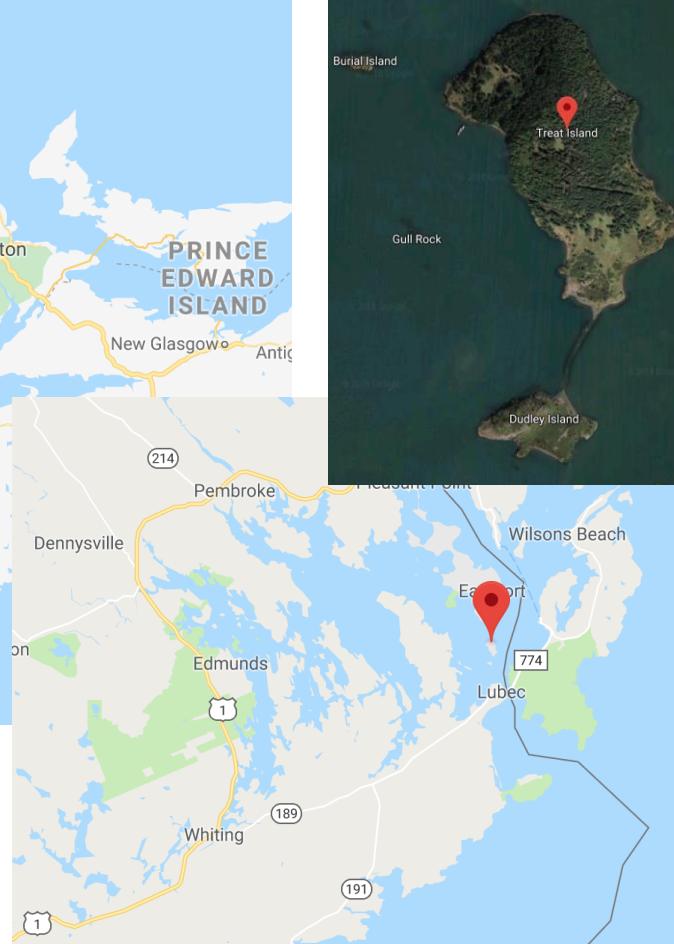
- organic corrosion inhibitor
- salt of alkenyl-substituted succinic acid (ASSA)
- contains an air-entraining admixture



# Treat Island, Maine, U.S.A.







# Treat Island, Maine, U.S.A.



**Portland Cement:** ASTM Type I with 8% silica fume replacement

**Fly Ash:** ASTM Type F ( $\text{CaO} = 2.96\%$ )

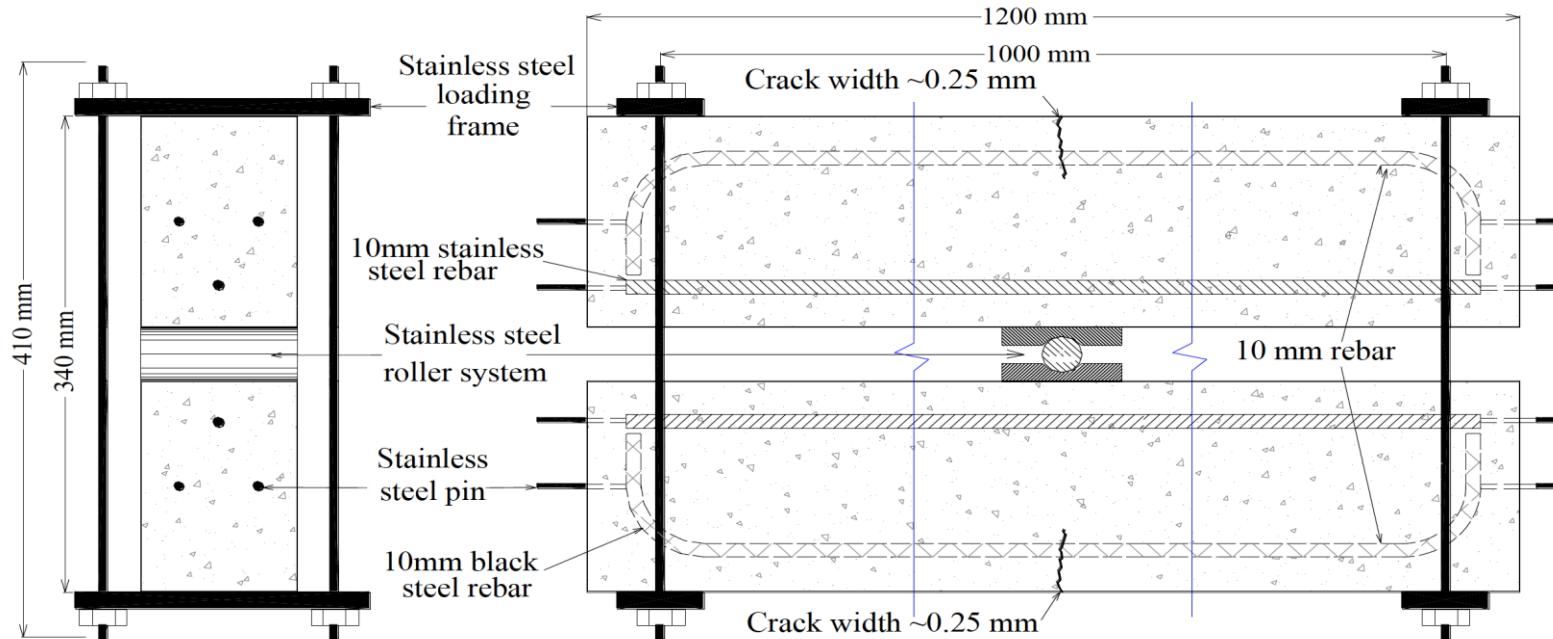
**W/CM** = 0.37

**Cementitious content** = 470 kg/m<sup>3</sup> (790 lb/yd<sup>3</sup>)

**Air** = 6-8%

**Slump** = 140-180 mm (5.5-7.0 in.)

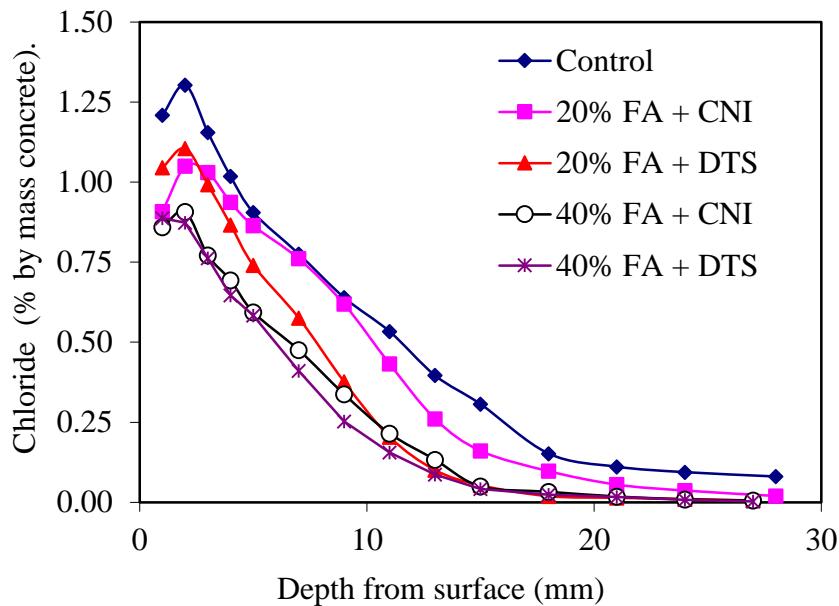
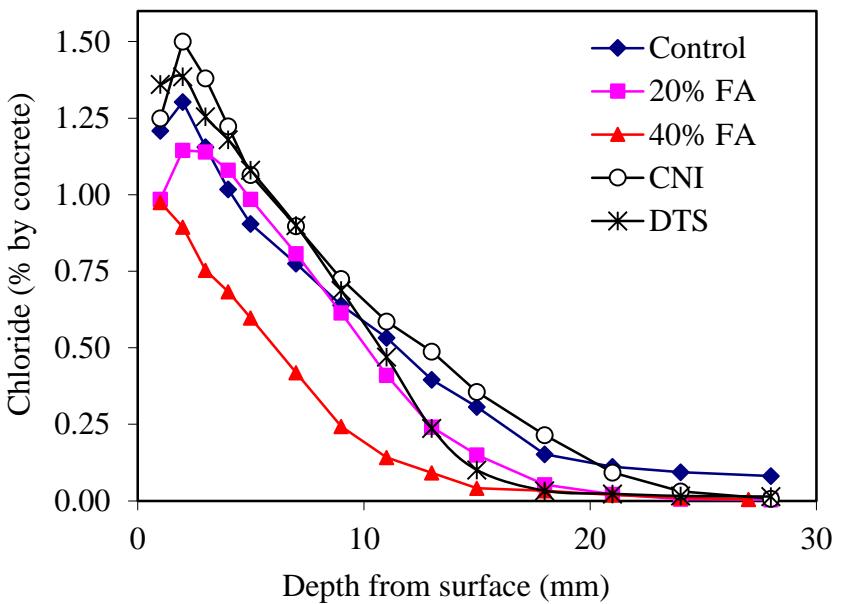
	<b>Mix</b>	<b>Mixture Properties</b>
Double combinations	1	100% PC
	2	20% FA
	3	40% FA
	4	12.5 L/m <sup>3</sup> CNI
Triple combinations	5	5 L/m <sup>3</sup> DTS
	6	20% FA + 12.5 L/m <sup>3</sup> CNI
	7	20% FA + 5 L/m <sup>3</sup> DTS
	8	40% FA + 12.5 L/m <sup>3</sup> CNI
	9	40% FA + 5 L/m <sup>3</sup> DTS



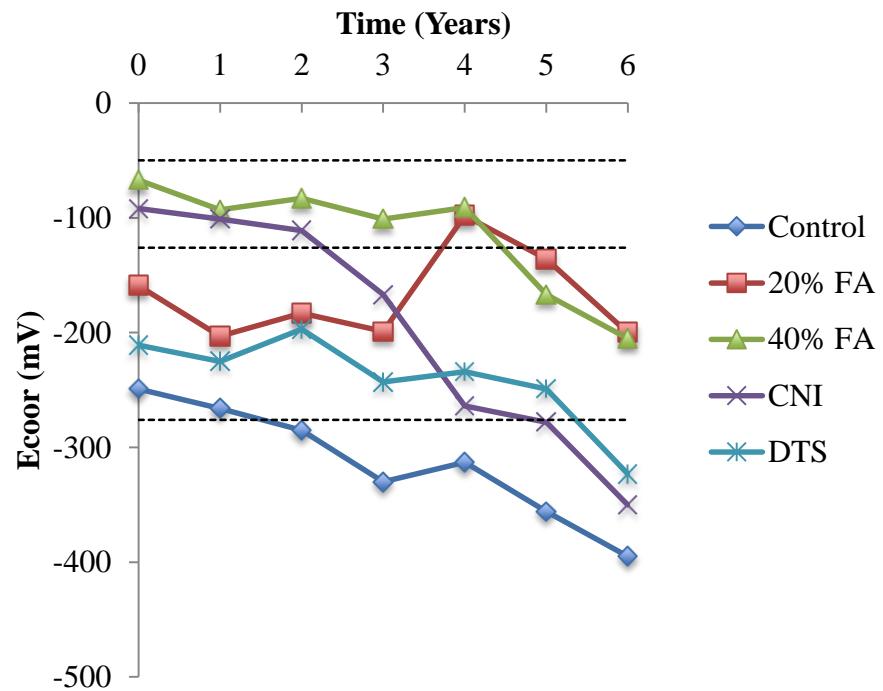




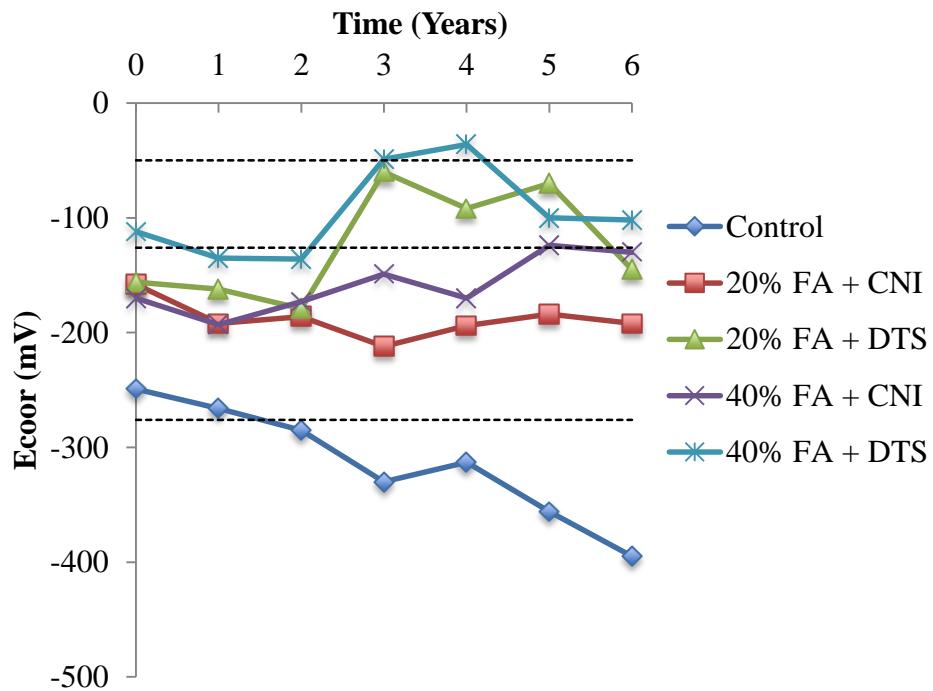
<b>Mix</b>	<b>Mixture Properties</b>	<b>Compressive Strength (MPa)</b>	<b>Diff. Coefficient (<math>\times 10^{-12}</math> m<math>^2</math>/s)</b>
1	100% PC	49.8	1.90
2	20% FA	56.8	1.40
3	40% FA	50.4	0.85
4	12.5 L/m $^3$ CNI	62.2	1.80
5	5 L/m $^3$ DTS	45.9	1.30
6	20% FA + 12.5 L/m $^3$ CNI	47.2	1.40
7	20% FA + 5 L/m $^3$ DTS	39.3	0.83
8	40% FA + 12.5 L/m $^3$ CNI	45.1	0.85
9	40% FA + 5 L/m $^3$ DTS	36.4	0.77



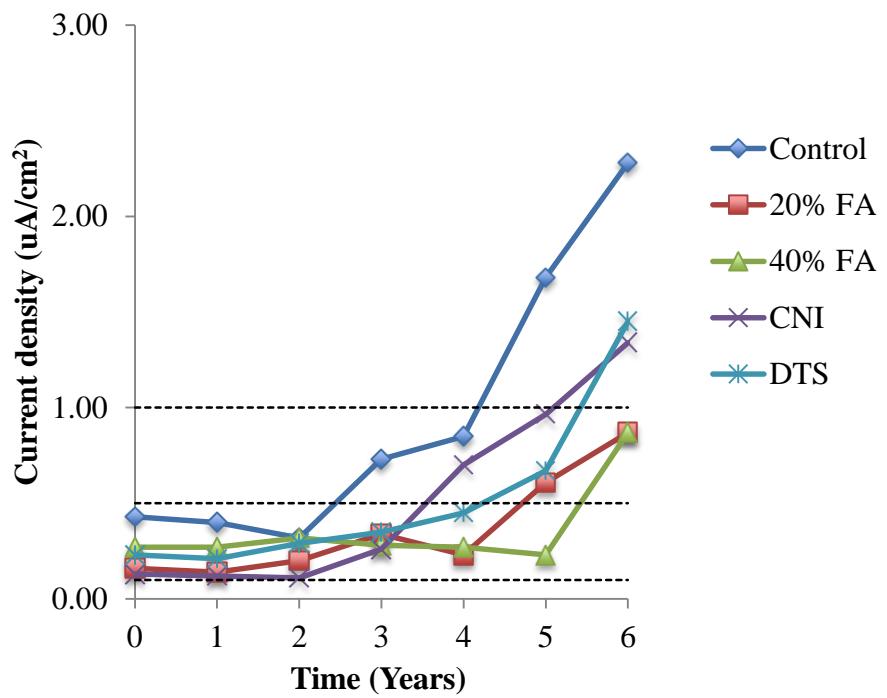
## *Double combinations*



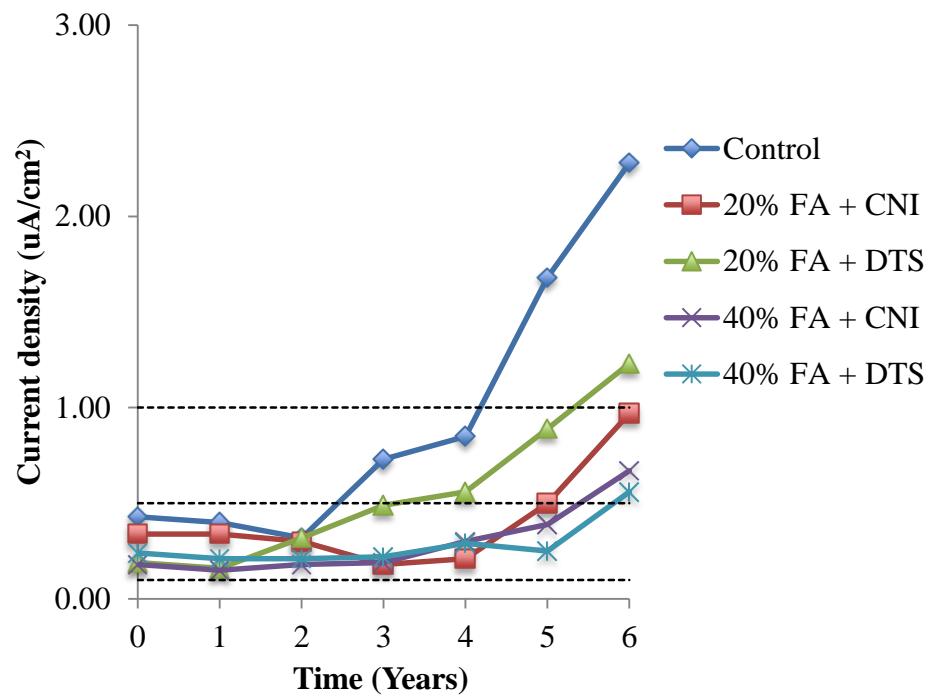
## *Triple combinations*



## *Double combinations*

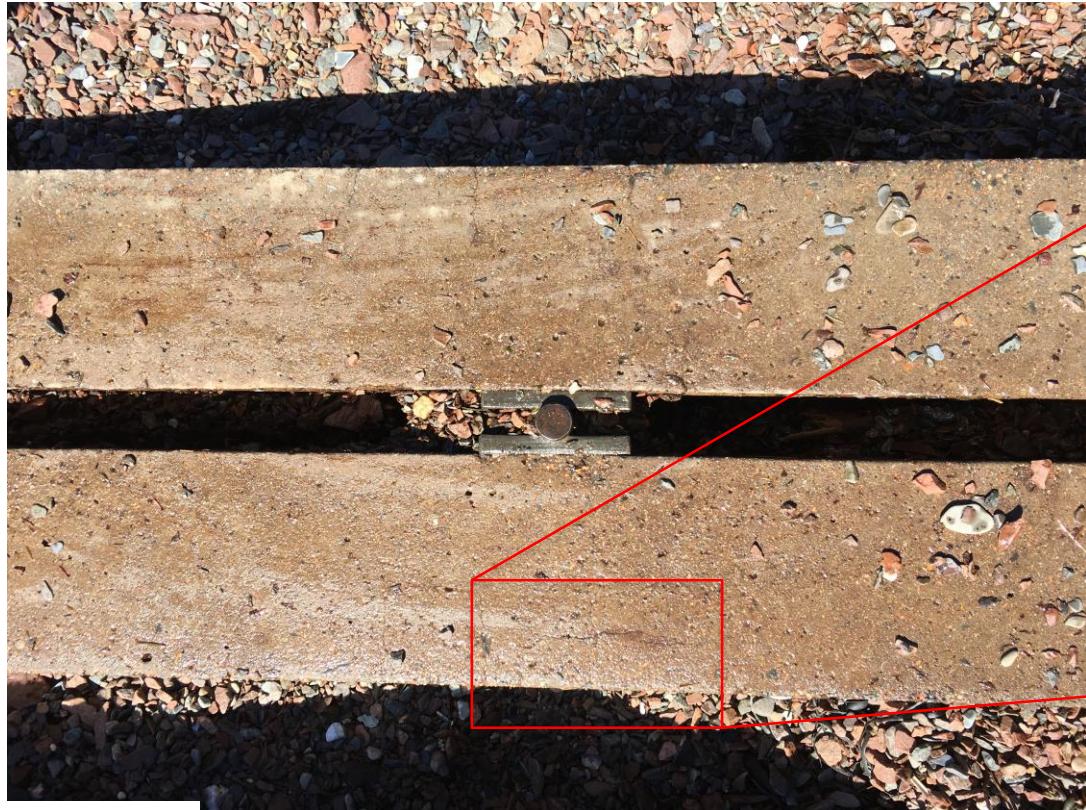


## *Triple combinations*





100% PC



DTS

# Treat Island, Maine, U.S.A.



<b>Variables</b>	<b>No. of Levels</b>	<b>Description</b>
W/CM	3	0.29, 0.37, 0.45
Fly Ash	3	0, 20, 40 %
CNI	3	0, 12.5, 25 L/m <sup>3</sup>
Crack	3	0, 0.25, 0.50 mm

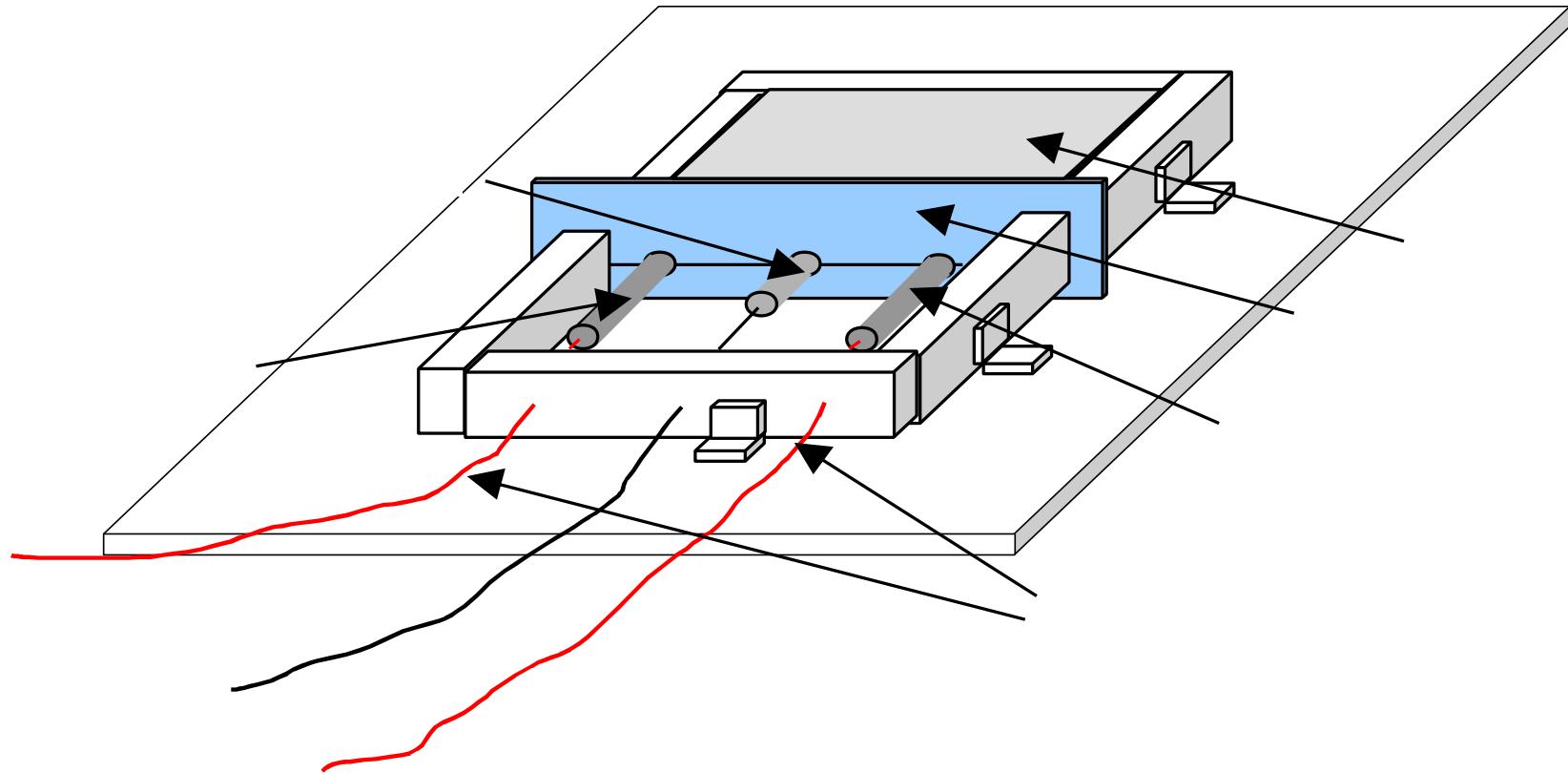
***Portland Cement:*** ASTM Type I with 8% silica fume replacement

***Fly Ash:*** ASTM Type F (CaO = 2.96%)

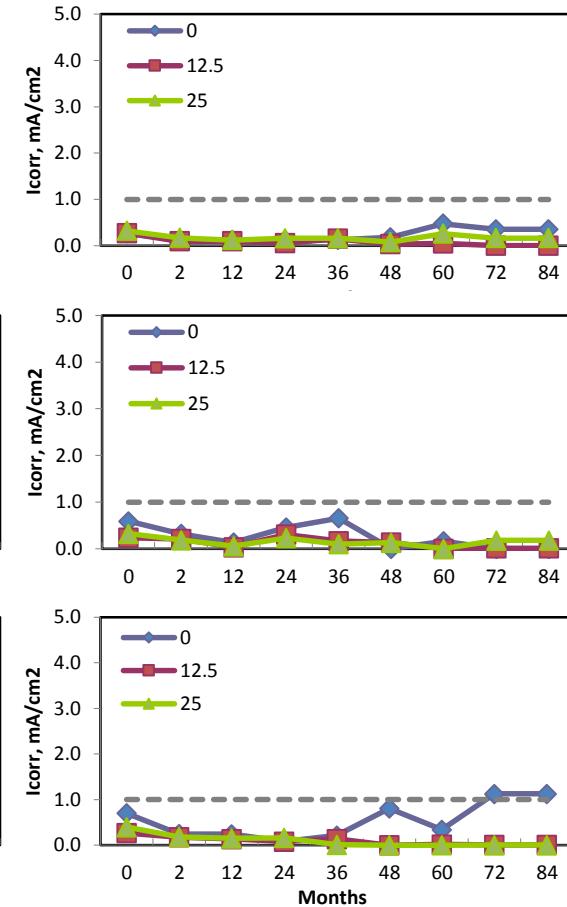
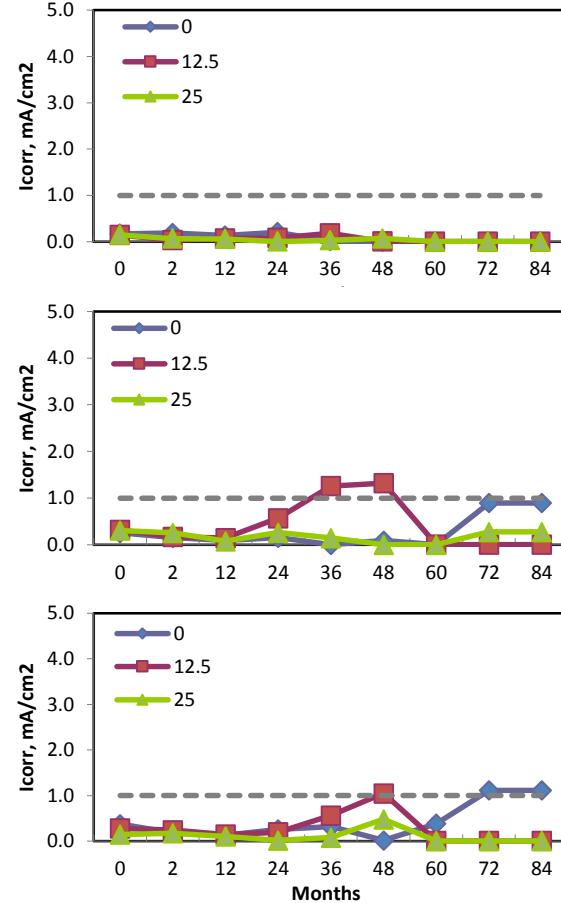
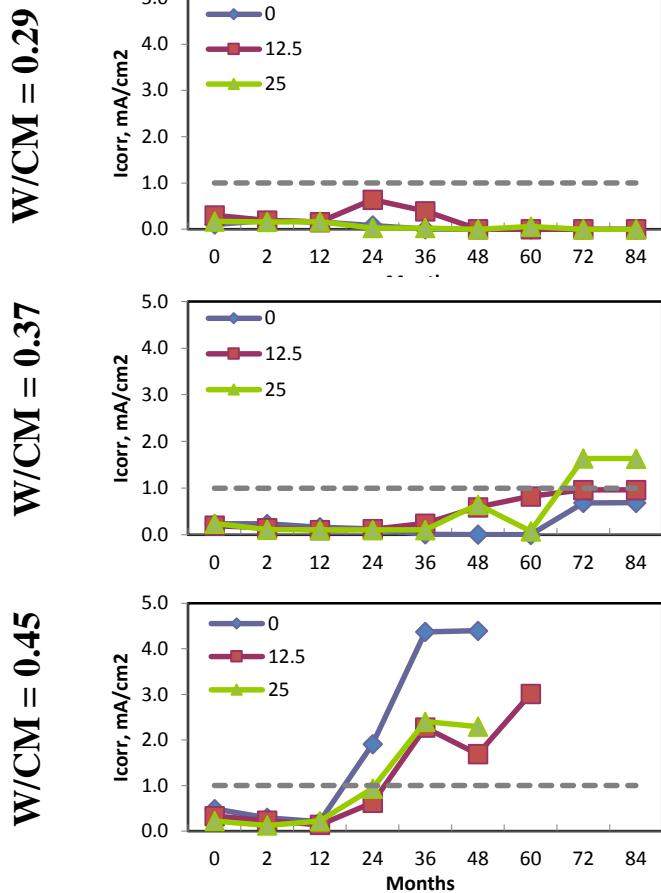
***Cementitious content*** = 360-540 kg/m<sup>3</sup>

***Air*** = 6-8%

***Slump*** = 140-180 mm (5.5-7.0 in.)



# Crack Width (0 mm)



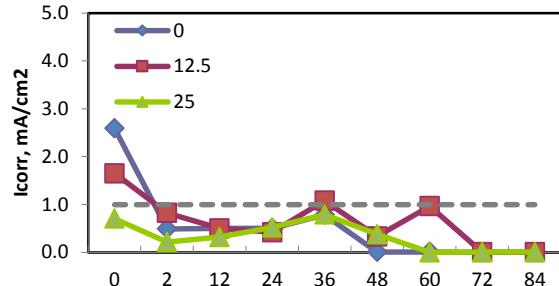
**FA = 0%**

**FA = 20%**

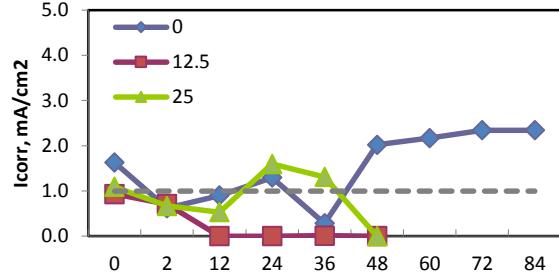
**FA = 40%**

# Crack Width (0.25 mm)

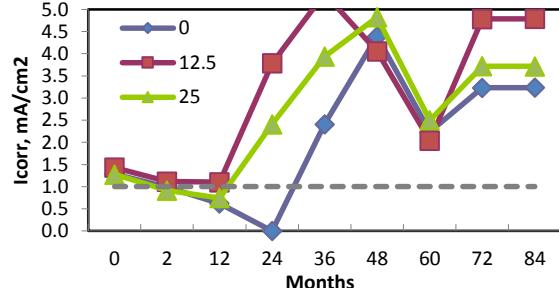
**W/CM = 0.29**



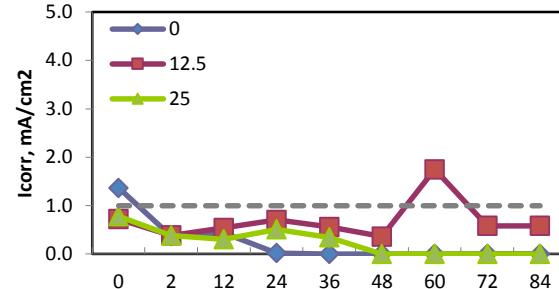
**W/CM = 0.37**



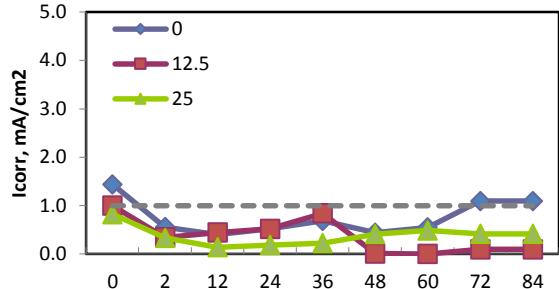
**W/CM = 0.45**



**FA = 0%**



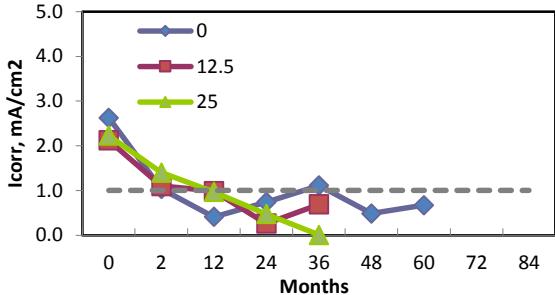
**FA = 20%**



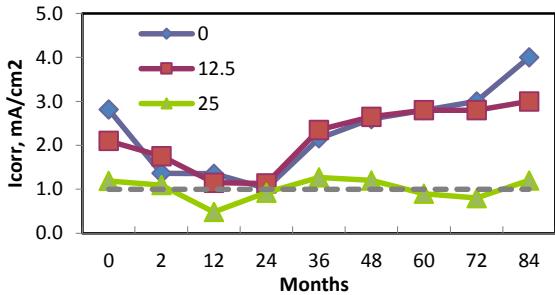
**FA = 40%**

# Crack Width (0.50 mm)

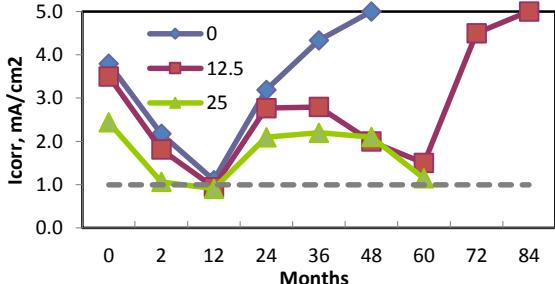
**W/CM = 0.29**



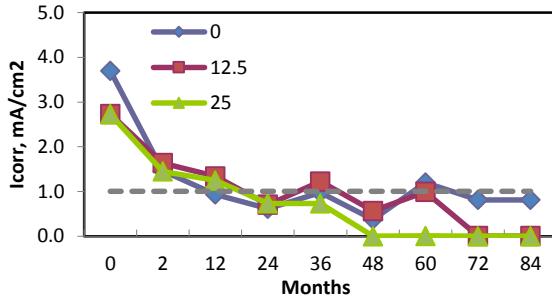
**W/CM = 0.37**



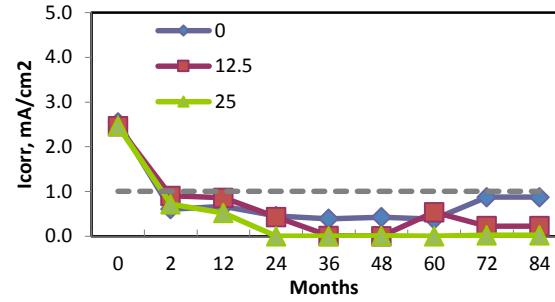
**W/CM = 0.45**



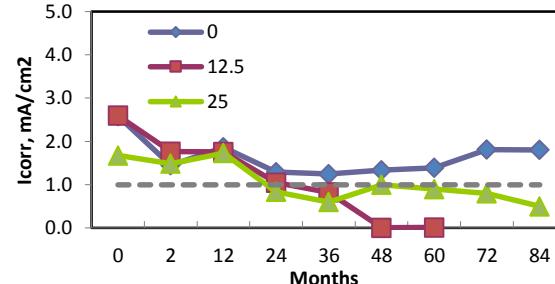
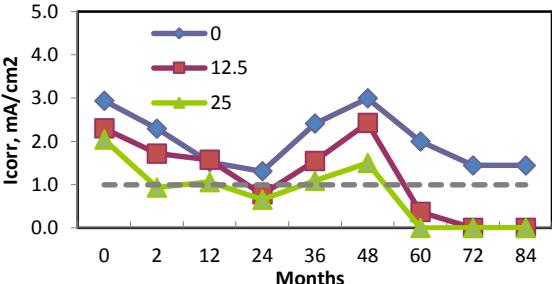
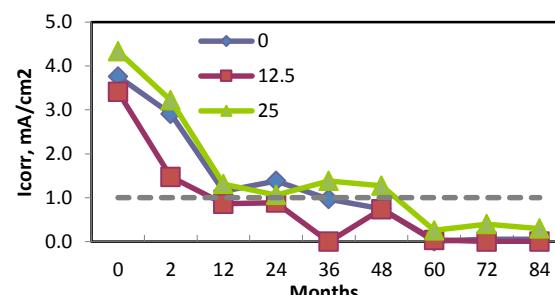
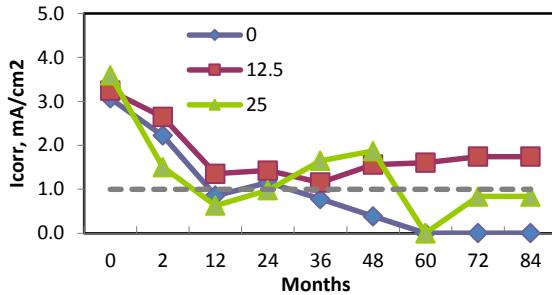
**FA = 0%**



**FA = 20%**



**FA = 40%**



**W/CM = 0.29, FA= 0%, CNI = 0 L/m<sup>3</sup>**



0mm

0.25mm

0.50mm

**W/CM = 0.29, FA= 40%, CNI = 25 L/m<sup>3</sup>**



0mm

0.25mm

0.50mm

**W/CM = 0.37, FA= 0%, CNI = 0 L/m<sup>3</sup>**

**W/CM = 0.37, FA= 40%, CNI = 25 L/m<sup>3</sup>**



0mm

0.25mm

0.50mm



0mm

0.25mm

0.50mm

**W/CM = 0.45, FA= 0%, CNI = 0 L/m<sup>3</sup>**

**W/CM = 0.45, FA= 40%, CNI = 25 L/m<sup>3</sup>**



0mm

0.25mm

0.50mm



0mm

0.25mm

0.50mm

# Conclusions

- **Compressive strength** of HPC is significantly influenced by the combination of CIAs and SCMs.
- The combination of CIA and SCMs showed a synergistic effect in reducing **permeability** of HPC.
- CNI or DTS alone is relatively ineffective in providing protection of reinforcing steel in precracked and cracked HPC. However, the presence of SCMs showed a reduced **corrosion rate**.
- **W/CM** has a marked influence on cracking and corrosion.
- Based on the studied variables, the **width of crack** had no additional detriment effect on corrosion.
- From on the results presented herein, the **best performance** was found in binders containing 40% FA in combination with 25 L/m<sup>3</sup> CNI at all W/CM ratios studied.

**Questions?**

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