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**Development and Application of** Non-proprietary UHPC Mixtures for **Pretensioned Bridge Girders** ACI / JCI – 6th Joint Seminar Mary Beth Hueste, Anol Mukhopadhyay, Stefan Hurlebaus, John Mander Amreen Fatima, Hyeonki Hong, Tevfik Terzioglu, Brittni Cooper, Jay Shah

Zachry Department of Civil & Environmental Engineering Texas A&M University Texas A&M Transportation Institute College Station, Texas

## **Research Objectives**

Development of Nonproprietary UHPC Mixtures
 Production of Full-Scale Precast Pretensioned Bridge Girders
 Full-Scale UHPC Girder Testing





# Part I: Development of Nonproprietary UHPC Mixture and Plant Production





# **Requirements for UHPC Mixture Development**

#### Questionnaire Results

- Constituent materials
  - Currently used materials
  - Type III cement, fly ash, HRWR, natural sand
- Curing
  - No heat treatment
- Prestressing transfer
  - Within 16 20 hours
- Mixing and Placement
  - Use existing mixer (50-60% of capacity) and standard transporters

#### Properties and Durability

- Workability
  - Sufficient flow spread
- Mechanical Properties
  - $f'_{ci}$  at release = 12 14 ksi
  - $f_c'$  at service = 18 20 ksi
- Durability
  - Superior transport properties

Challenge: achieving 12 – 14 ksi within 20 hours without heat treatment



# Selected Mixture Optimized with Precast Plant Materials

#### **Mixture Proportion Comparison**

Constituent	Proprietary UHPC <sup>1</sup>	Developed Plant UHPC	Material used in Study
Cement	1.00	1.00	Type III
Silica fume	<u>0.33</u>	<u>0.08</u>	Densified
GQ / <u>Fly ash</u>	0.30 (GQ)	0.10	Class F fly ash
Sand	1.43	1.12	Natural sand, #4
Water	0.15	0.21	
HRWR	0.04	0.024	
Accelerator	0.04		
Steel fiber	2.0% by volume	<u>1.5% by</u> volume	0.008" diameter 0.5" long



1. FHWA-HRT-06-103

Mix proportion by cement weight

2. GQ: Ground Quartz



# Production of UHPC Girder at Precast Plant





UHPC Mixing using existing twin shaft mixer



*Vibrating the screen for steel fiber addition* (2 in. spacing screen)



Placement using Tuckerbuilt

# Production of UHPC Girder at Precast Plant

Tx34-2 Girder, 50 ft long





## **Compressive Strength**

Property	Target	Average Value (cast samples at plant)	Comment
Compressive strength	<ul> <li>12 – 14 ksi (release)</li> <li>18 – 20 ksi (service)</li> </ul>	<ul> <li>&gt; 12 ksi at release (20 hours)</li> <li>14.3 – 16.1 ksi (24 hours)</li> <li>17.9 – 19.2 ksi (28 days)</li> </ul>	✓ Target met





# **Additional Hardened Properties**

Property	Target	Average Value (cast samples at plant)	Comment
Modulus of Elasticity	_	• 6300 – 7400 ksi	Consistent with literature
Uniaxial Tensile Strength	<ul><li>0.75 ksi at release</li><li>1.0 ksi at service</li></ul>	<ul> <li>0.55 – 0.81 ksi (7 days)</li> <li>0.31 – 1.28 ksi (28 days)</li> </ul>	Average is slightly less than target, but individual specimens met the target.
Inferred Flexural Tension Strength	<ul> <li>2.0 ksi at service (PCI recommendation)</li> </ul>	<ul> <li>1.9 – 2.0 ksi (3 days)</li> <li>2.0 – 2.4 ksi (28 days)</li> </ul>	✓ Strength target met



Modulus of Elasticity Test Setup



Uniaxial Tensile Strength Test Setup



Inferred Tension Bending Test Setup

# Durability

Bulk / Surface Resistivity at 56 days (kΩ-cm)	RCPT (Coulombs)	ASR (with reactive sand)	Freeze-Thaw Resistance	Scaling Resistance	Abrasion Resistance (mass loss)	Service Life Prediction*
210 / 214 (Very Low)	54 (Negligible)	0.049x10 <sup>-3</sup> at 90 days (Negligible)	No degradation (Mass Change: 0.04%)	Rating 1 (Very slight scaling)	Top: 0.07% Bottom: 0.03%	> 150 years



- \* Service life prediction analyzed using Fick's 2<sup>nd</sup> law with bulk resistivity data.
- \* Diffusion coefficient: 2.75 x  $10^{-14}$  m<sup>2</sup>/s





Surface resistivity testing

Abrasion resistance testing (left) and samples after abrasion (right)

# Fiber Distribution and Orientation

• Fiber distribution was investigated using <u>cored samples from the girders</u> with X-ray CT scanning and infrared images.



Well Distributed and Randomly Oriented Fibers

Possible Formation of Elephant Skin for Tx54 Girder Specimen



# **Cost Analysis**

#### Cost Comparison

UHPC	\$ / cyd	Materials (Fiber volume) Source		
TxDOT	\$602	Type III, natural sand (1.5%)	This research study	
Michigan DOT	\$893	Type I, quartz sand (2.0%)	El-Tawil et al. (2018)	
Montana DOT	\$561	Type I/II, masonry sand (2.0%)	Berry et al. (2017)	
Missouri DOT	\$1017	Type III, natural sand (2.0%)	Khayat and Valipour (2018)	
FHWA \$730		Type II/V, natural sand (1.5%)	Wille (2013)	
	\$965	White, natural sand (1.5%)		
	\$1122	White, quartz sand (1.5%)		
Proprietary	\$2000	Not listed	Tadros (2019)	

#### Cost of Developed Mix (\$/cyd)\*



\*Cost analysis was conducted in 2020.



# Part I: Development of UHPC Mixture: Summary and Conclusions

#### • Development of Nonproprietary UHPC Mixture

- ✓ Locally available and commonly used materials at precast plant in Texas.
- ✓ Reduction in steel fiber content (1.5 percent) for cost-effectiveness.
- ✓ High early strength (12–14 ksi within 20 hours) without heat treatment and accelerator.
- ✓ Superior durability: high resistivity and freeze-thaw, scaling, abrasion, and ASR resistance.
- ✓ Long service life span (150+ years)

#### • Production and Fabrication

- ✓ Successful use of existing mixer (50–60% mixer capacity)
- $\checkmark$  Girder fabrication with multiple batches and placements using Tuckerbuilt
- ✓ Release at 20 hours (compressive strength > 12 ksi)
- Fiber Distribution and Orientation
  - $\checkmark$  Overall, steel fibers were well-distributed with random orientation.
  - ✓ Possible risk of fiber segregation due to a high flow spread (> 11 in.) or elephant skin formation



### Part 2: Structural Full-Scale Testing





# Structural Full-Scale Testing

#### Major Technical Objectives

- ✓ Conduct *flexure test* at midspan each girder specimen
- ✓ Conduct *shear test* at each end of girder specimen
- ✓ Compare the *experimental* observations with the *predicted* capacity and *design* strength



Tx34-1 Girder Test Setup

Tx34-2 Girder Specimen

Tx54 Girder Test Setup



# Tx54 Girder Specimen: Harped Tendon Profile





# **Tx54 Flexure Test**

- Flexure crack occurred at 560 kips (total actuator load)
- Shear crack developed at the ends at 698 kips
- Flexure and shear crack formation increased at 720 kips





Flexure Cracks Tx54

# Tx54 Minimum Web Reinf. End - Shear Test

- Shear Span-to-Depth Ratio = 2.37
- Uniaxial Tensile Strength = 0.95 ksi







Shear Force vs Maximum Deflection

### Tx54 No Web Reinf. End - Shear Test



Shear Force vs Maximum Deflection

### Girder Specimens – Demand and Capacity



# Girder Testing: Summary and Conclusions

#### • Design

- ✓ AASHTO Draft Recommendations for UHPC: nominal flexure and shear strengths are conservative relative to measured strengths
- ✓ UHPC bridge girders provide increased design efficiency compared to CC girders with reduced crosssections, longer spans, and larger girder spacings.

#### • Flexure Performance

- $\checkmark$  No cracking observed up to factored load demand.
- ✓ Applied moment demand on girder specimens ranged from 30–47 percent higher than factored design moment.

#### • Shear Performance

- ✓ Minimum transverse reinforcement and harped tendons enhance shear performance.
- ✓ All girder ends provided at least twice the shear capacity of the factored demand [except Tx34-1 end with no web reinforcement and low uniaxial tensile strength].

#### Composite Action

- ✓ Interface shear reinforcement controlled the interface slip up to factored design loads.
- ✓ Limited slip was observed at higher loads.









# Thank you!

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#### Final Report

- Vol. 1 UHPC Mixture Development and Material-Level Experiments
- Vol. 2 Structural Analysis, Design, and Fullscale Testing of Precast, Pretensioned Girders
- Vol. 3 UHPC Production Guidelines and Design Recommendations with Design Examples

# Appendix



# **UHPC Project Team**

#### **Texas Department of Transportation**

- Tom Schwerdt (TxDOT, Project Manager)
- Robert Owens (TxDOT, Project Director)
- TxDOT Project Monitoring Committee: Ahmed Al-Basha, Biniam Aregawi, Rachel Cano, Geetha Chandar, Chad Dabbs, Jamie Farris, Igor Kafando, Andy Naranjo, Joe Roche, Prapti Sharma, Jason Tucker



#### TAMU/TTI Research Team

- Mary Beth Hueste RS
- Anol Mukhopadhyay, Stefan Hurlebaus, John Mander
- Amreen Fatima, Hyeonki Hong, Tevfik Terzioglu, Brittni Cooper, Jay Shah



# Recommended Flow Spread Value for Qualification and Acceptance Testing

Flow Spread Range, in.	Color Code	Description	Comments
flow < 9.5	Red	Unacceptable	<ul> <li>Poor workability</li> </ul>
			<ul> <li>Higher risk of elephant skin</li> </ul>
			formation
$9.5 \le \text{flow} < 10.0$	Orange	Acceptable	<ul> <li>Relatively low workability</li> </ul>
			<ul> <li>Some risk of elephant skin</li> </ul>
			formation
$10.0 \le \text{flow} \le 10.5$	Green	Desirable	<ul> <li>Good workability</li> </ul>
			<ul> <li>None or negligible risk of</li> </ul>
			elephant skin
			<ul> <li>Negligible fiber segregation*</li> </ul>
$10.5 < flow \le 11.0$	Yellow	Acceptable	<ul> <li>Some risk of fiber segregation</li> </ul>
			<ul> <li>Better acceptability compared</li> </ul>
			to mixture with flow < 10.0 in.
flow > 11.0	Red	Unacceptable	<ul> <li>High risk of fiber segregation</li> </ul>



### Recommended Values for Qualification and Acceptance Testing

Property	Recommended Value
Temperature at	80 – 100 °F is recommended. A high discharge
discharge	temperature near 100 °F demands placement within
	a relatively short period (less than 10 minutes).
Density	150 – 155 lb/ft <sup>3</sup> is recommended for 1.5 percent fiber
	volume.
Compressive strength	$f'_{c \ at \ release} \geq 65\% \ of \ f'_{c \ at \ service}$
	$[f'_{c \ at \ release} \ge 12 \ ksi \ when \ f'_{c \ at \ service} = 18 \ ksi]$
Direct uniaxial tension	0.70 – 0.75 ksi at release, 0.85 – 1.0 ksi at service
test	

