



# **Assessing Deterioration of Concrete Structures using Self-Sufficient Reactive-Transport Modeling**

**O. Burkan Isgor and W. Jason Weiss**

# Acknowledgements



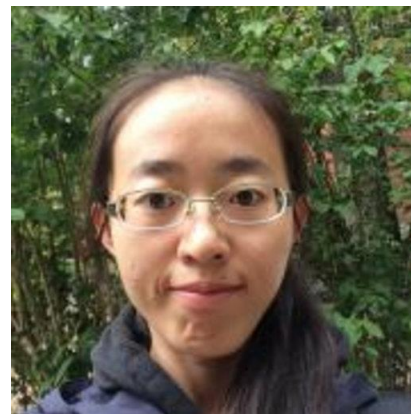
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# Concrete sustainability



(Vector Corrosion Technologies)

Life Cycle  
Performance

Increase the service life of the structures

Performance-based  
mixture proportioning

Service life modeling

Reduced  
carbon  
footprint

Reduce  
Clinker

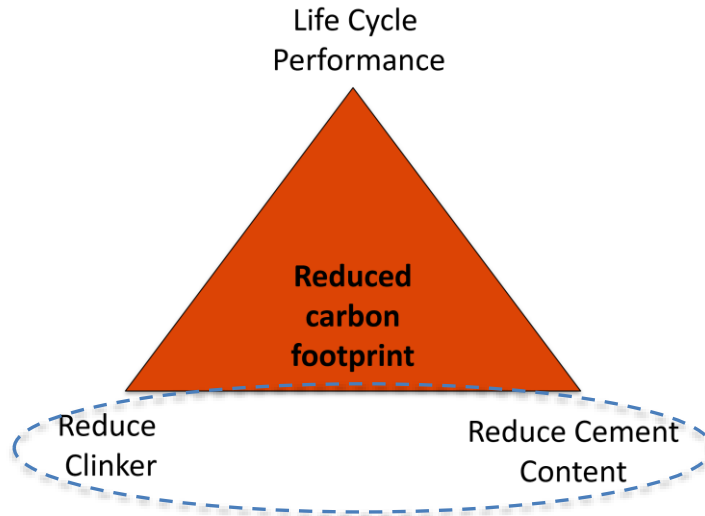
Reduce Cement  
Content

Increase the use of low-carbon footprint  
cementitious materials and powder extenders

# Concrete sustainability



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**Increase the use of low-carbon footprint cementitious materials and powder extenders**

- We have been using conventional (in-spec) SCMs, some limestone, etc.
- Time to consider
  - underutilized, novel, low-carbon footprint binders
    - Off-spec SCMs (off-spec fly ash, natural pozzolans, slag, etc.)
    - Other types of ashes (bottom ash, reclaimed ash, agricultural ash, etc.)
    - Other industrial and natural products (pumice, clays, etc.)
- Increased use of powder extenders
  - Larger limestone replacement
  - Synergies with binders (e.g., limestone + Al-containing binders)

# Challenges



OPC chemistry  
 $C_3S$ ,  $C_2S$ ,  $C_3A$ ,  $C_4AF$ ,  
 $Na_2O$ ,  $K_2O$ , etc



Other binder  
chemistry  
 $SiO_2$ ,  $Al_2O_3$ ,  $CaO$ ,  
 $Na_2O$ ,  $K_2O$ , etc.

- **Do we know how these unconventional binders react?**
  - Maximum reactivity (portion of the reactive components)?
  - Reactions vs. time
- **Do we know how to proportion mixtures with these unconventional binders?**
  - For specified performance
  - For cost
  - For lowest carbon footprint
  - Etc.
- **Can we perform service life modeling of concrete produced with these materials?**
  - Modeling transport of deteriorative species (e.g., chlorides, sulfates, etc.)
  - Modeling reactive processes (e.g., chloride binding, sulfate attack, salt damage, etc.)

Performance-based mixture  
proportioning  
Bharadwaj et al. 2022

Service life modeling  
(this presentation)

# Service life modeling of concrete



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Moisture movement (e.g., wetting/drying, ponding, etc.)



Transport of ionic (e.g., chloride, sulfates, etc.), gaseous (e.g.,  $\text{CO}_2$ ,  $\text{O}_2$ ) species

Diffusion

+

Electrical  
migration

+

Chemical  
activity

+

Advection



Reactions (e.g., chloride binding, sulfate attack, carbonation, etc.)

# Service life modeling of concrete



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Moisture movement (e.g., wetting/drying, ponding, etc.)



Transport of ionic (e.g., chloride, sulfates, etc.), gaseous (e.g., CO<sub>2</sub>, O<sub>2</sub>) species

Diffusion

+

Electrical  
migration

+

Chemical  
activity

+

Advection



Reactions (e.g., chloride binding, sulfate attack, carbonation, etc.)

# Service life modeling of concrete



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Ionic flux = Diffusion + Electrical migration + Chemical activity + Advection



# Service life modeling of concrete



$$\underbrace{-D_i \nabla c_{aq,i}}_{\text{Diffusion}} - \underbrace{D_i c_{aq,i} \frac{Fz}{RT} \nabla \phi}_{\text{Electrical migration}} - \underbrace{D_i c_{aq,i} \nabla \ln \gamma_i}_{\text{Chemical activity}} + \underbrace{c_{aq,i} v_L + c_{G,i} v_G}_{\text{Advection}}$$

Ionic flux =

Diffusion

+

Electrical  
migration

+

Chemical  
activity

+

Advection

# Reactive-transport modeling



$$\frac{\partial [\varphi c_{aq,i}]}{\partial t} \frac{\partial c_{s,i}}{\partial t} = - \sum_{n_i} \nabla \cdot \left( \underbrace{-D_i \nabla c_{aq,i}}_{\text{diffusion}} - \underbrace{D_i c_{aq,i} \frac{Fz}{RT} \nabla \phi}_{\text{electrical migration}} - \underbrace{D_i c_{aq,i} \nabla \ln \gamma_i}_{\text{chemical activity}} \right)$$

# Reactive-transport modeling



$$\frac{\partial [\phi c_{aq,i}]}{\partial t} - \frac{\partial c_{s,i}}{\partial t} = - \sum_{n_i} \nabla \cdot \left( \underbrace{D_i \nabla c_{aq,i}}_{\text{diffusion}} - \underbrace{D_i c_{aq,i} \frac{Fz}{RT} \nabla \phi}_{\text{electrical migration}} - \underbrace{D_i c_{aq,i} \nabla \ln \gamma_i}_{\text{chemical activity}} \right)$$

Porosity  
 Reactions  
 (e.g., chloride binding, carbonation, etc.)  
 Diffusivities

# Reactive-transport modeling



$$\frac{\partial[\phi c_{aq,i}]}{\partial t} - \frac{\partial c_{s,i}}{\partial t} = - \sum_{n_i} \nabla \cdot \left( \underbrace{D_i \nabla c_{aq,i}}_{\text{diffusion}} - \underbrace{D_i c_{aq,i} \frac{Fz}{RT} \nabla \phi}_{\text{electrical migration}} - \underbrace{D_i c_{aq,i} \nabla \ln \gamma_i}_{\text{chemical activity}} \right)$$

Porosity

Reactions  
(e.g., chloride binding)

Diffusivities

Experimentally obtained

- Error prone
- Inaccurate / unrepresentative
- Time consuming
- Expensive

# “Self-sufficient” model



$$\frac{\partial[\phi c_{aq,i}]}{\partial t} - \frac{\partial c_{s,i}}{\partial t} = - \sum_{n_i} \nabla \cdot \left( \underbrace{-D_i \nabla c_{aq,i}}_{\text{diffusion}} - \underbrace{D_i c_{aq,i} \frac{Fz}{RT} \nabla \phi}_{\text{electrical migration}} - \underbrace{D_i c_{aq,i} \nabla \ln \gamma_i}_{\text{chemical activity}} \right)$$

Porosity  
 Theoretical  
 (using MPPM)

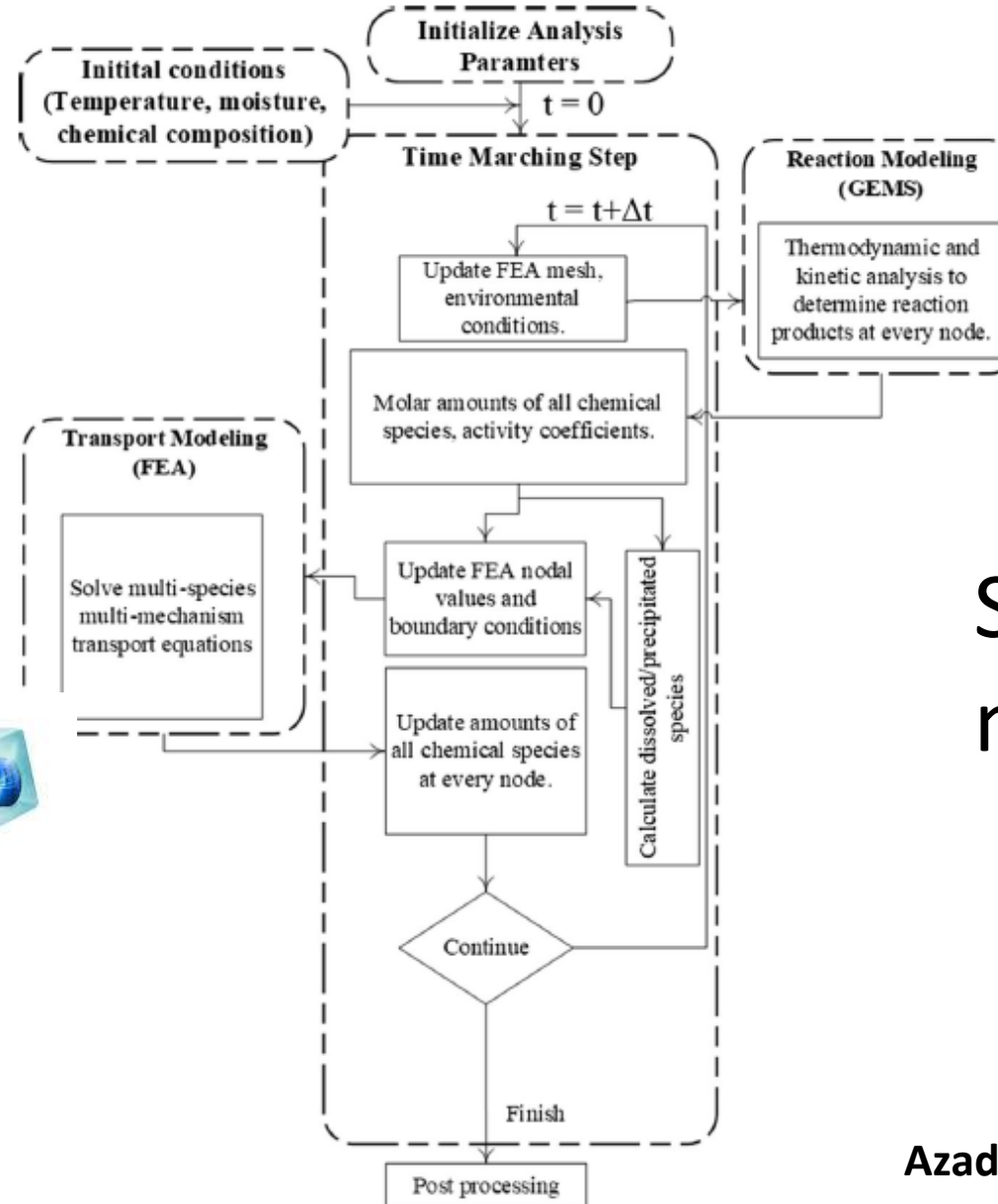
Reactions  
 (e.g., chloride binding)  
 Theoretical  
 (using kinetic/thermodynamic modeling)

Diffusivities  
 Theoretical  
 (using MPPM)

Isgor and Weiss, *Materials & Structures*, 2019  
 Azad et al., *Computer & Geosciences*, 2016

**MPPM:** Modified Pore Partitioning Model  
 (Powers + GEMS) up-scaled to concrete

# Time marching



Multiphysics Object-Oriented Simulation Environment



## Self-sufficient modeling algorithm

Azad et al., Computer & Geosciences, 2016



# How do we move from “empirical” to “self-sufficient”?

# Gibbs energy minimization (GEM)



## EXAMPLE:

### INPUT

1000 g OPC + 400 g H<sub>2</sub>O

425 g C<sub>3</sub>S

325 g C<sub>2</sub>S

80 g C<sub>3</sub>A

70 g C<sub>4</sub>AF

30 g Na<sub>2</sub>O

20 g K<sub>2</sub>O

50 g gypsum (CaSO<sub>4</sub>)

Etc.



### OUTPUT

??? g of C-S-H

C-S-H-1, C-S-H-2, etc.

??? g of CH

??? g of AFm

AFm1, AFm2, etc.

??? g of AFt

AFt1, AFt2, etc.

??? pore solution

Ca<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>, etc.

1,400 g



# Gibbs energy minimization (GEM)



## EXAMPLE:

### INPUT

1000 g OPC + 400 g H<sub>2</sub>O

425 g C<sub>3</sub>S

325 g C<sub>2</sub>S

80 g C<sub>3</sub>A

70 g C<sub>4</sub>AF

30 g Na<sub>2</sub>O

20 g K<sub>2</sub>O

50 g gypsum (CaSO<sub>4</sub>)

Etc.

Gibbs Free Energy



Trials

### OUTPUT 1

500 g of C-S-H

C-S-H-1, C-S-H-2, etc.

400 g of CH

200 g of AFm

AFm1, AFm2, etc.

200 g of AFt

AFt1, AFt2, etc.

100 g pore solution

Ca<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>, etc.

1,400 g

# Gibbs energy minimization (GEM)

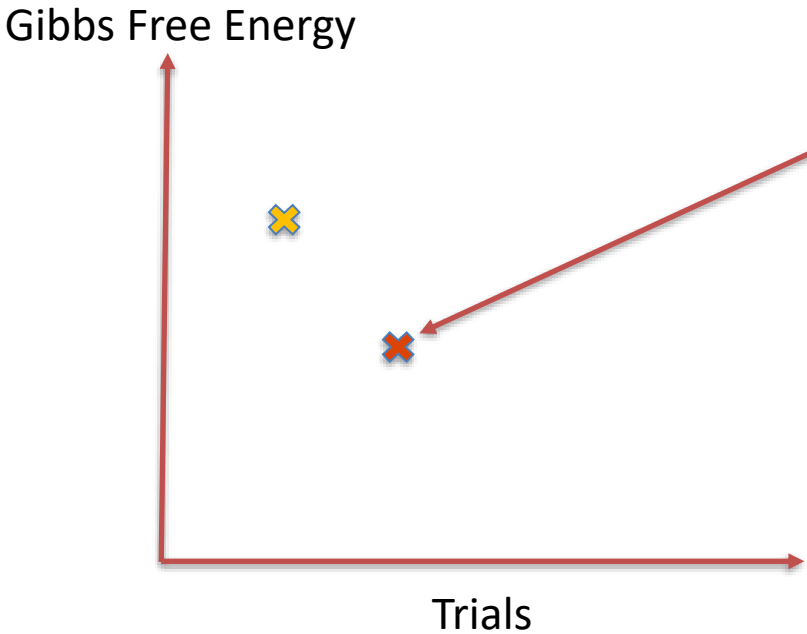


EXAMPLE:

INPUT

1000 g OPC + 400 g H<sub>2</sub>O

- 425 g C<sub>3</sub>S
- 325 g C<sub>2</sub>S
- 80 g C<sub>3</sub>A
- 70 g C<sub>4</sub>AF
  
- 30 g Na<sub>2</sub>O
- 20 g K<sub>2</sub>O
  
- 50 g gypsum (CaSO<sub>4</sub>)
  
- Etc.



OUTPUT 2

- 550 g of C-S-H  
C-S-H-1, C-S-H-2, etc.
  - 350 g of CH
  - 175 g of AFm  
AFm1, AFm2, etc.
  - 225 g of AFt  
AFt1, AFt2, etc.
  - 100 g pore solution  
Ca<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>, etc.
- 1,400 g

# Gibbs energy minimization (GEM)



## EXAMPLE:

### INPUT

1000 g OPC + 400 g H<sub>2</sub>O

425 g C<sub>3</sub>S

325 g C<sub>2</sub>S

80 g C<sub>3</sub>A

70 g C<sub>4</sub>AF

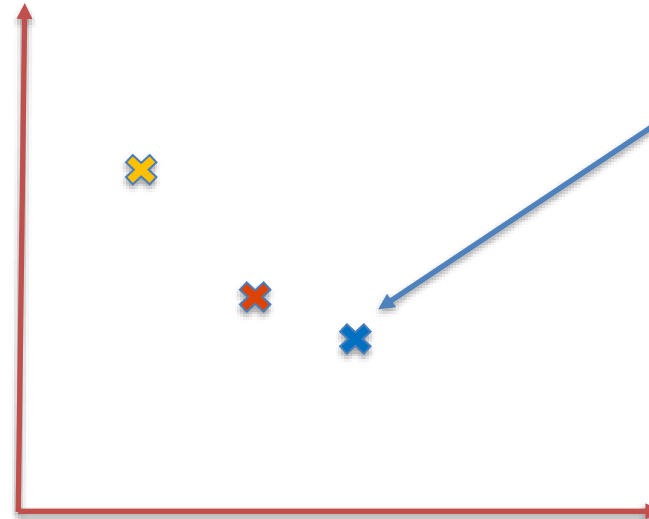
30 g Na<sub>2</sub>O

20 g K<sub>2</sub>O

50 g gypsum (CaSO<sub>4</sub>)

Etc.

Gibbs Free Energy



Trials

### OUTPUT n

555 g of C-S-H

C-S-H-1, C-S-H-2, etc.

345 g of CH

180 g of AFm

AFm1, AFm2, etc.

210 g of AFt

AFt1, AFt2, etc.

110 g pore solution

Ca<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>, etc.

1,400 g

# Gibbs energy minimization (GEM)



## EXAMPLE:

### INPUT

1000 g OPC + 400 g H<sub>2</sub>O

425 g C<sub>3</sub>S

325 g C<sub>2</sub>S

80 g C<sub>3</sub>A

70 g C<sub>4</sub>AF

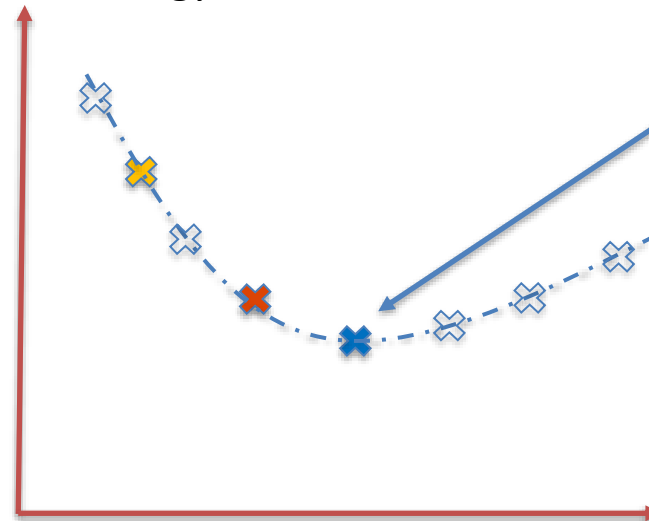
30 g Na<sub>2</sub>O

20 g K<sub>2</sub>O

50 g gypsum (CaSO<sub>4</sub>)

Etc.

Gibbs Free Energy



Trials

### SOLUTION

555 g of C-S-H

C-S-H-1, C-S-H-2, etc.

345 g of CH

180 g of AFm

AFm1, AFm2, etc.

210 g of AFt

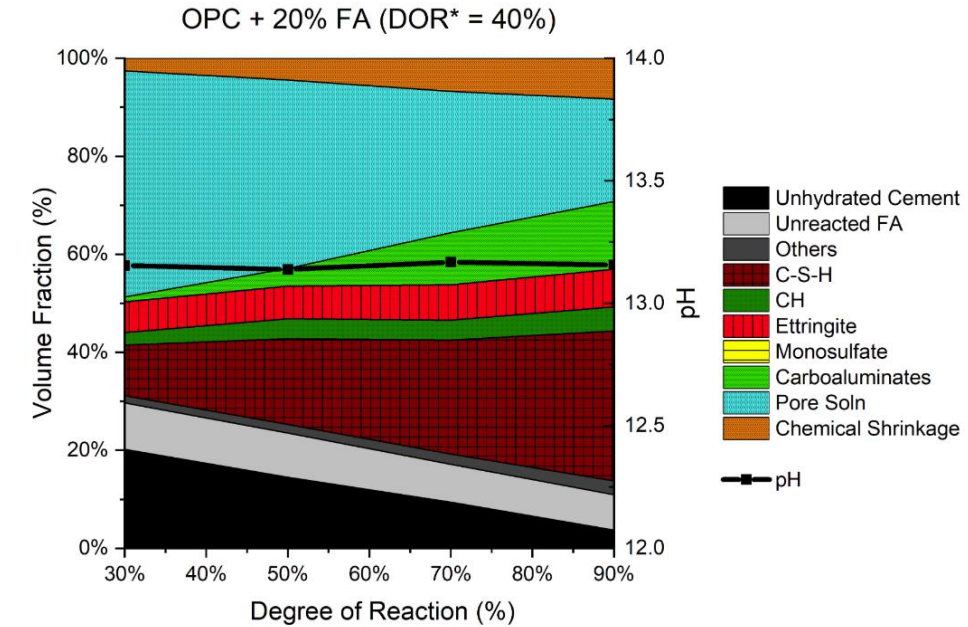
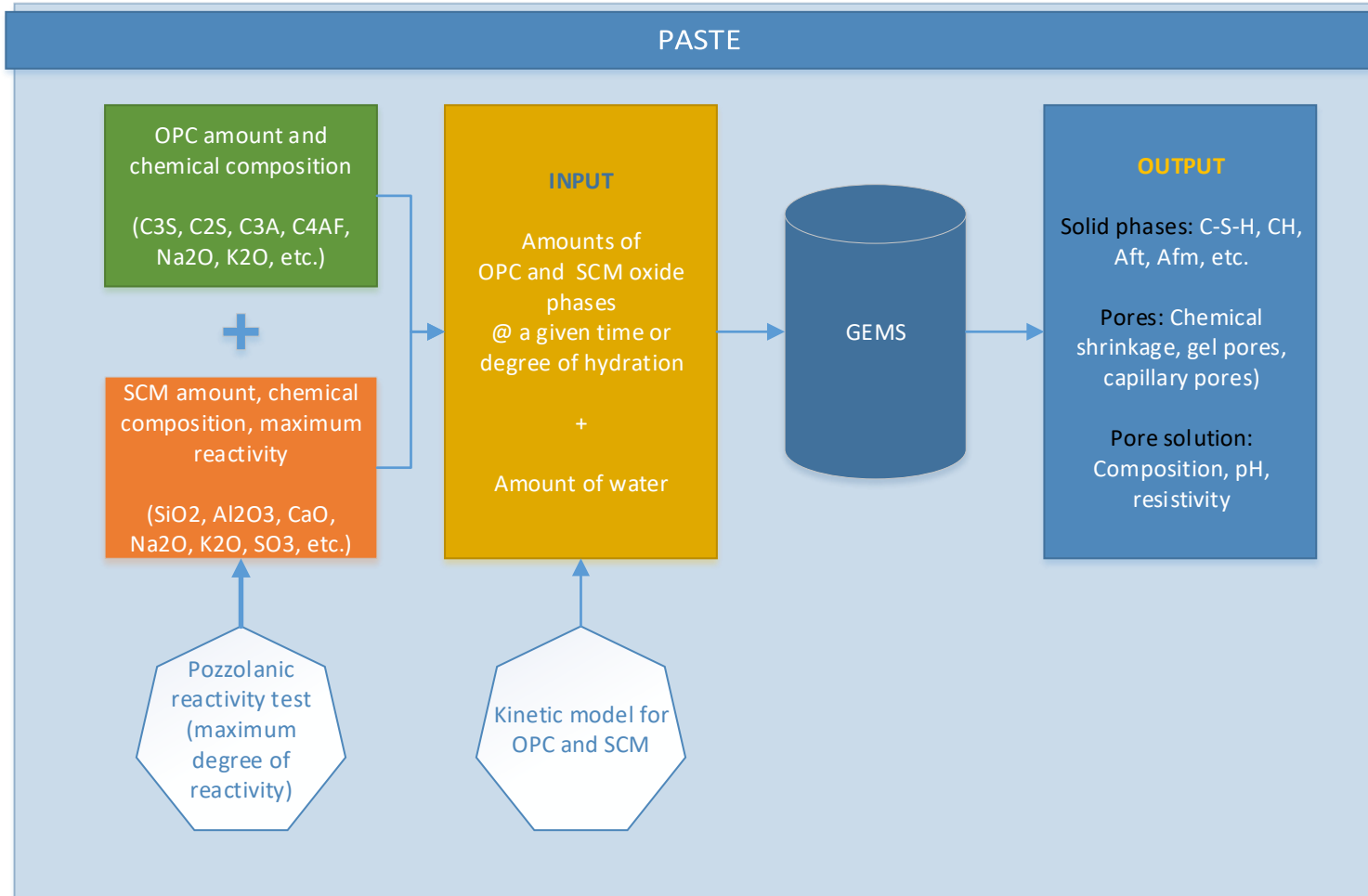
AFt1, AFt2, etc.

110 g pore solution

Ca<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>, etc.

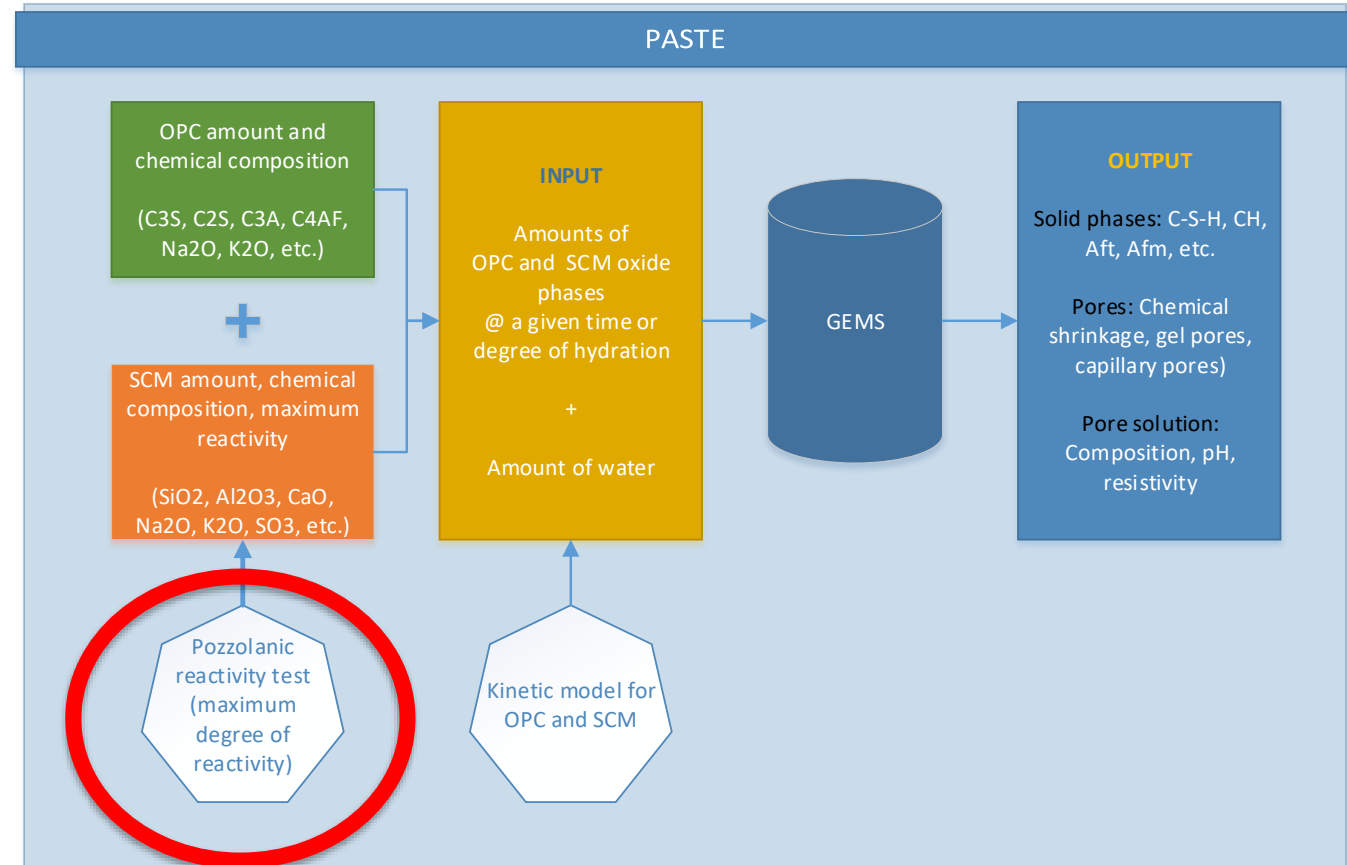
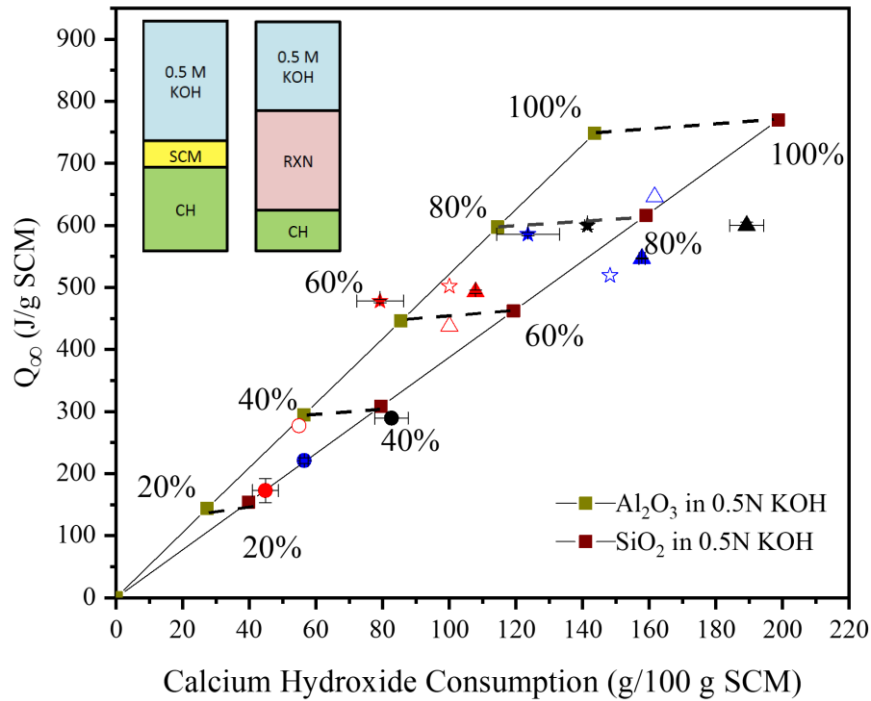
1,400 g

# Kinetic/thermodynamic modeling



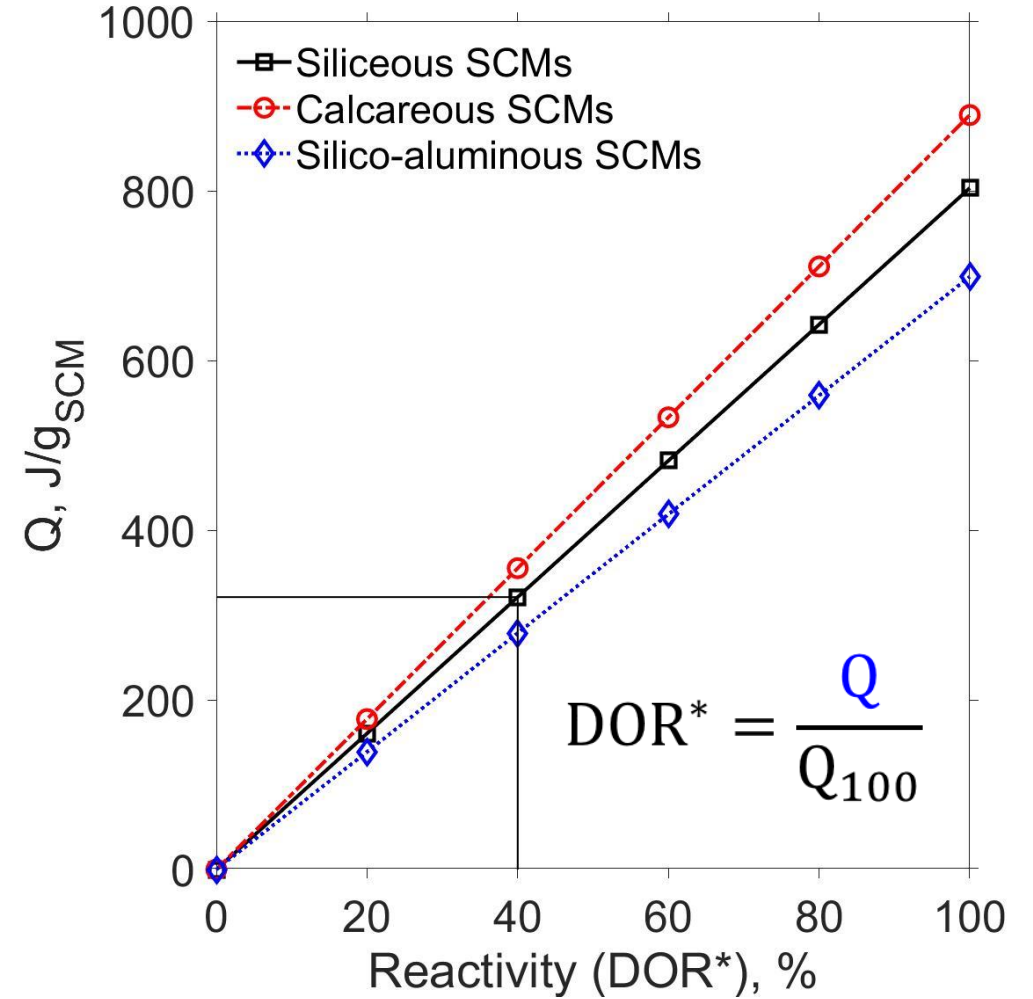
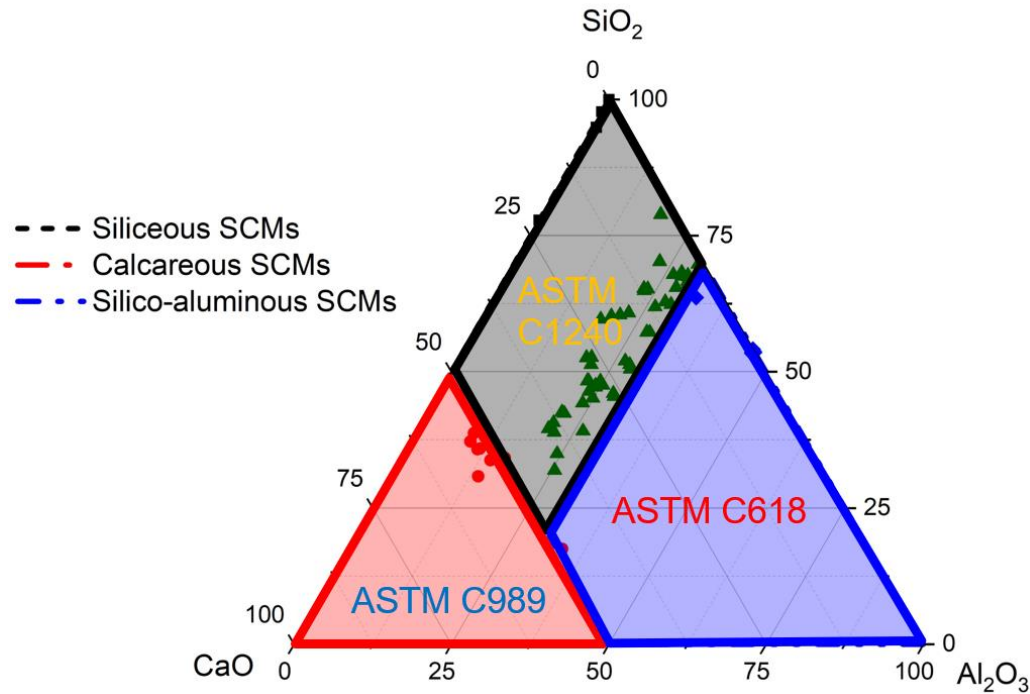
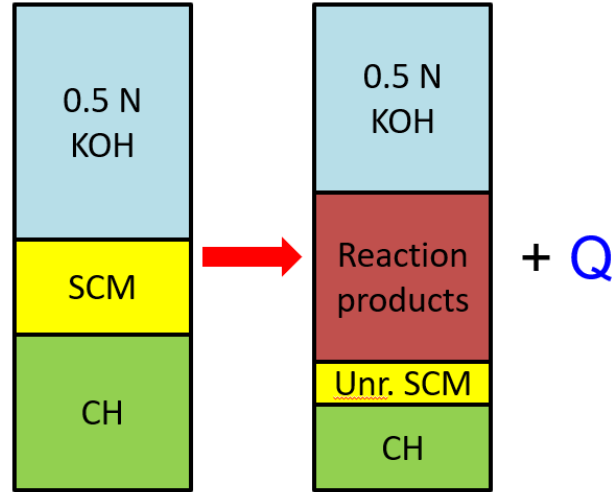
(Simulation by K. Bharadwaj)

# Reactivity

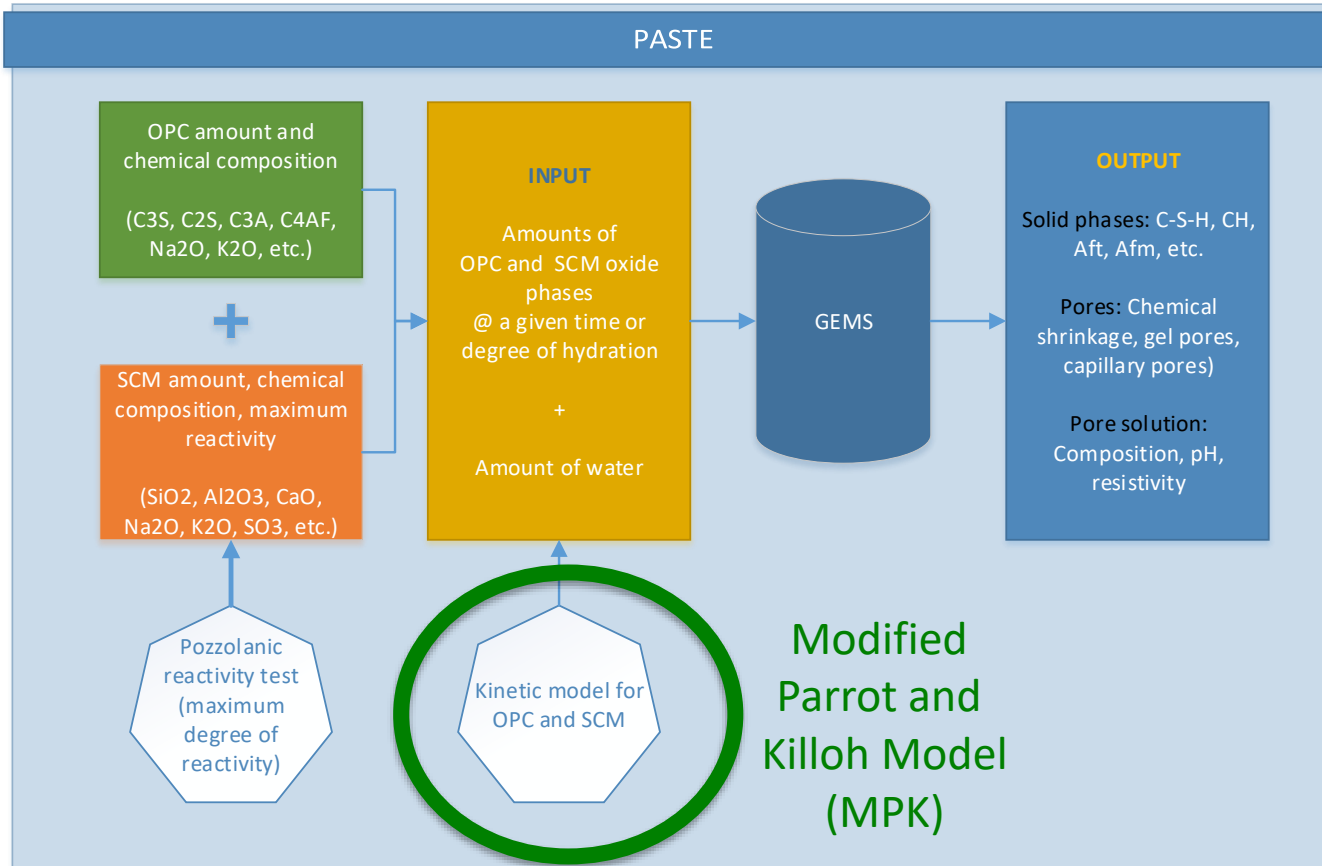


Pozzolanic Reactivity Test (PRT)

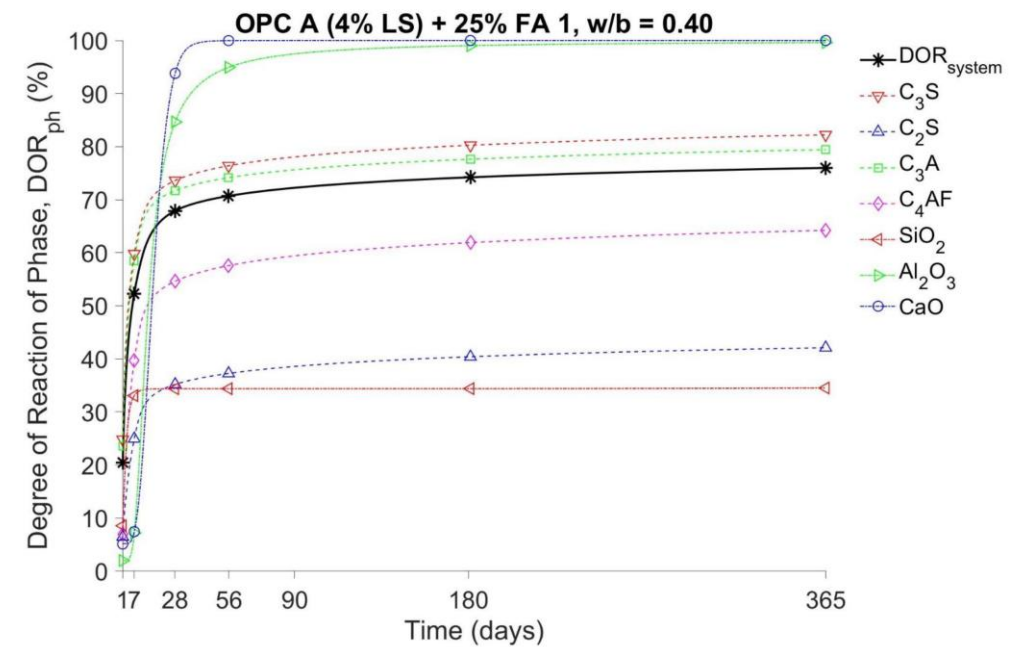
Glosser et al. 2019, 2020, 2021



Bharadwaj et al. 2022

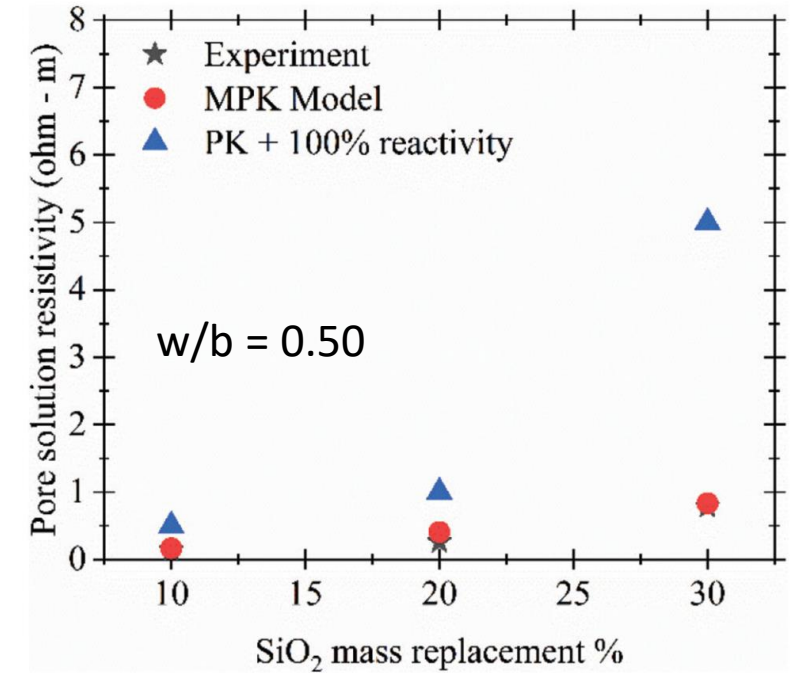
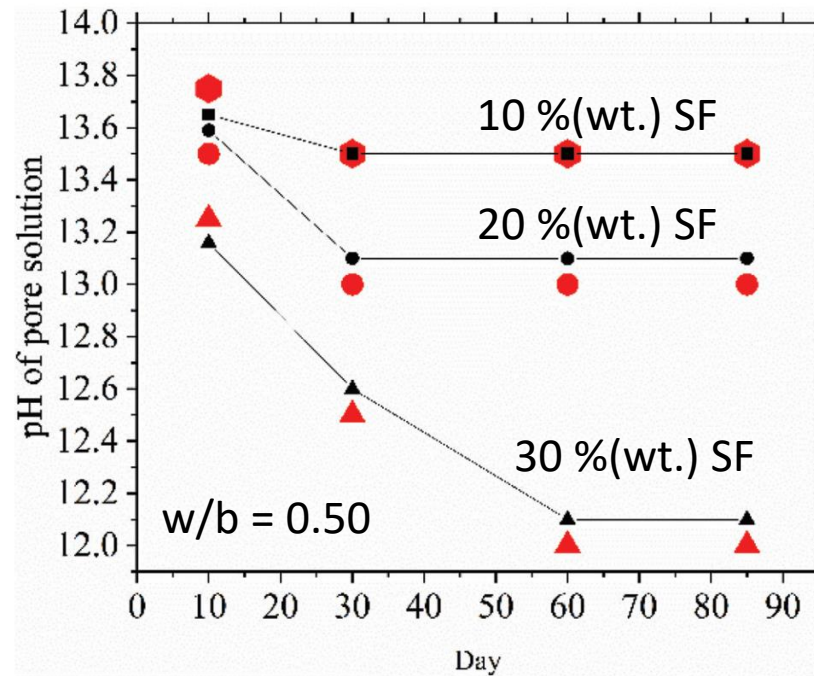
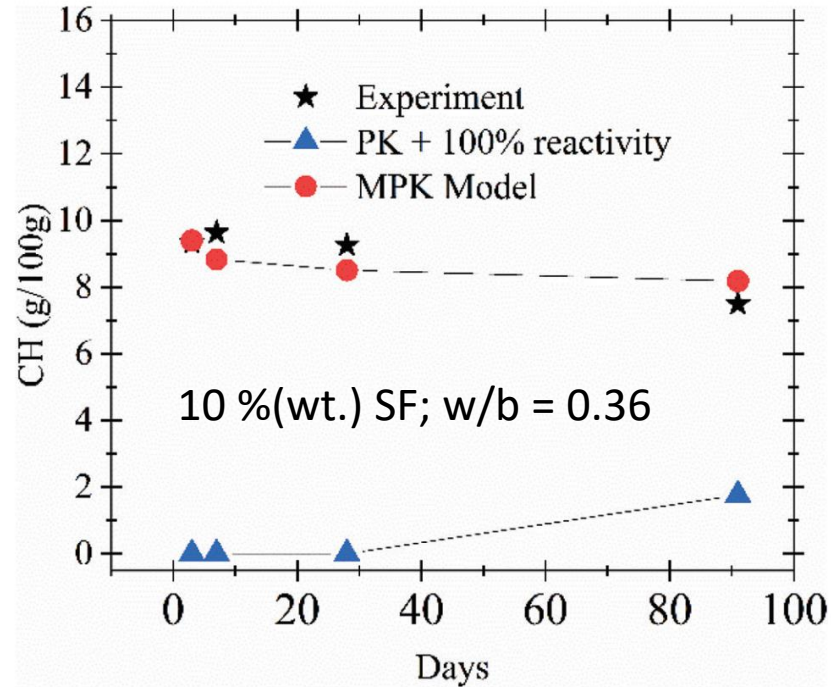


Glosser et al. 2019, 2020, 2021



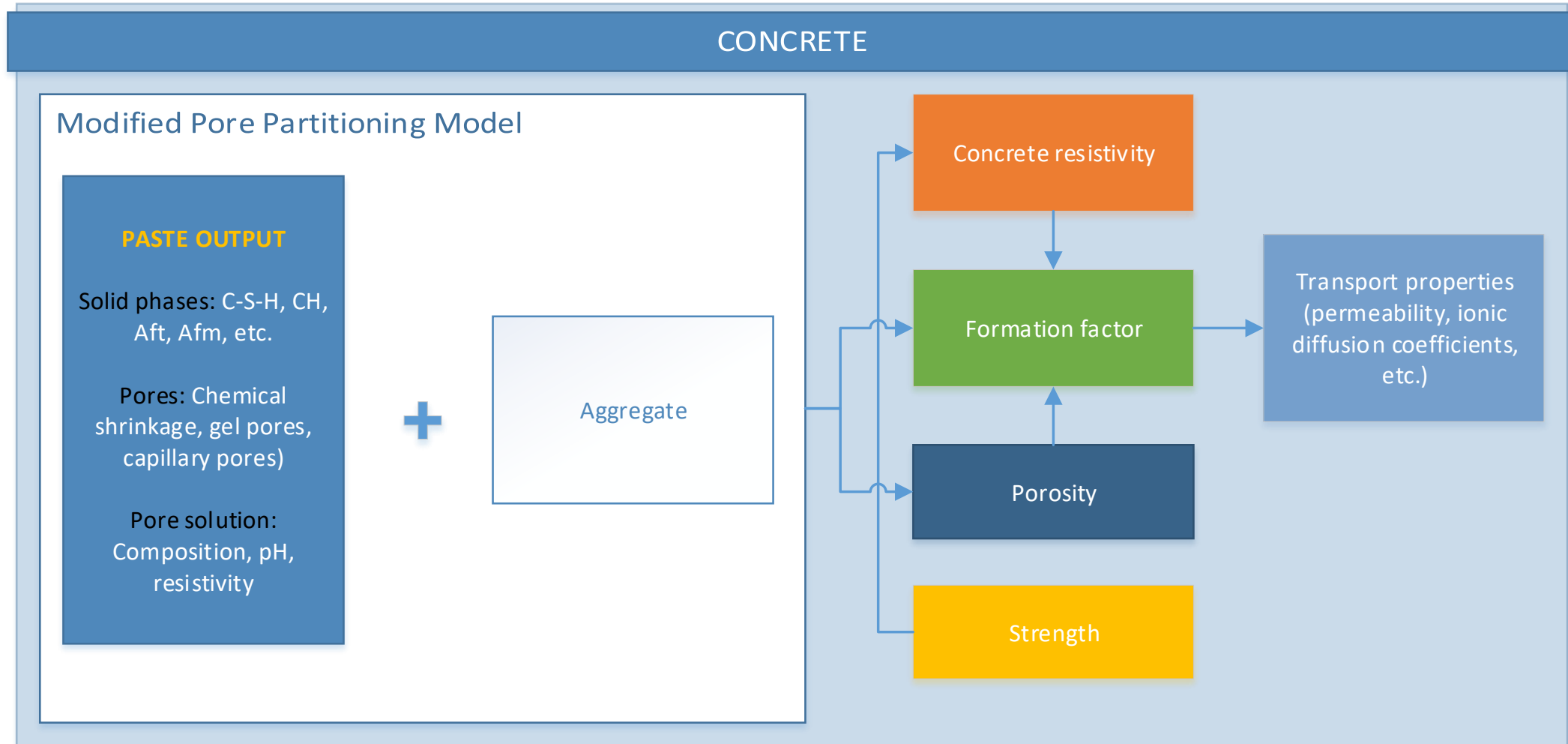


## OPC + Silica fume



Glosser et al. (2020) "Non-Equilibrium Thermodynamic Modeling Framework for Ordinary Portland Cement/Supplementary Cementitious Material Systems," ACI Mat. J., 117(6): 111-123

# Modified Pore Partitioning Model for Concrete



Bharadwaj et al. 2019, 2020

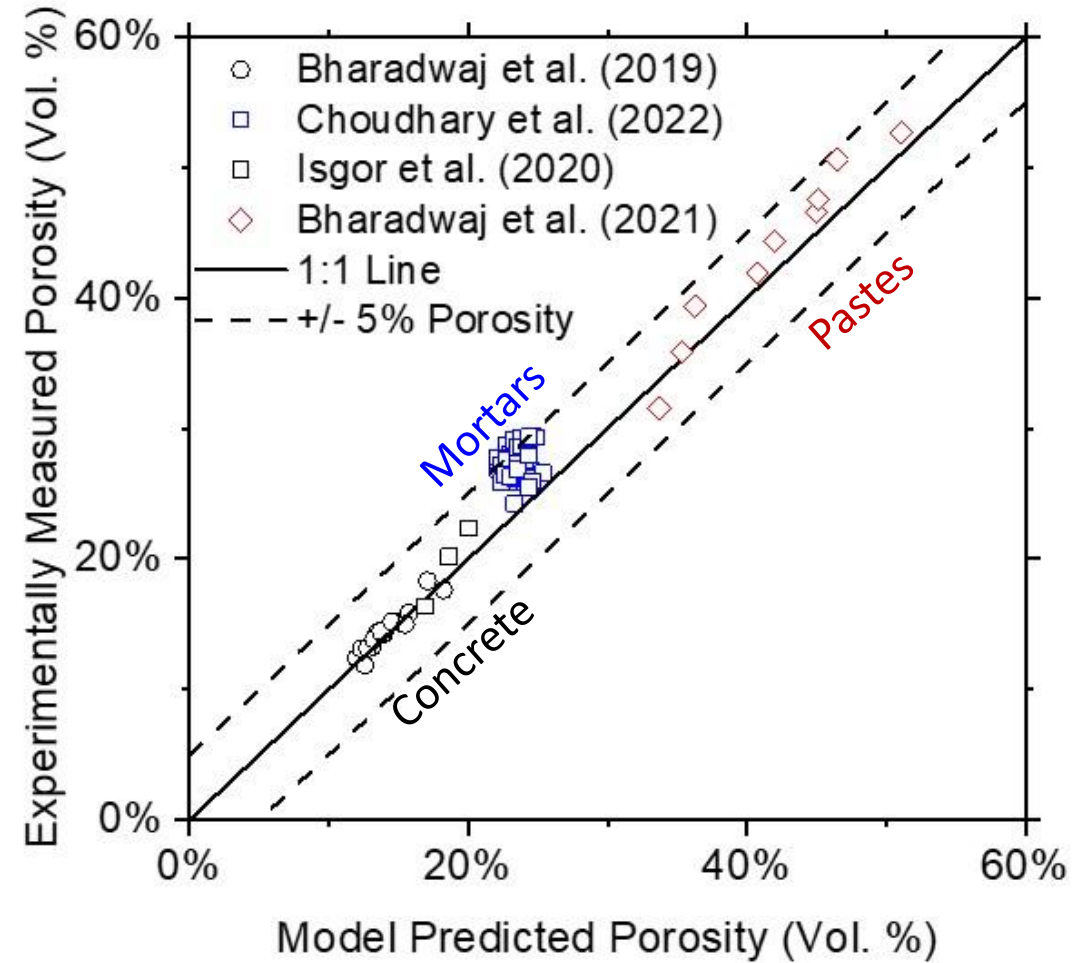
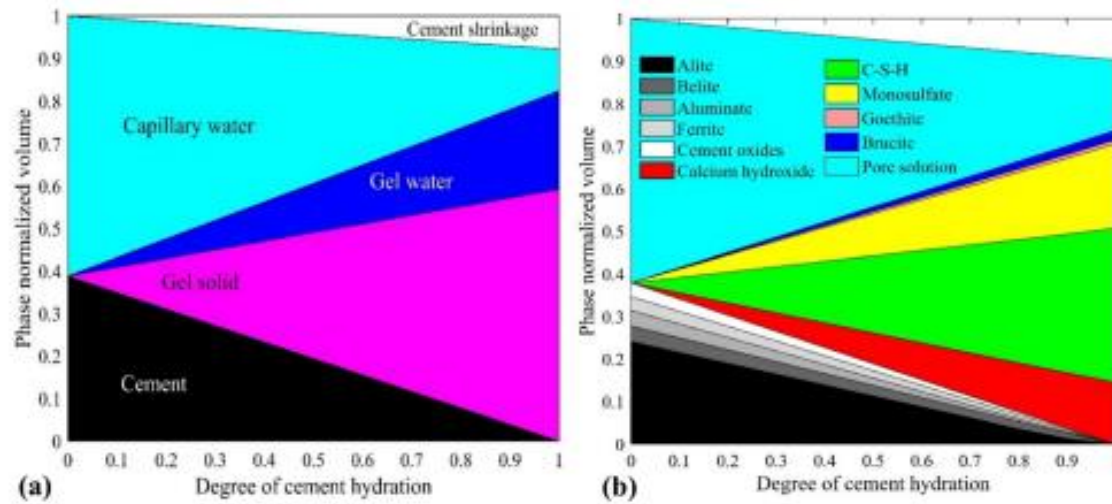
# MPPM - Porosity



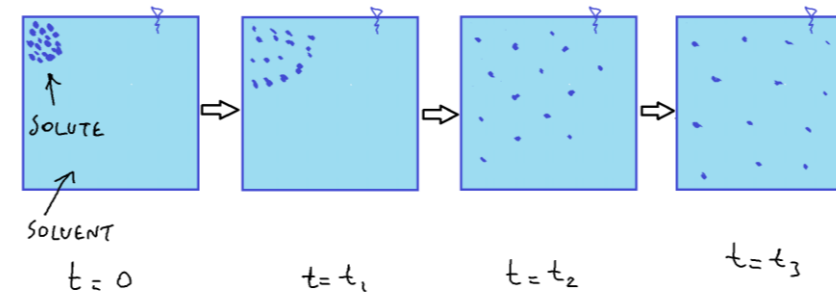
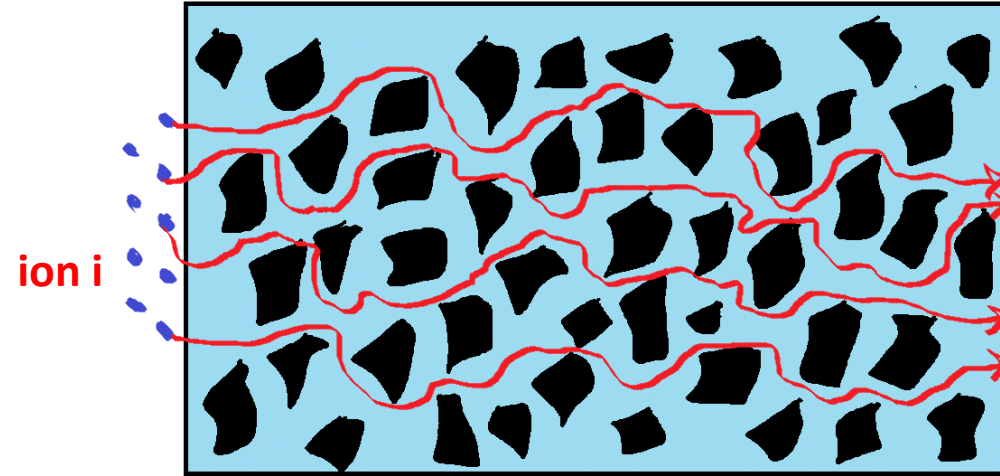
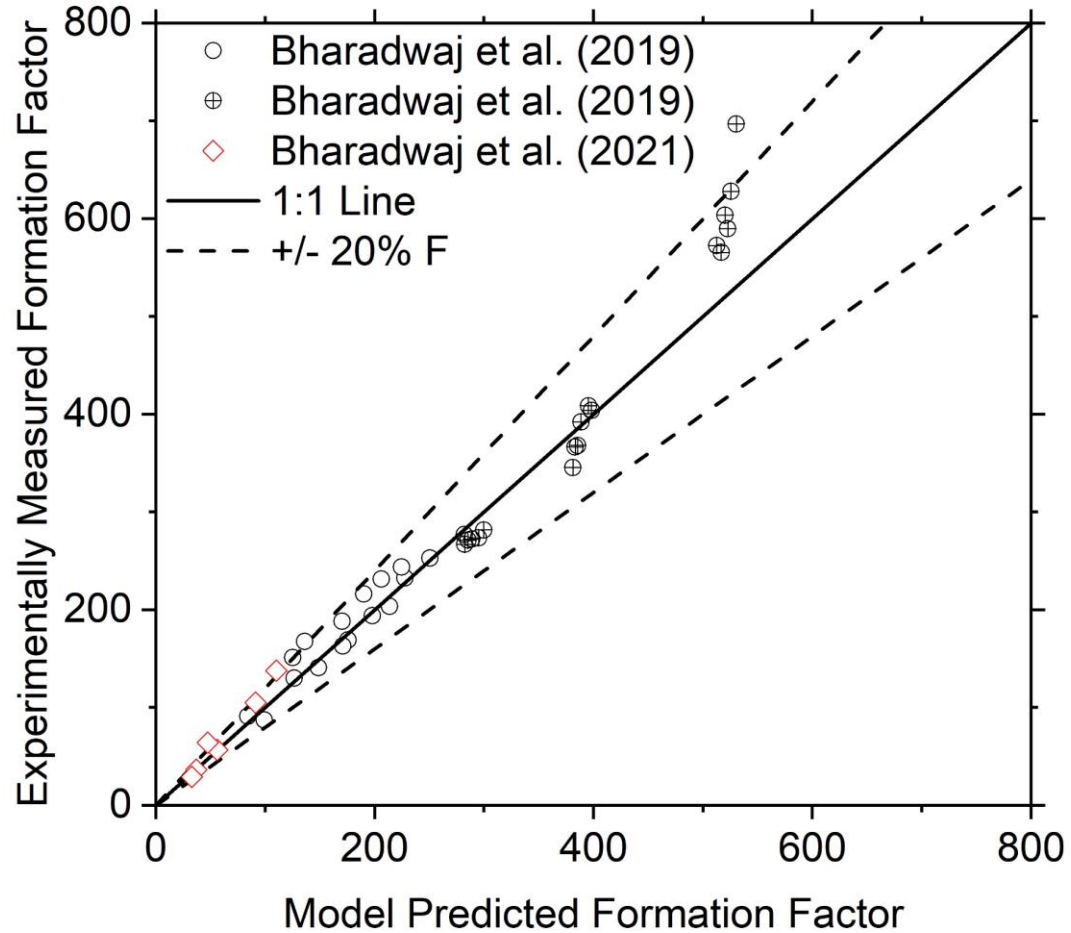
$$\phi_{paste} = V_{air} + (v_{gw} + v_{cw} + v_{cs}) \cdot V_{paste}$$



From GEMS and Powers Model

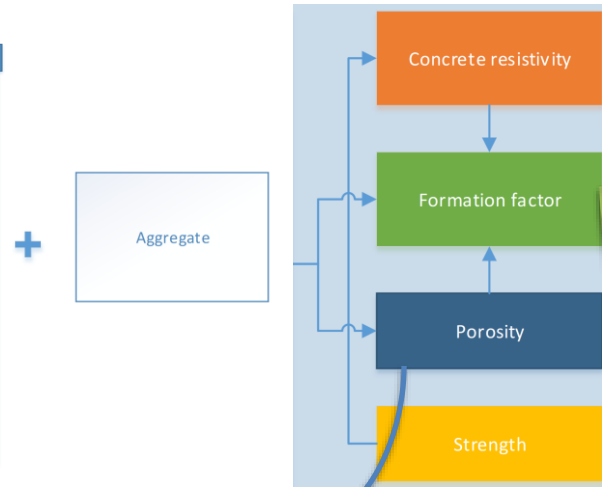
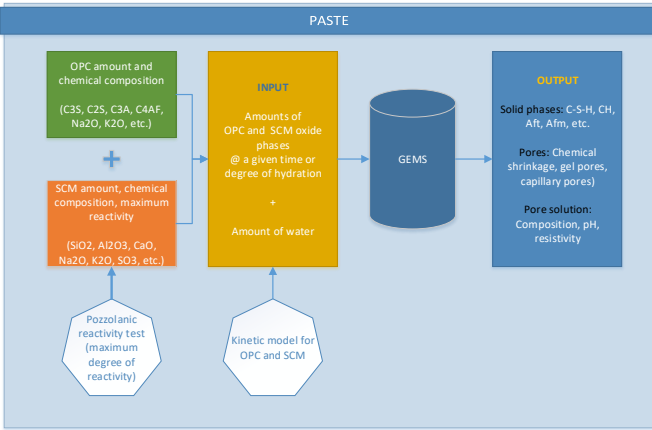
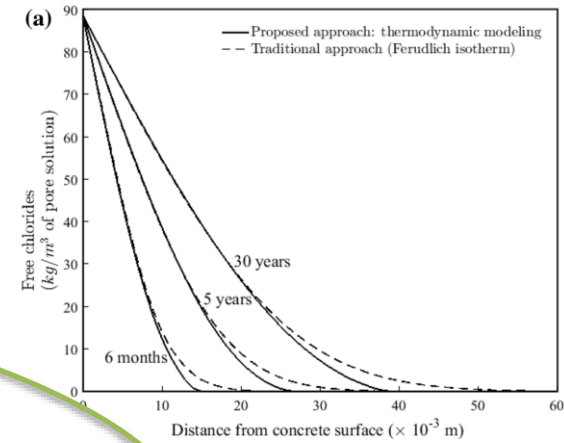


# MPPM - Formation Factor



$$D_{i,concrete} = \frac{D_i}{F}$$

# Summary

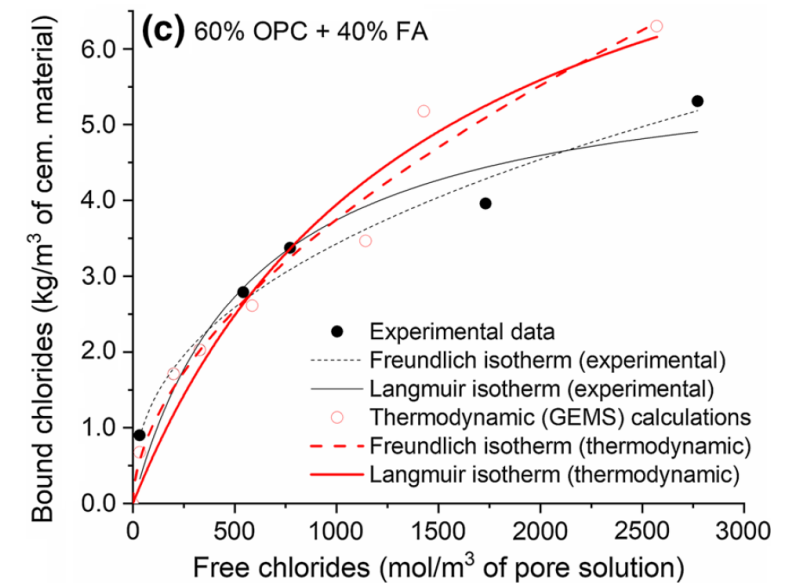
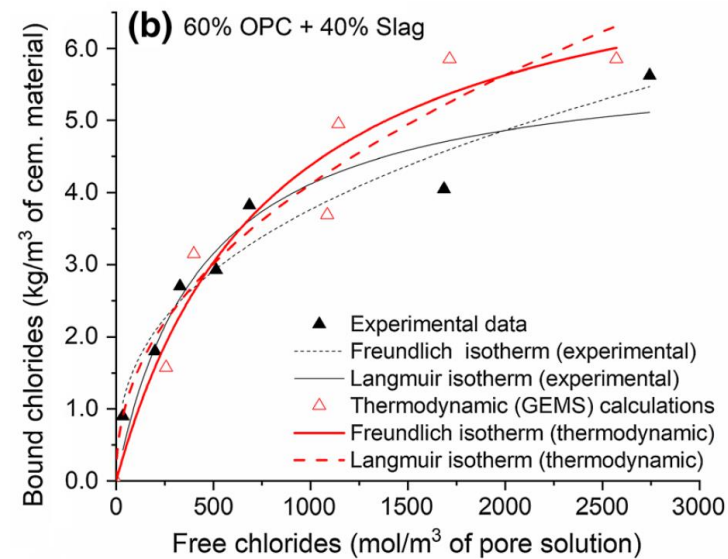
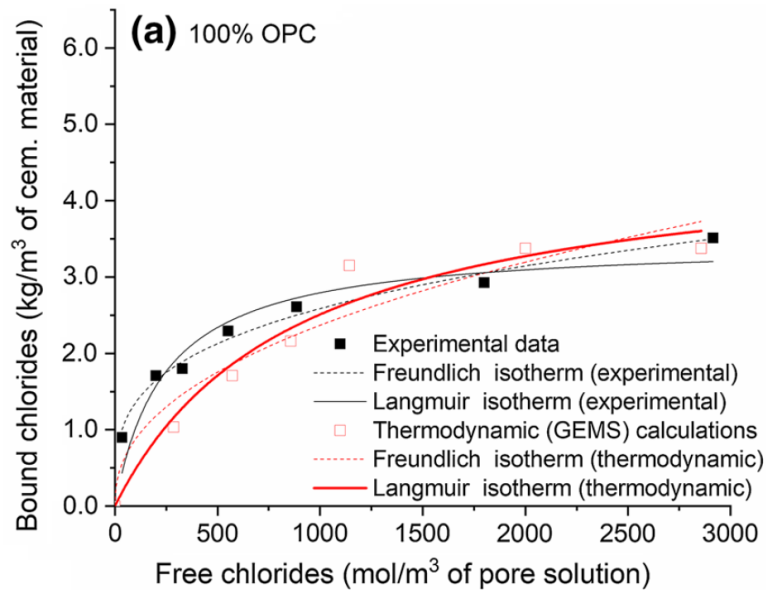


$$\frac{\partial[\varphi c_{aq,i}]}{\partial t} \frac{\partial c_{s,i}}{\partial t} = - \sum_{n_i} \nabla \cdot \left( \underbrace{-D_i \nabla c_{aq,i}}_{\text{diffusion}} - \underbrace{D_i c_{aq,i} \frac{Fz}{RT} \nabla \phi}_{\text{electrical migration}} - \underbrace{D_i c_{aq,i} \nabla \ln \gamma_i}_{\text{chemical activity}} \right)$$

# Validation



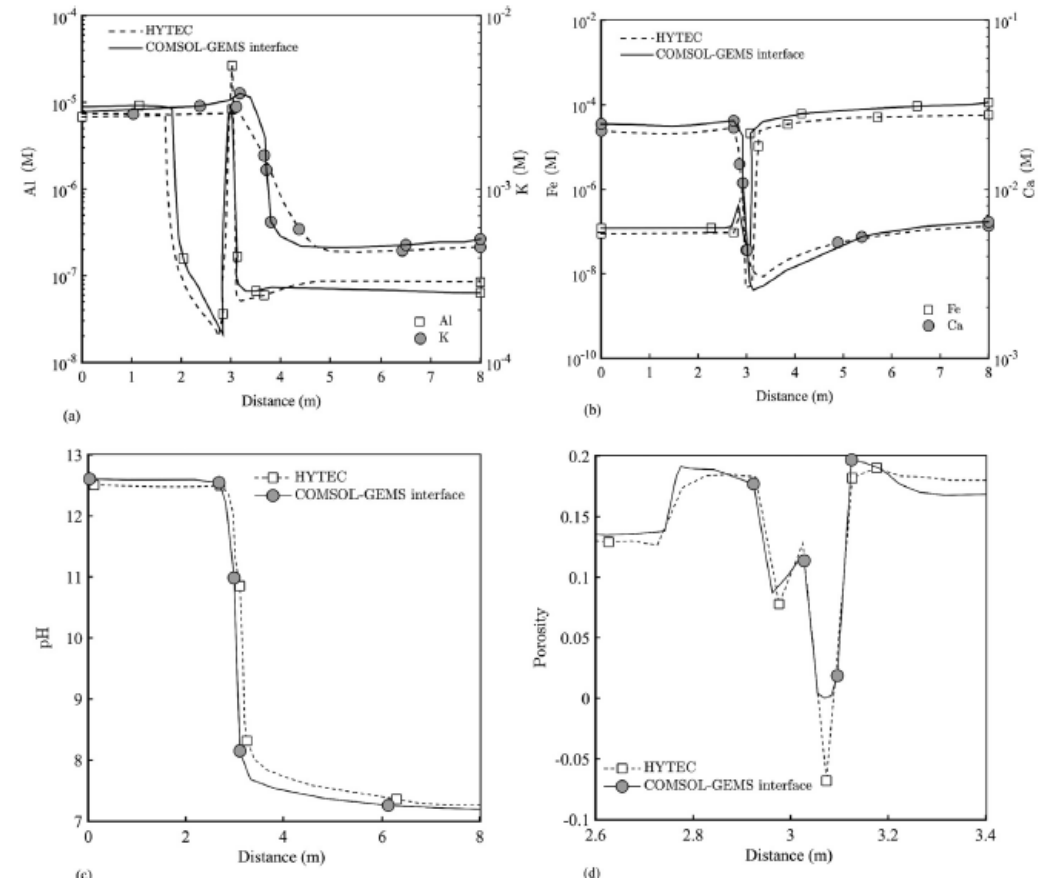
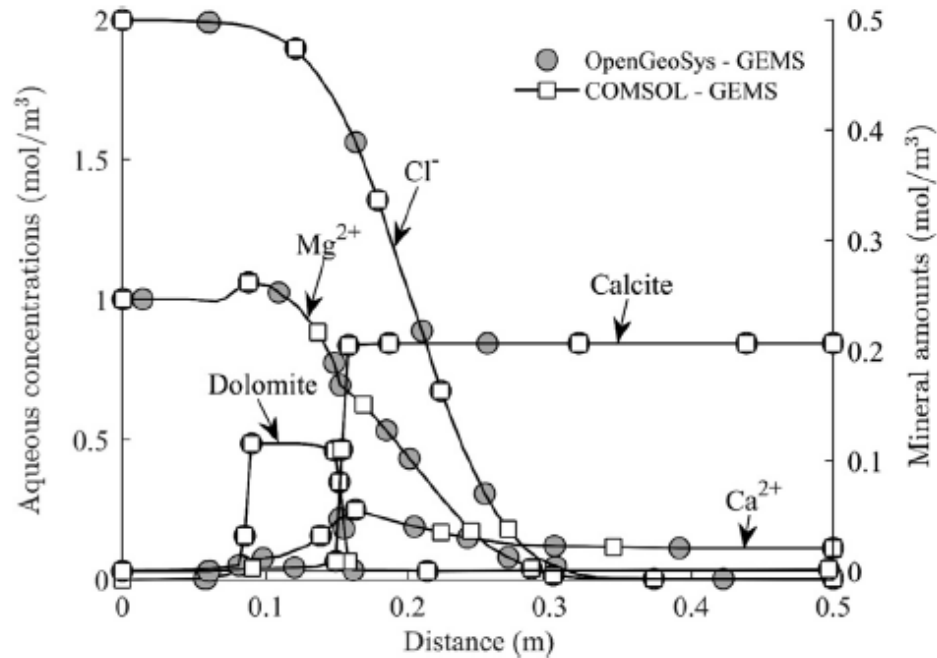
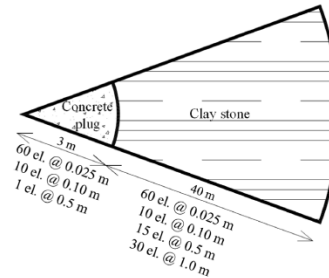
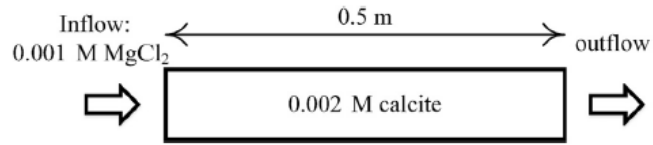
## Thermodynamically calculated chloride binding isotherms:



(Isgor and Weiss, Materials and Structures, 2019)

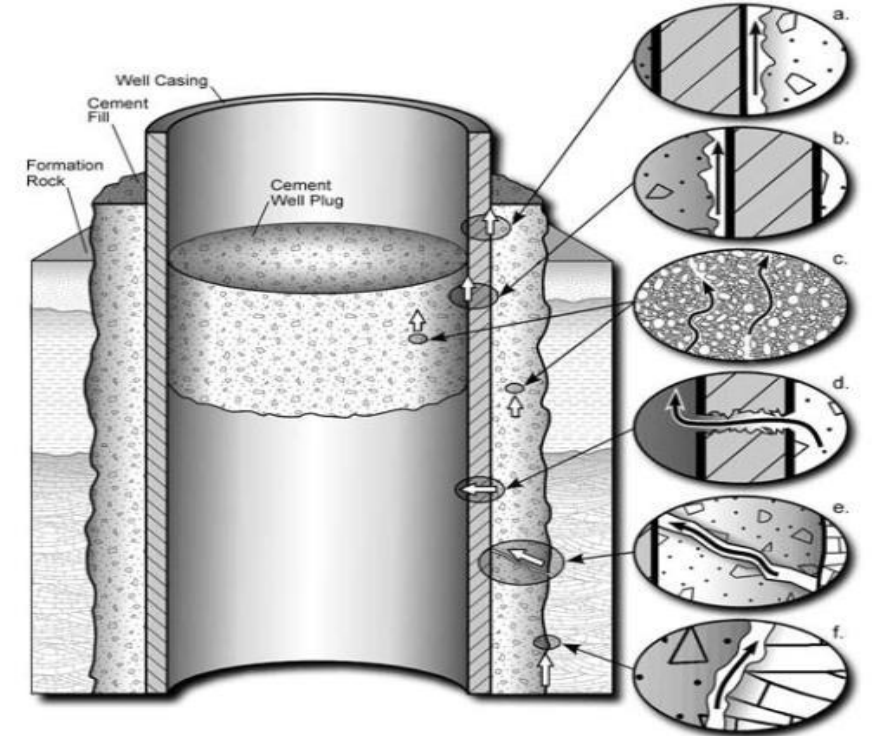
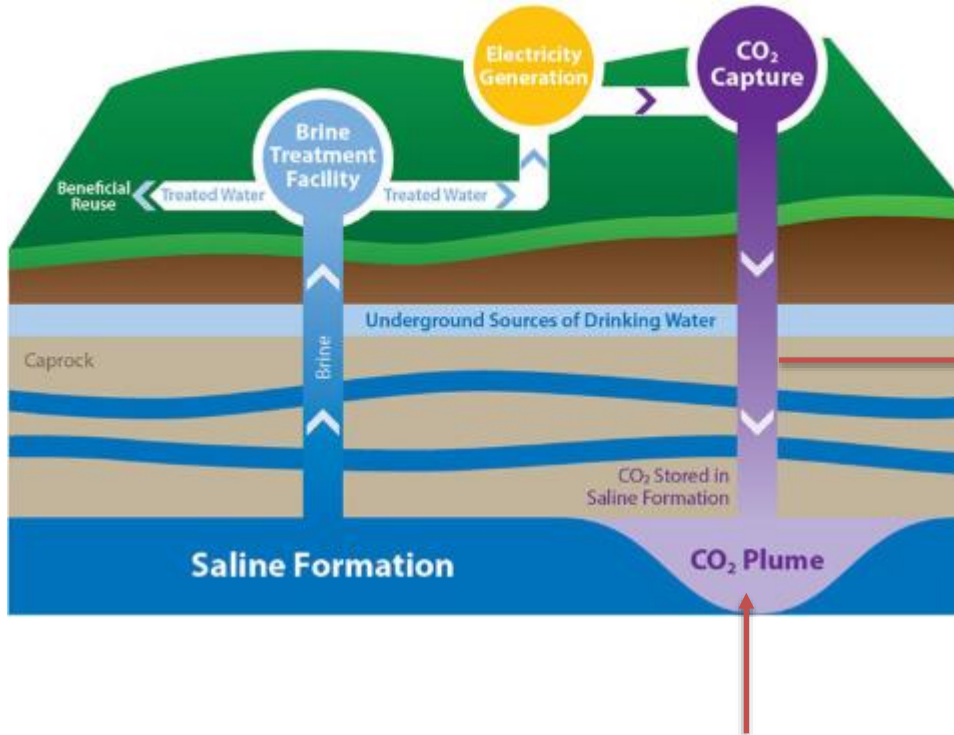
(Azad et al., Computer & Geosciences, 2016)

# Validation / benchmarking



Azad et al., Computer & Geosciences, 2016

# An application

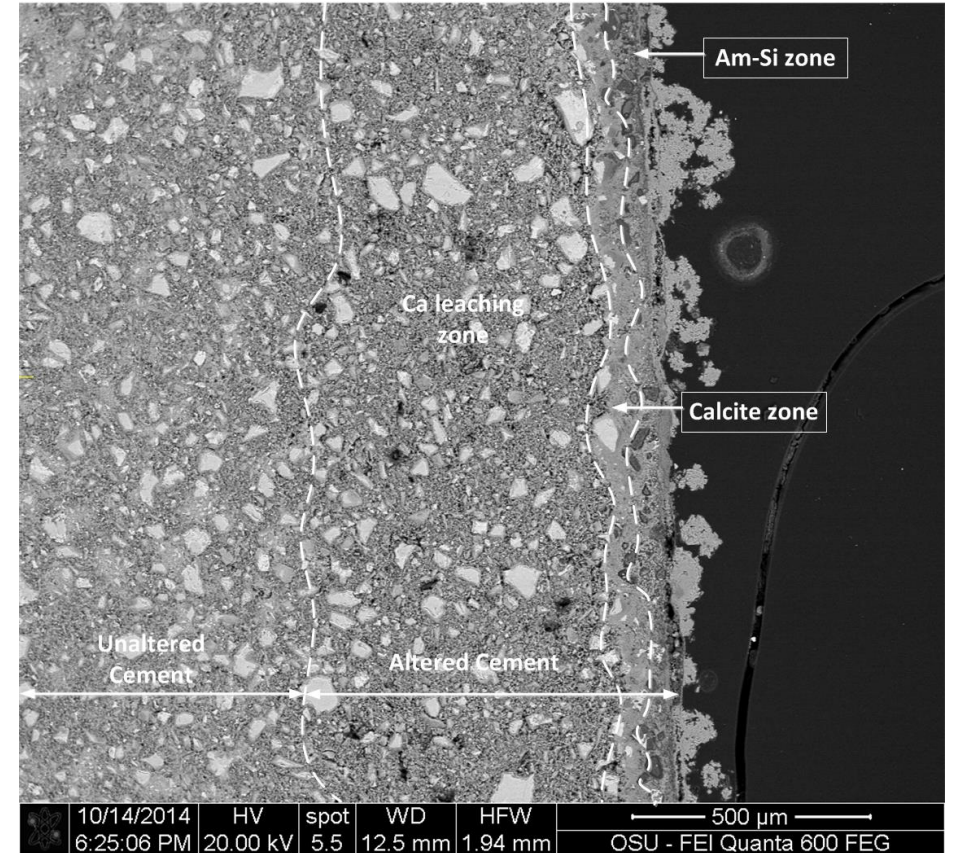
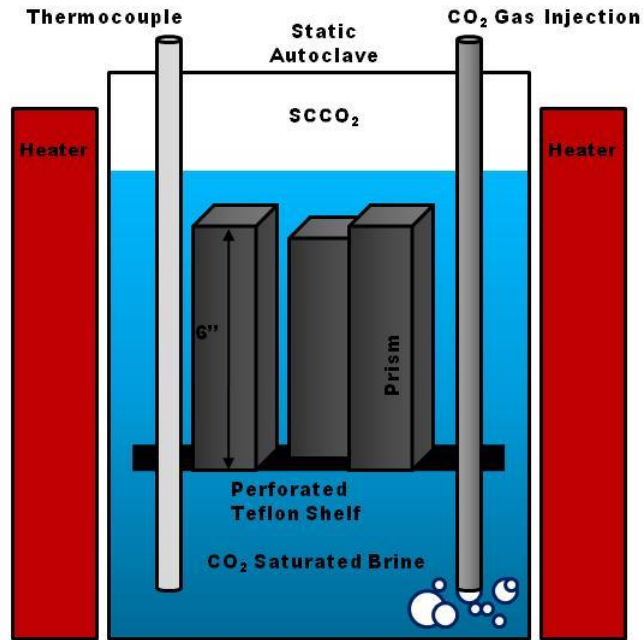


High temperature (85°C), high pressure (14.7 psi),  
supercritical CO<sub>2</sub>, complex brine chemistry

Source: NETL



# An application

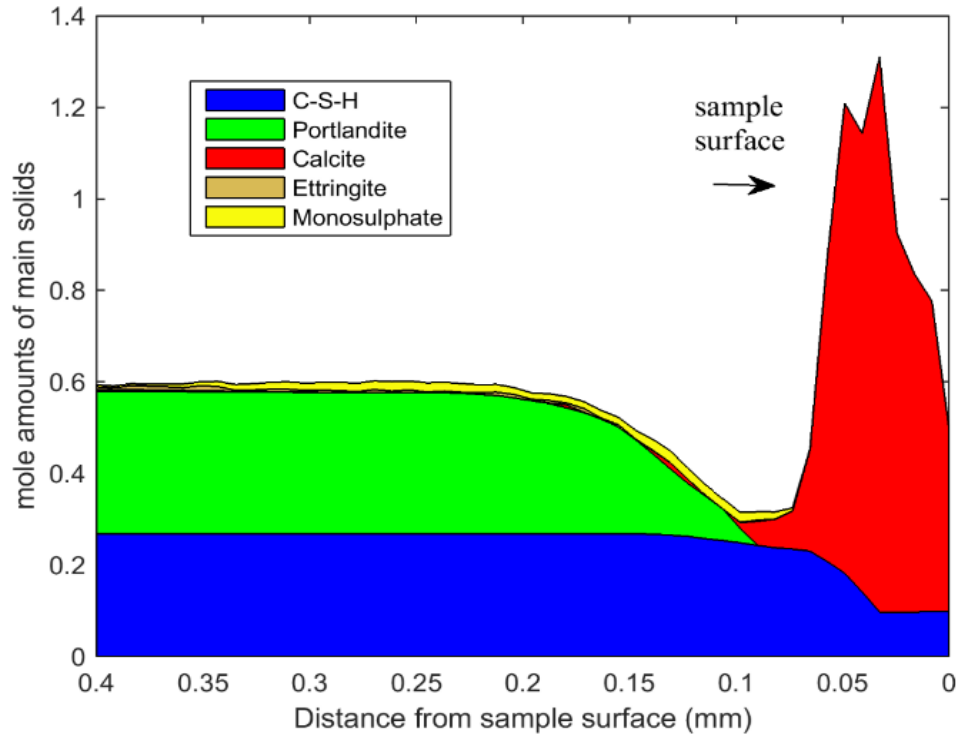


Ideker, Isgor, et. al. (2014)

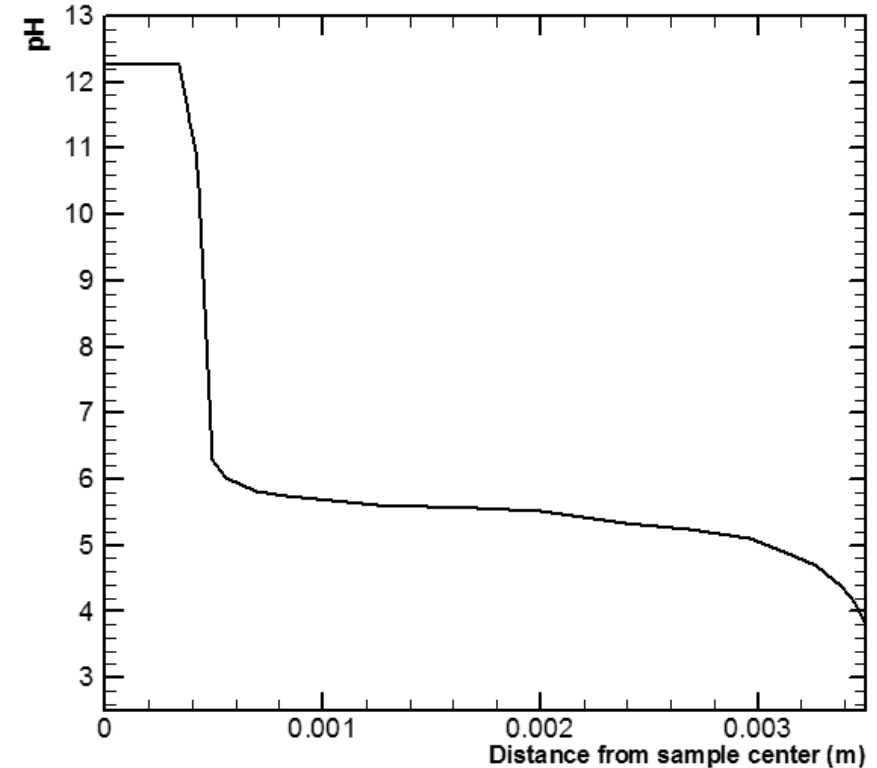
# An application



At 42 days

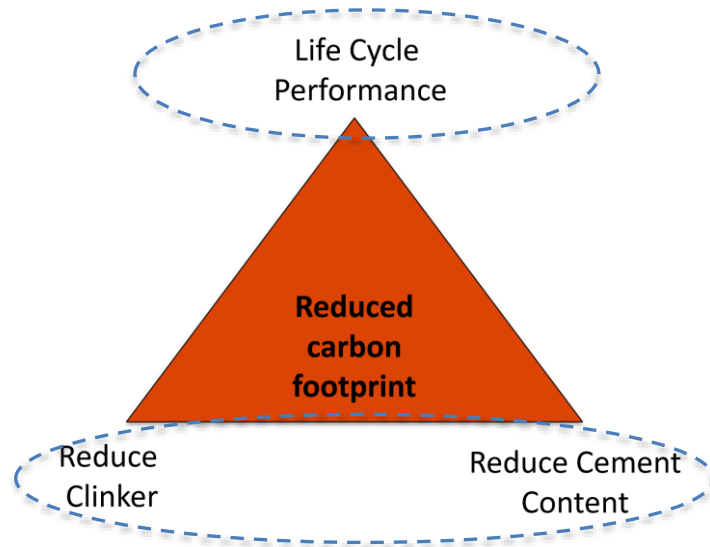


~1000 years to achieve ~1 m of deterioration



Corrosion of the casing and the leakage through cement-plug/steel interface is the main concern

# Conclusion



**Increase the use of low-carbon footprint cementitious materials and powder extenders**

- Modeling reactive transport processes in concrete for predicting service life is possible irrespective of
  - Chemical composition of the materials
  - Reactivity of the materials
- We can do this using a coupled approach in which we model **reactive processes** using thermodynamic / kinetic algorithms and **transport processes** using finite element analysis.
- This approach eliminates the need to experimentally characterize every concrete mixture for modeling, hence it is dubbed “self-sufficient”.
- This approach allows the modeling of concrete produced with underutilized, novel, low-carbon footprint binders and powder extenders.

# Thank you



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