



### Evaluation of Chloride-induced Corrosion in Reinforced Calcined Clays and Volcanic Ashes Based Alkali-activated Concretes

Shubham Mishra Clarkson University Potsdam, NY Sulapha Peethamparan, PhD Clarkson University Potsdam, NY



# **Background & Motivation**

Annual Production and Use (Million Tons)

- By 2025, global cement demand 4.7 billion metric tons (an increase of 2.9% per year).
- Low environmental impact binders-Alkali-activated materials
- Fly ash and GGBS popular precursors
- Rapid decommissioning of thermal power plants in and competitive use of Slag as SCMs.
- Calcined clays and volcanic ashes- an emerging unconventional precursor for Alkali activated systems.



Qin et al (2022)



### **Non-traditional Precursors**



Almenares et al. (2017), Case studies in Construction

materials



Khan et al. (2022) Crystals

Investigate chloride-induced corrosion resistance in calcined clay and volcanic ash-based alkali-activated concrete via potentiodynamic tests.
Examine the compatibility of current standard specifications, primarily designed for OPC-based binders, when applied to alkali-activated Calcined clay and Volcanic ash-based concrete(AAC).



## Materials - Binders

#### **Calcined Clays (CC)**

3 kaolinite-based clays (calcined at 750°C) and ground to acquire a reactive form of clay.

#### Volcanic ash (VA)

3 types of ground volcanic ashes of obsidian, pumice, and pumiceous tuff.

| Material ID                        | CC1                | CC2                | CC3                | VA1               | VA2               | VA3               |
|------------------------------------|--------------------|--------------------|--------------------|-------------------|-------------------|-------------------|
| SiO <sub>2</sub> (%)               | 56.0               | 56.3               | 54.4               | <mark>72.0</mark> | <mark>72.4</mark> | <mark>70.4</mark> |
| Al <sub>2</sub> O <sub>3</sub> (%) | <mark>25.02</mark> | <mark>34.89</mark> | <mark>36.83</mark> | 12.13             | 11.50             | 12.83             |
| Fe <sub>2</sub> O <sub>3</sub> (%) | 14.55              | 2.68               | 0.74               | 0.82              | 1.34              | 2.0               |
| CaO (%)                            | <mark>0.06</mark>  | <mark>0.32</mark>  | <mark>0.08</mark>  | 0.72              | 0.84              | 1.91              |
| SO <sub>3</sub> (%)                | 0.04               | 0.05               | 0.09               | 0.06              | n/a               | 0.08              |
| Na <sub>2</sub> Oeq(%)             | 1.01               | 0.78               | 0.20               | <mark>6.72</mark> | <mark>5.83</mark> | <mark>5.51</mark> |
| LOI                                | 0.63               | 1.71               | 4.17               | 4.81              | 4.21              | 3.18              |



Activator Solution: Hybrid solution of sodium hydroxide and sodium

aci) CONCRETE

CONVENTIO



## **Materials**

Concrete mix proportions: 35% paste volume Fine aggregate (FA) / Total aggregate (TA) = 0.45 by volume

 Thapa et al.(Under review) CC and VA-based alkaliactivated concretes(AACs) yielded comp. strength of about 40 MPa.

| Materials                     | s/b            | Binder<br>(kg/m <sup>3</sup> ) | Activator      | Fin <b>Acti</b><br>aggregate | vatoroPaseame | ters<br>Water<br>s/b |
|-------------------------------|----------------|--------------------------------|----------------|------------------------------|---------------|----------------------|
| <b>C<b>C</b>1<b>(9</b>3%)</b> | <b>C83</b>     | Sinder<br>+ 7%CH               | $(kg/m^3)$     | $(kg7m^3)$<br><b>101</b> 8   | $(kg/m^3)$    | $(kg/m^3)$           |
| CC2C27%                       | 0,62           | + <b>3%CH</b> )                | 288            | 84625                        | 107.25        | 0160                 |
| C <b>C3C97</b> %              | 0,03           | + <b>3%CH</b> )                | 432            | 1088                         | <b>1385</b> 5 | 0290                 |
| VAVLAd3%                      | <b>V)}75</b> - | 30%4862-                       | -7% <b>66</b>  | 1016                         | <b>1293</b> 0 | 0195                 |
| VA <b>QA@3%</b>               | <b>VA25</b> -  | 30%CC2-                        | -7% <b>SH)</b> | 101132                       | <b>1290</b> 0 | 01.95                |
| VA3 (63%                      | <b>VA3</b> +   | 30%CC2-                        | -7%CH)         | 12                           | 1.50          | 0.75                 |
| VA3                           | 0.75           |                                | 360            | 999                          | 1271          | 18                   |
| OPC                           | 0.45           | 340                            |                | 510                          | 650           | 154                  |



# **Specimen Preparation**

- Lollipop specimens
   50.8 mm x 101.6 mm.
- An exposure length of 60 mm simulating a cover depth of 20 mm --> region of interest.
- Cured for 28 days
- Immersed in 16.5% NaCl (NT Build 443/ASTM C1556) solution at 23 to 25°C.









- Working electrode: rebar
- Reference electrode:Ag/AgCl electrode
- Counter electrode:

#### stainless steel cylinder





### **Electrochemical Parameters / techniques**

- 1. Open Circuit Potential (OCP) / Corrosion Potential
- OCP most widely used corrosion index
- Monitored for 900 seconds

 Table 1. ASTM C876-91 criteria for corrosion of steel in concrete for Ag/AgCl/1M KCl standard

 reference electrode

| Silver/silver chloride/ 1.0M KCl | Corrosion condition                               |
|----------------------------------|---|
| > - 100 mV                       | Low (10%) risk of corrosion                       |
| - 100 to -250 mV                 | Uncertain corrosion risk                          |
| < - 250 mV                       | High (> 90%) risk of corrosion                    |
| < - 400 mV                       | Severe corrosion (or low oxygen/water saturation) |

#### 2. Linear Polarization Resistance (Rp)

- Rp : ratio of the applied potential (E) to the resulting current density (i) in the E vs. i plot.
- ASTM G 59
- Forward scan from OCP -30 mV to OCP+30 mV at 0.1 mV/s.





### **Electrochemical Parameters / techniques**

- Corrosion current density (i<sub>corr</sub>) only electrochemical parameter that quantifies the rate of loss of metal
- Tafel tests were conducted to estimate B using anodic and Cathodic constants.
- Forward scan from OCP 100 mV to OCP +100 mV at a scanning rate of 1 mV/s.

$$i_{corr} = \frac{B}{Rp} = \left[\frac{\beta_a.\beta_c}{2.303(\beta_a + \beta_c)}\right] \frac{1}{Rp}$$

B = Tafel constant

 $\beta_a$  = Anodic Tafel constant, mV/decade  $\beta_c$  = Cathodic Tafel constant, mV/decade Rp= Polarization resistance, k $\Omega$ -cm<sup>2</sup>



| $i_{\rm corr}$ ( $\mu$ A/cm <sup>2</sup> ) | Classification   |  |  |
|--|------------------|--|--|
| < 0.1                                      | Passive/very low |  |  |
| 0.1 to 0.5                                 | Low/moderate     |  |  |
| 0.5 to 1.0                                 | Moderate/high    |  |  |
| > 1.0                                      | Very High        |  |  |



# **Open Circuit Potential (OCP)**



- Higher negative potentials observed for rebars embedded in AACs
- AAC's unique pore solution chemistry and lack of oxygen at the steelconcrete interface particularly at cathodic regions → refined microstructure



## Linear Polarization Resistance (Rp)



- A sharp decline followed by a stable trend is noted in Rp observation for reinforced AACs.
- Similar to corrosion potential trends.
- OPC the constant decline in Rp indicates the onset of corrosion activity.

# **Corrosion Current Density (i<sub>corr</sub>)**



- Higher apparent corrosion current densities for AACs -> potential depassivation of embedded rebars
- Indicates lower resistance of such AACs to chloride-initiated corrosion.



### Retrieved reinforcements @ 1 year



- No signs of active corrosion/ rust stains/ pitting spots – noted for AACs.
- For OPC rebar: exposed area corroded



# **Tafel constants**

| Mixoc   | Tafel Constant (B) values in mV/decade |         |         |         |          |          |          |          |
|---------|--|---------|---------|---------|----------|----------|----------|----------|
| IVIIXES | 0 days                                 | 28 days | 56 days | 84 days | 112 days | 180 days | 270 days | 360 days |
| OPC     | 68.07                                  | 59.91   | 50.25   | 44.4    | 47       | 29.54    | 23.31    | 19.21    |
| CC1     | 13.20                                  | 17.87   | 12.89   | 9.65    | 17.29    | 18.38    | 29.24    | 26.40    |
| CC2     | 16.25                                  | 15.08   | 18.02   | 16.35   | 16.34    | 22.58    | 28.17    | 25.62    |
| CC3     | 31.33                                  | 18.00   | 44.72   | 21.98   | 39.59    | 28.22    | 33.91    | 29.26    |
| VA1     | 27.05                                  | 10.79   | 11.75   | 12.18   | 32.23    | 35.52    | 31.77    | 35.49    |
| VA2     | 17.49                                  | 17.69   | 10.49   | 12.24   | 40.22    | 31.28    | 34.00    | 32.86    |
| VA3     | 18.77                                  | 13.19   | 14.36   | 15.93   | 35.29    | 34.22    | 37.92    | 29.09    |

| lcorr (µA/cm²) | <b>Corrosion level</b> |
|----------------|------------------------|
| < 0.5          | Negligible             |
| 0.5-2.5        | Low                    |
| 2.5-5          | Moderate               |
| >5             | High                   |

 Existing literature suggests a revision of the thresholds to increase by 3 to 5 times.

- Literature B for OPC: 26 (active) and 52(passive)
- AAC's vary b/w 10 to 35.
- Literature B values (13 to 25) for passive low calcium binder-based AACs Vs. 52 for OPC.
- OPC-centric thresholds are unfit to verify the corrosion activity in AACs.



### **Recommended Thresholds**





# **Summary and Future Works**

- All the tested AACs demonstrate significant resistance to chloride-induced corrosion.
- Distinction in corrosion response from conventional concrete Unique pore solution composition
- OPC-specific standard limits were unfit to predict corrosion activity in studied AACs.
- Need to redesign the thresholds to accommodate the actual condition of rebars as confirmed by extractions.
- Revised limits indicate negligible to minor corrosion activity in AACs.

#### **Future Works**

- Correlating the pore solution chemistry of AACs to the corrosion characteristics
- Relating bulk chloride diffusion response of AACs to the corrosion behavior.



## Acknowledgement

- Federal Highway Administration (FHWA)- Funding
- Penn State University and Purdue University Collaborators
- CAMP- Clarkson University









