Struc'tur'al

Load Testing After Strengthening Of A Prestressed Double Tee Beam That Had Failed In Shear

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Introduction

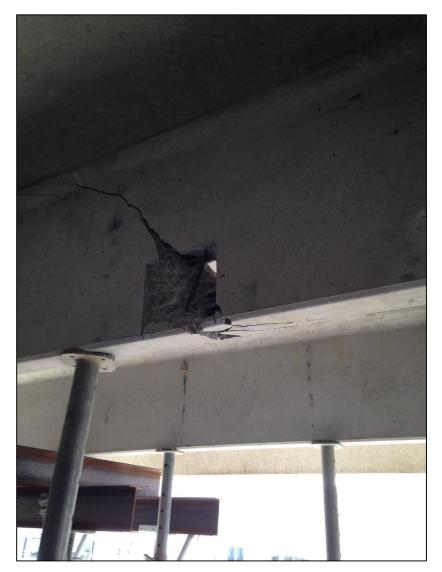
- Fountain Square Garage is located at the Reston Town Center in Reston, Virginia.
- The roof floor framing consists of precast, pre-stressed concrete double tees (DT) supported by precast concrete girders and columns.
- Following a heavy snow storm, a landscape contractor had piled up all the snow on the roof on two DT beams showing signs of imminent shear failure.







Existing Conditions





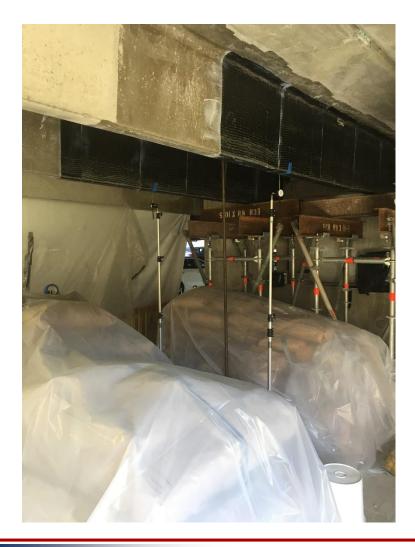




FRP Strengthening Details

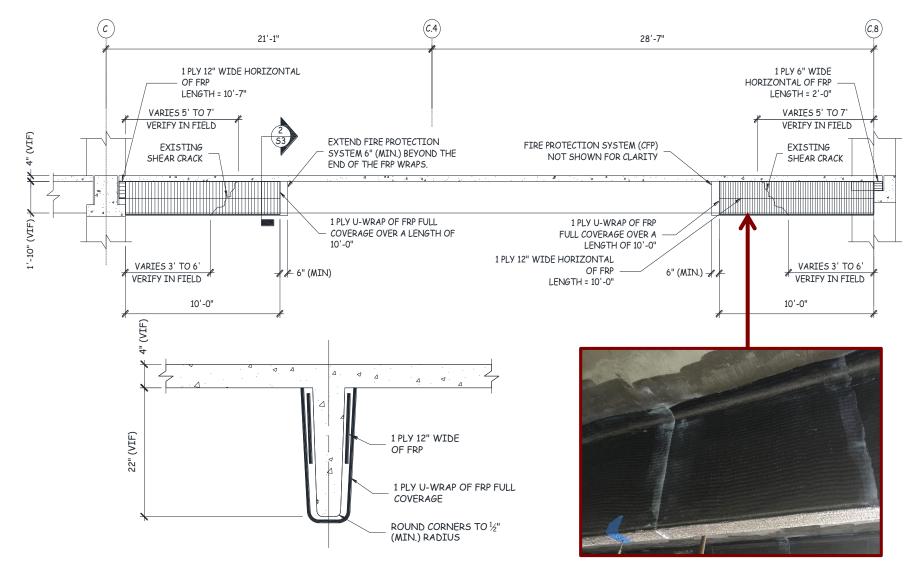
Strengthening procedure:

- 1. Restore structural integrity of the DT beams (epoxy injection/form and pump delaminated concrete)
- 2. Strengthen damaged DT beams with FRP U-Wrap designed as RC member (PT contribution considered as zero)





FRP Strengthening Details



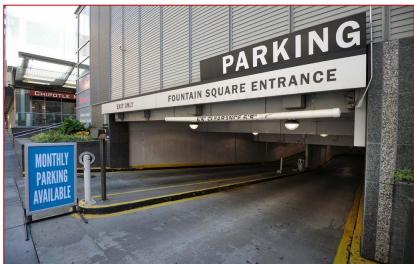


Testing Objectives

- Load testing was performed on the most damaged DT beam after FRP was installed.
- The objective of the load test was to confirm the shear capacity of the repaired DT beam.









Load Test Strengthening Beams

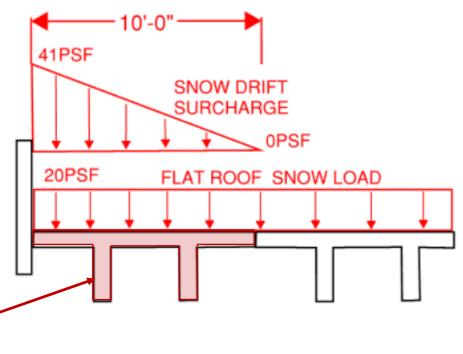
- The load test was designed to verify the shear performance of the repaired zone.
- All Loading was achieved using hydraulic jacks. Hydraulic jacks can remove the load quickly in the event of failure.
- Steel spreader beams and wood bearing pads used to transfer load to DT stems.





Loading on the structure

- Self-weight of the structure;
- Snow load consisting of a flat snow load of 20 psf and snow drift supercharge having a triangular distribution over a width of 10 ft and maximum value of 41 psf;
- Live load of 40 psf (parking).





Failed DT Beam

Load Test Magnitude

- ACI 437.2 considers two sets equations when determining the load test magnitude.
 - 1. Statically indeterminate Eq. (4.2.2a) through (4.2.2c)

 $TLM = 1.3(D_W + D_S)$ (4.2.2a)

 $TLM = 1.0D_W + 1.1D_S + 1.6L + 0.5(L_r \text{ or } S \text{ or } R)$ (4.2.2b)

$$TLM = 1.0D_W + 1.1D_S + 1.6(L_r \text{ or } S \text{ or } R) + 1.0L$$
(4.2.2c)

2. Statically determined	
$TLM = 1.2(D_W + D_S)$	(4.2. <i>3a</i>)
$TLM = 1.0D_W + 1.1D_S + 1.4L + 0.4(L_r \text{ or } S \text{ or } R)$	(4.2.3b)
$TLM = 1.0D_W + 1.1D_S + 1.4(L_r \text{ or } S \text{ or } R) + 0.9L$	(4.2.3c)



Load Test Magnitude

 If the deficiency in statically determinate members is not tensioncontrolled, then Eq. (4.2.2a) through (4.2.2c) shall be used to determine the TLM".

$$TLM = 1.3(D_W + D_S)$$

$$TLM = 1.0D_W + 1.1D_S + 1.6L + 0.5(L_r \text{ or } S \text{ or } R)$$

$$(4.2.2a)$$

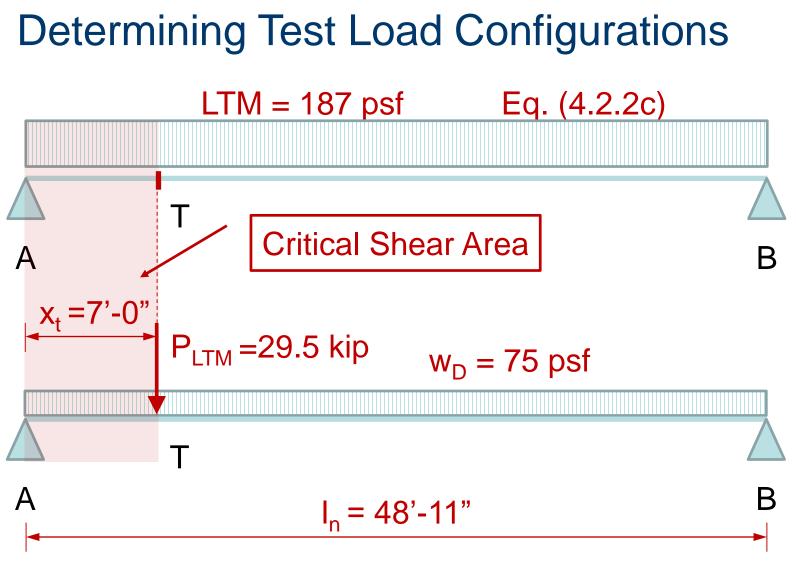
$$(4.2.2b)$$

$$TLM = 1.0D_W + 1.1D_S + 1.6(L_r \text{ or } S \text{ or } R) + 1.0L = 187 \text{ psf}$$

$$(4.2.2c)$$

When testing to evaluate shear strength, the moment in the section will influence the shear strength of the section. Therefore, it is important to arrange the testing load that duplicate the suspected shear deficiency.

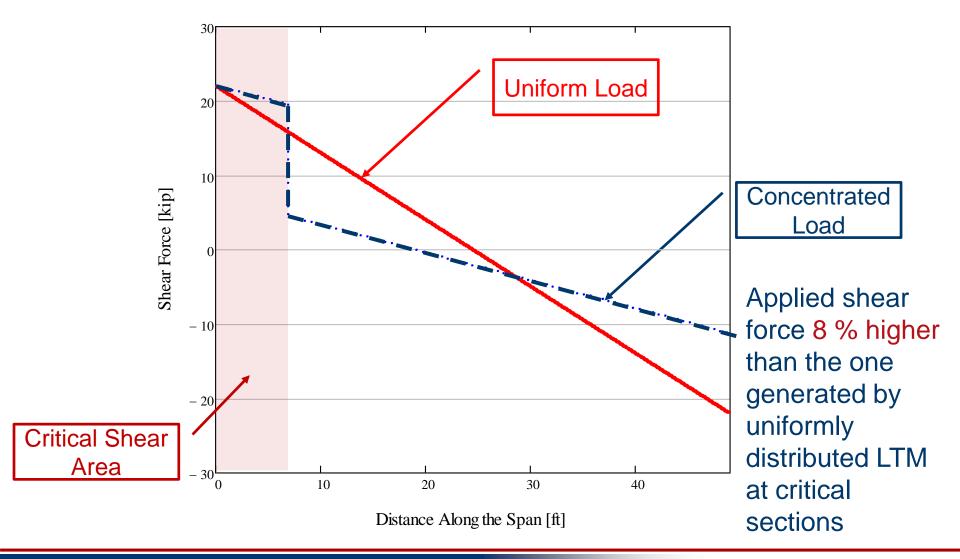




Equivalent Point Load

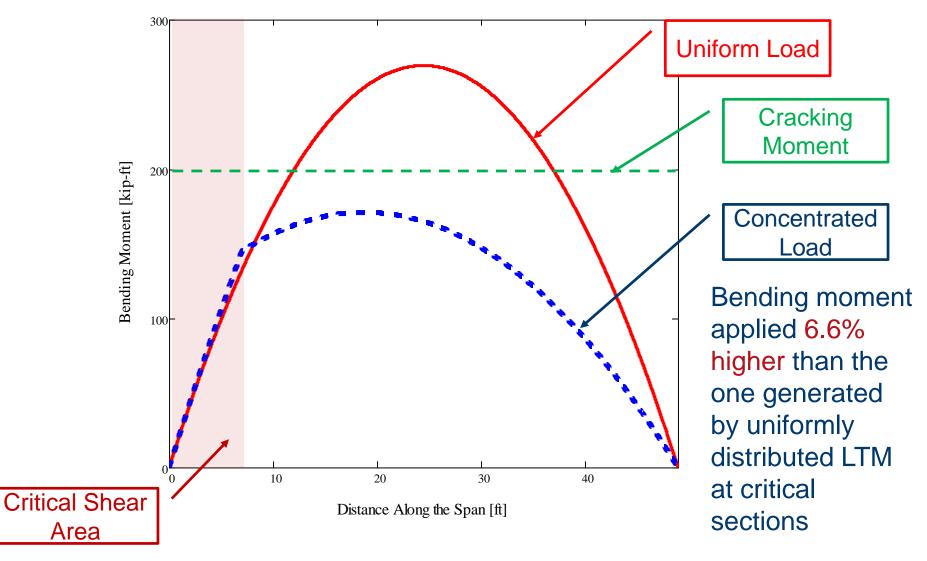


Shear Distribution LTM



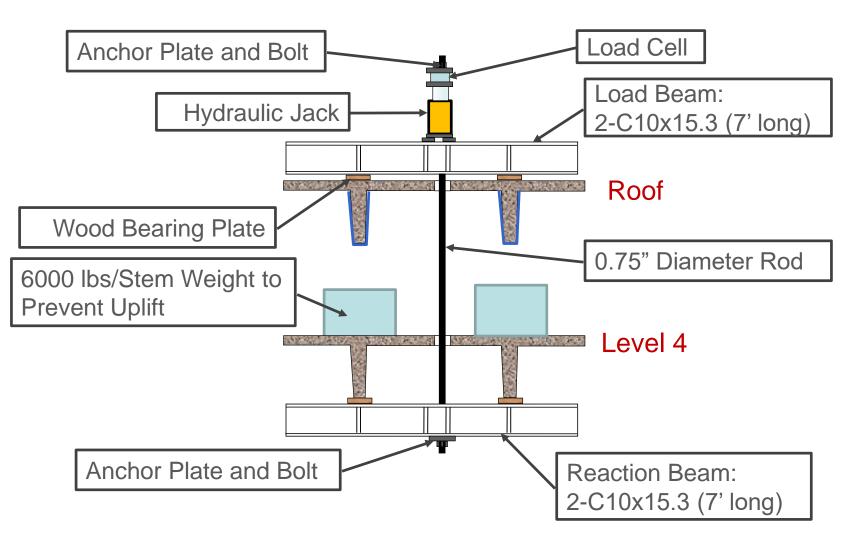


Moment Distribution LTM

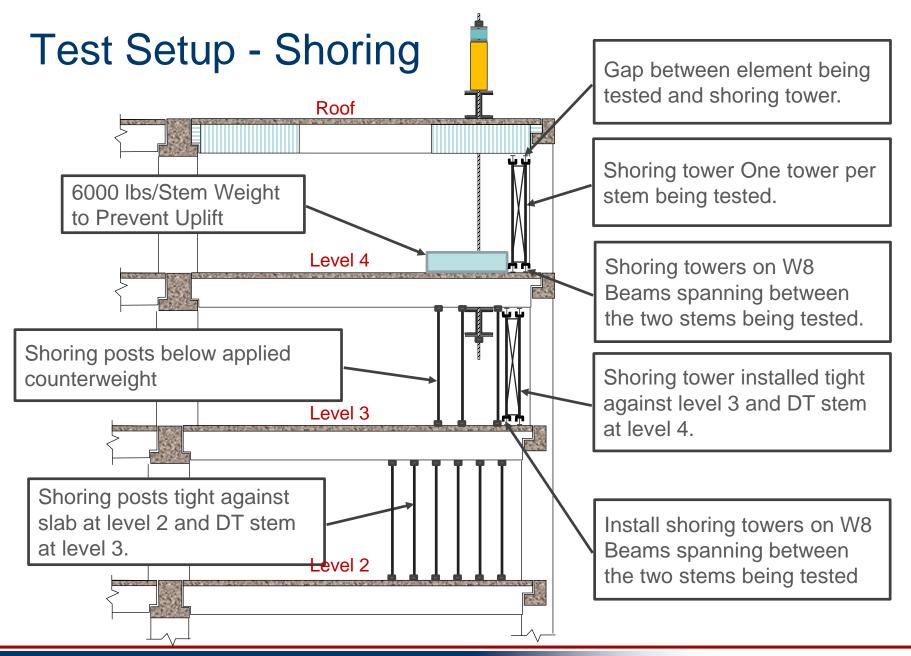




Load Test Set Up









Load Test Equipment



Load Cell and Jack



Steel Spreader Beam with High Strength Williams Bar



Data Acquisition Unit



Reaction Beam



Hydraulic Pump



Load Test Equipment



6000 lbs./Stem Weight to Prevent Uplift



3 TO 6 kip Capacity Shoring Posts

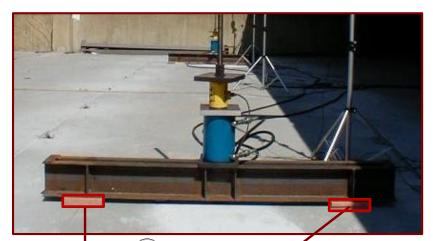


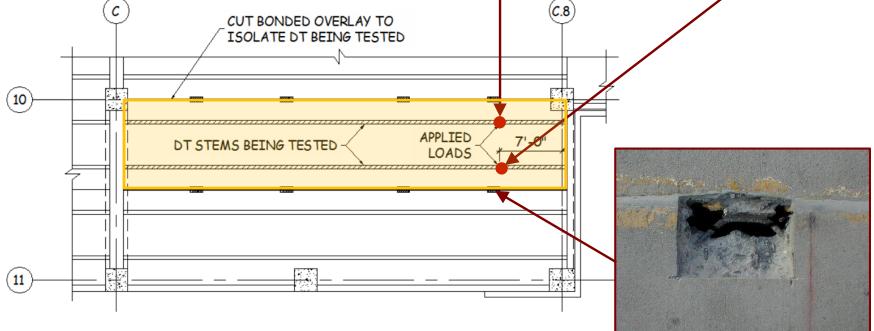
Dial Gages at Underside of DT Beams



Applied Loads

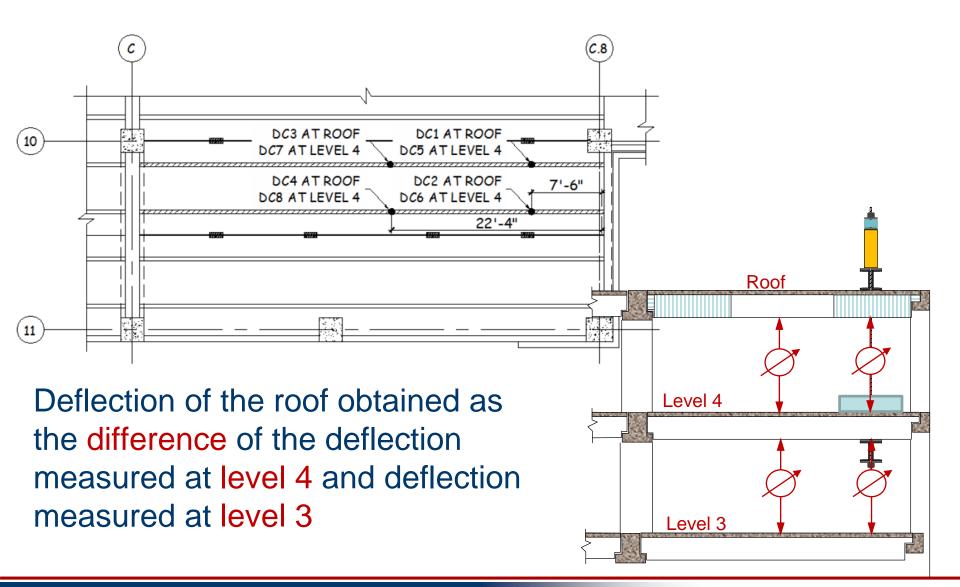
Tested DT beam was disconnected from the remaining structure







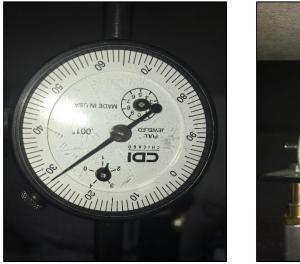
Deflection Measurements





Deflection Measurements



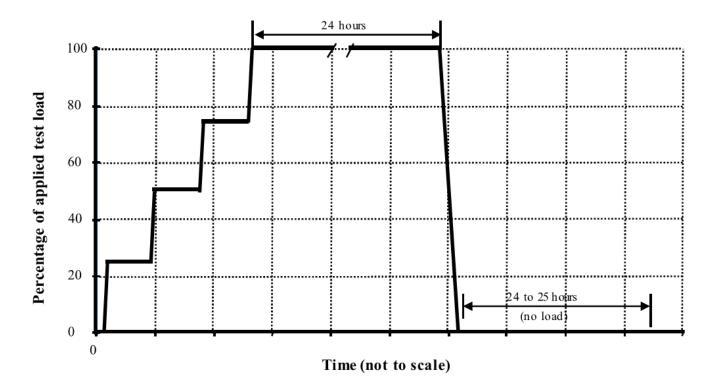




What is the maximum expected deflection? $\cong 0.2$ *in*. Dial gages with 0.001 in. resolution are adequate



Loading Protocol



Test Load shall be applied in not less than 4 approximately equal increments Test Load applied for 24h and final response within 24h test load has been removed

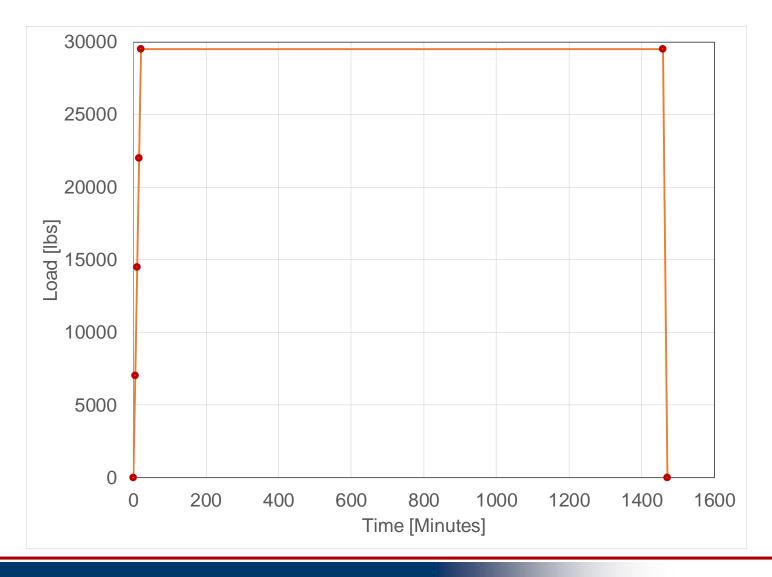


Testing Protocol and Test Magnitudes

Load Step	Min. Time per Step	Load Applied at Each Point (kips)	Total Applied Test Load (kips)
1	-	0.3	0.6*
2	5 min	3.5	7
3	5 min	7.25	14.5
4	5 min	11	22
5	24 hours	14.75	29.5
6	-	0.3	0.6*
* Weight of equipment			



Load - Time





Acceptance Criteria

The maximum and residual deflection shall satisfy

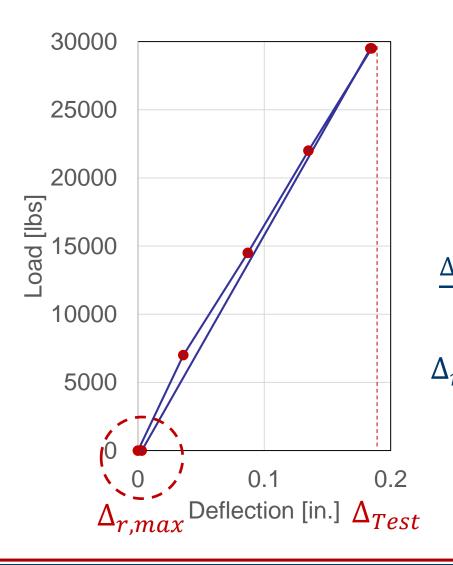
$$\Delta_{Test} \leq \Delta_{Max} = \frac{l_t}{180} = 3.3 \text{ in.}$$
Does Not Governs
Limit for re-testing
$$\Delta_{r,max} \leq \frac{\Delta_{Test}}{4}$$

where:

 l_t = span of the member under test Δ_{Test} = measured max deflection $\Delta_{r,max}$ = measured residual deflection



Test Results – Load Deflection



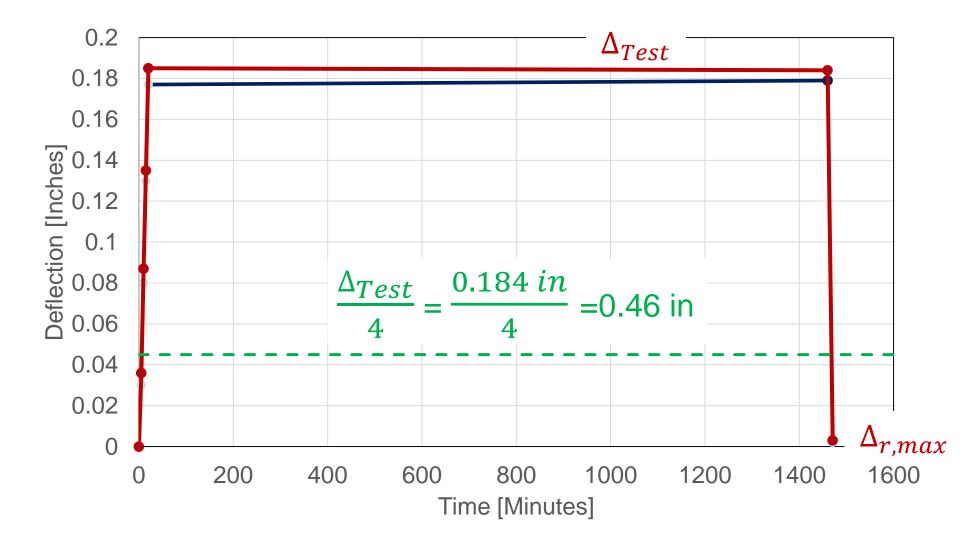
$$\Delta_{Test} = 0.184 \text{ in } \leq \Delta_{Max} = 3.3 \text{ in.}$$

$$\Delta_{Test} = \frac{0.184 \text{ in}}{4} = 0.046 \text{ in}$$

$$M_{Test} = 0.003 \text{ in } \leq 0.046 \text{ in (PASS)}$$



Test Results – Deflection Time





Conclusions

- The monotonic load testing was used to verify the shear capacity of a double tee beam failed in shear.
- The load test was designed to verify the shear performance of only the repaired zone. The remaining portion of the beams was below cracking.
- The structure met the acceptance criteria of ACI 437.2 and stayed elastic during the load test.
- Is a deflection criteria meaningful when testing for shear or would a pass/fail criteria be more feasible?



Thank You

Any Questions?

