



## **Overview Of EPRI Concrete Projects**

Ken Barry Technical Executive <u>kbarry@epri.com</u>

## **EPRI Team**

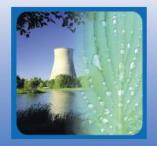
- Key People
  - EPRI Technical Leads: Ken Barry, <u>kbarry@epri.com</u>, Maria Guimareas, <u>mguimaraes@epri.com</u>
- Relevant EPRI Products
  - General Outline for Conducting Quality Inspections and Tests of Concrete Placement at Nuclear Facilities (3002000520)
  - Nondestructive Evaluation of Steel-Concrete Construction Mockups (3002000294)
  - Embedded Sensors in Concrete(1023006)
  - Quality Control of Concrete During Construction Voids Detection (1025300)



# Concrete Inspection Field Guide - published in pocketbook and iPad format

 Guidelines on quality control of new pours, addressed to utility engineers who will ultimately be responsible for the quality of the concrete placement.





General Outline for Conducting Quality Inspections and Tests of Concrete Placement at Nuclear Facilities

3002000520



Check that procedures are OK.

Surveillance – Oversight role

Readiness review document: List of items that need to be checked before, for example, "pouring concrete"



## **Concrete Inspection Field Guide**

#### ACI - American Concrete Institute

- SP-2, "ACI Manual of Concrete Inspection"
- ACI-311.4R, "Guide for Concrete Inspection"
- ACI 311.5R, "Guide for Concrete Plant Inspection and Testing of Ready-Mixed Concrete"
- ACI 318, "Concrete Building Code"
- ACI 349, "Code Requirements for Nuclear Safety Related Concrete Structures"

#### • ASME - American Society of Mechanical Engineers

- Section III, Division 2, "Code for Concrete Containments" (ACI 359)
- Section III, Division 2, Mandatory Appendix V, "Qualifications of Concrete Inspection Personnel"
- NQA-1, Subpart 2.5, "Quality Assurance Requirements of Installation, Inspection, and Testing of Structural Concrete, Structural Steel, Soils, and Foundations for Nuclear Facilities

#### NRMCA - National Ready Mixed Concrete Association

QC Manual Section 3, "Plant Certification Checklist"



## **High Strength Rebar**

- The use of higher strength rebar in the design and construction of safety related concrete structures will result in a decrease in reinforcement congestion which is the main cause of void problems during concrete placement, but it is not allowed in ACI 349 nor 359
  - Current Code limit is 60ksi steel
- Develop technical basis informing modifications to ACI codes 349 and 359 enabling use of high-strength rebar in safety-related structures.
- Project Duration: 2012-2017



Leverage from: Kansas University Transportation Research Institute -Concrete Reinforcing Steel Institute -Charles Pankow Foundation



## **High Strength Reinforced Rebar**

#### **Project Details**

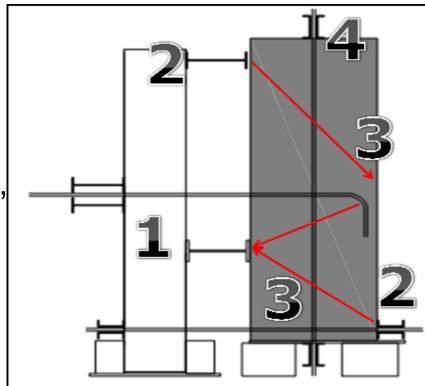
- The goal of the experimental study is to gain a firm understanding of the variation in hook and head strength as a function of bar size, concrete strength, member geometry, and transverse reinforcement.
- Emphasis in the tests will be placed on No. 5, No. 8, and No. 11 hooked bars tested at bar stresses of 60, 80 and 100 ksi. A limited number of bars will be tested at stresses as high as 120 ksi.
- Concrete compressive strengths of 5000, 8000, 12,000 and 15,000 psi will be used.



## **High Strength Rebar Testing**

#### **Design considerations included**

- (1) a compressive reaction simulating the compression zone of the beam,
- (2) reactions at the top and bottom of the specimen to prevent rotation of the specimen,
- (3) designing the specimen so that the compression struts from these reactions do not interfere with the hook,
- (4) simulating axial force in a normal column.





## **Hooked Bar Testing**

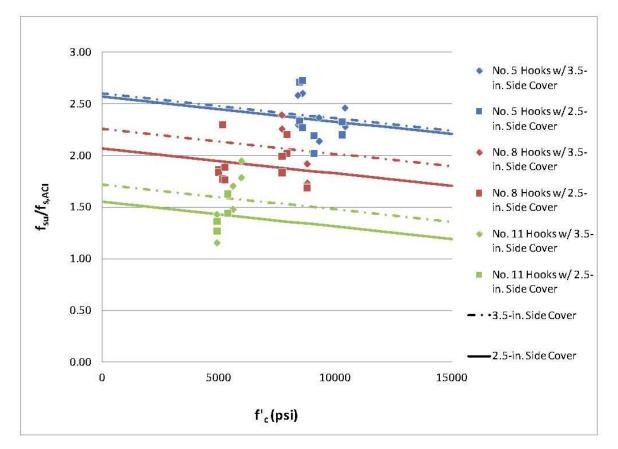
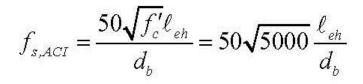
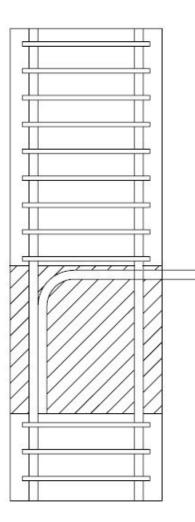


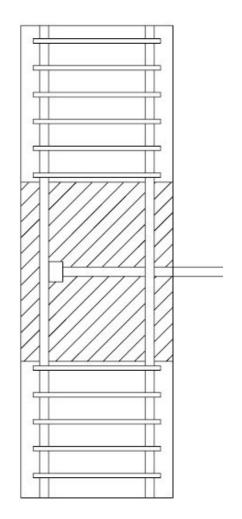
Figure 2: Ratio of measured to calculated stress for hooks without transverse reinforcement. Hooks inside column core





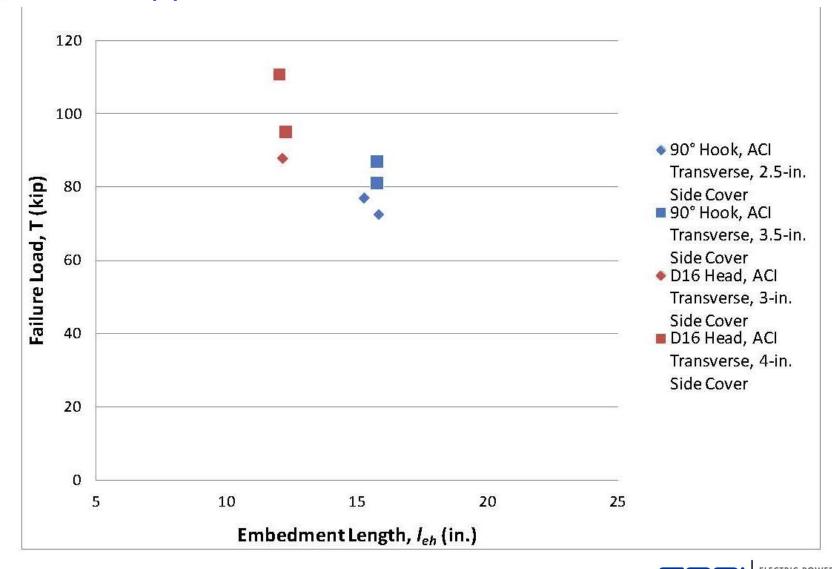
# Specimens with hooked and headed bars without transverse reinforcement showing regions without ties







# Anchorage strength of No. 8 hooked and headed bars in 5000 psi concrete with transverse reinforcement conforming to ACI 318 Section 12.5.3(b)







- 3' x 3' x 10' steel/concrete mockup fabricated
- Access from steel sides or concrete top
- Known voids/laminations installed





- 120 ton Steel/Concrete
  Composite Mockup
- Large voids installed at most probable locations
- Access from steel plates, concrete sides and vent lines





- Techniques Used
  - Pulse/Echo UT
  - Phased Array UT
  - Impact Echo Method
  - Ground Penetrating Radar (concrete face only)
- Tremendous quantity of data collected in 3 days
  - 5 methods, 14 separate locations
  - Pulse/Echo UT on concrete found all voids

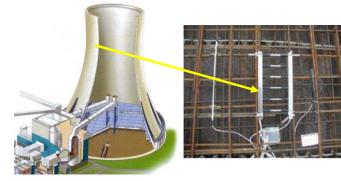


## **Embedded sensors in new structures**

Scoping study on the use of embedded sensors to monitor <u>aging</u> of concrete for new nuclear plants

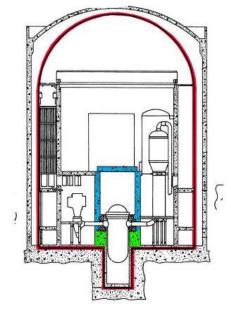














## **Embedded Sensors - Concrete structures**



**Cooling Towers** 

**Spent Fuel Pool** 

**Foundations** 

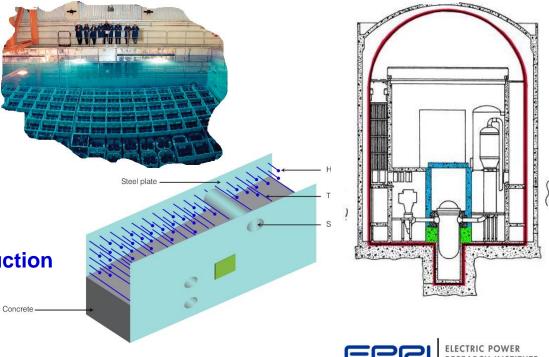
Hot penetration sleeves

Structures subjected to radiation

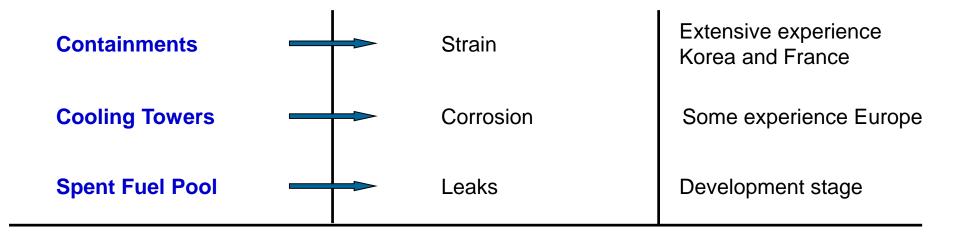
**Concrete based modular construction** 

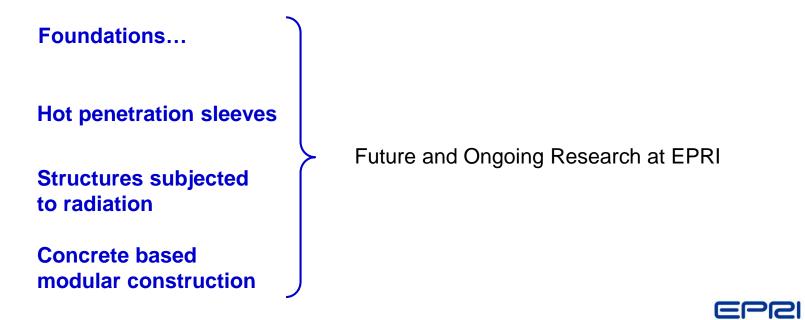






### **Embedded Sensors - Parameters to monitor**

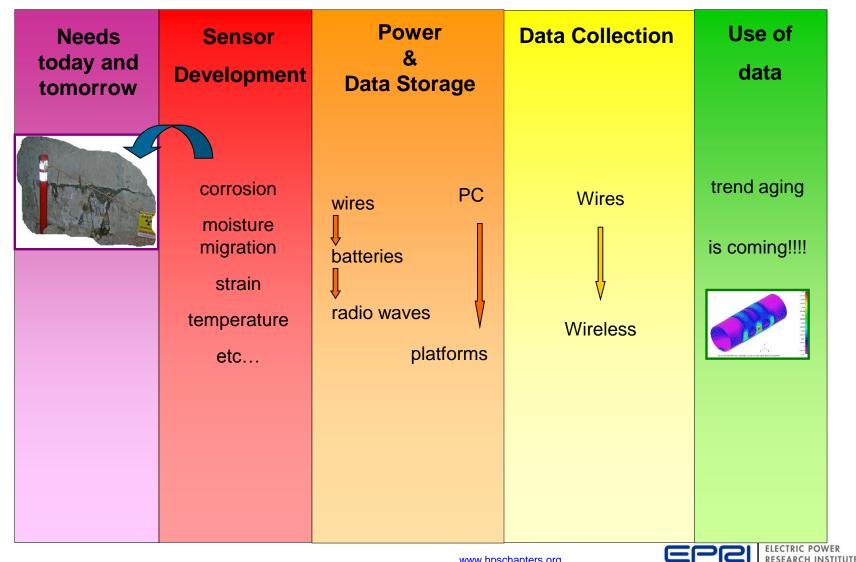




## **Concrete containments – Used before?**

Plant / country	Reactor type PT	Durability (years)	Type of sensors	Sensor location	Number of sensors
EdF fleet France	PWR	30+	Vibrating Wire		32 / unit 24 / unit
Gentilly 2 Canada	CANDU	30+	Vibrating Wire	Dome, perimeter wall, ring beam, base slab, openings	132 sensors
Pont Lepreau Canada	CANDU	10+	Vibrating Wire Fiber Optic Sensor	VW in dome and cylinder FOS attached to surface between buttresses	11 sensors 4 sensors
Uljin <mark>Korea</mark>	Framatome – PWR	Not available	Fiber Optic Sensor	Attached to surface	n/a
		20+ 15-20% malfunct.	Strain Gauge	Dome, wall, base mat, gusset,	52 / unit 24 / unit
Wolsong Korea	CANDU	20+ 15-20% malfunct.	Vibrating Wire	Dome, perimeter wall, ring beam, base mat, hinge	118 / unit
Temelin Czech Republic	VVER – PWR ungrouted	10+	Vibrating Wire	Dome, cylindrical wall, ring beam	246 / unit 256/ unit

## **Embedded Sensors – Future Application**



### **NDE for quality control for Fresh Concrete**

#### Can we use NDE for quality control during construction/repairs?

- Feasibility of using NDE in fresh concrete for quality control during construction. Several NDE techniques were tested.
  - Electrical conductivity
  - Electromagnetic permittivity
  - Mechanical P-Wave velocity (acoustics)
  - Gamma
  - Thermal



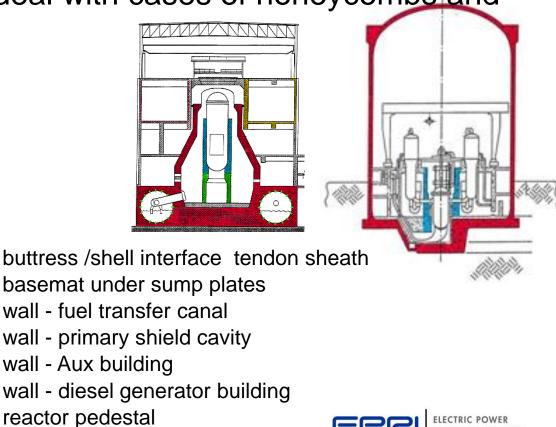


## Summary of cases from early construction

- NUREG 4652 summarizes construction related delays in existing fleet.
- Out of ~90 reports, 32 deal with cases of honeycombs and voids

#### **Structures affected**

Foundation and basemat wall – containment wall - containment - equipment hatch Wall - behind liner plate ring girder - containment concrete near tendon bearing plates Wall - drywell



# Can We Detect the Voids Before the Concrete Sets?



Go – No-go indication on the presence of voids and honeycombs

# The Future?

Multiple Probes Mounted on Vibrator



### NDE Techniques for Fresh Concrete Void Detection and Sizing

ΤοοΙ	SNR	Implementability	Comments / Limitations
Gamma density	4	<u>2</u>	license, certification, contamination
Temperature	1	3	very poor SNR
P-wave velocity	3	3	possible false-positives
Mechanical Impedance	<u>2</u>	4	data interpretation
Electrical conductivity	4	4	
Permittivity - TDR based	4	4	
Permeability - Gas Flow	3	3	emphasis on cementing fluids

1 = worst

SNR: signal-to-noise ratio

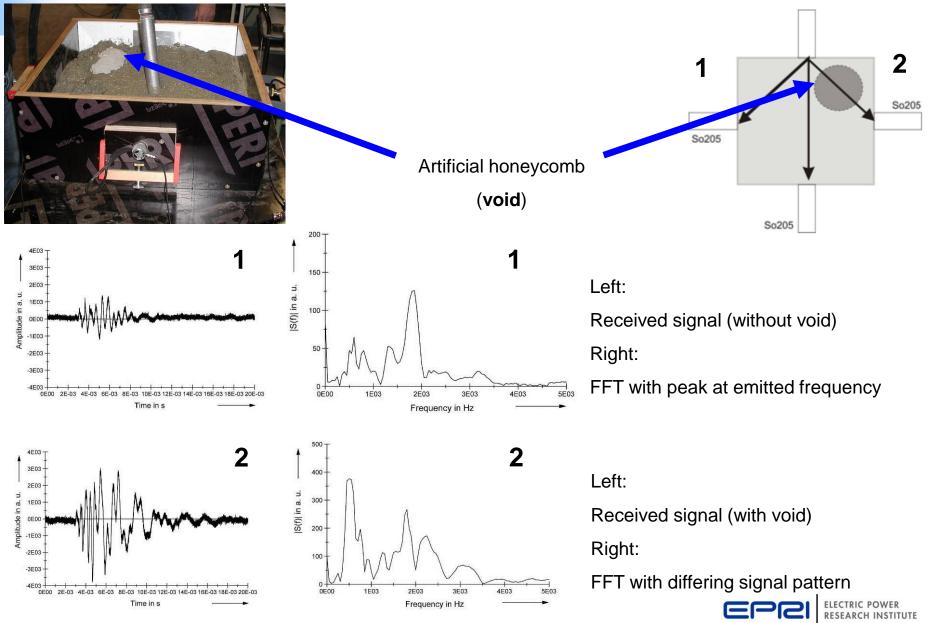
5 = best

### NDE Techniques for Fresh Concrete Void Detection and Sizing

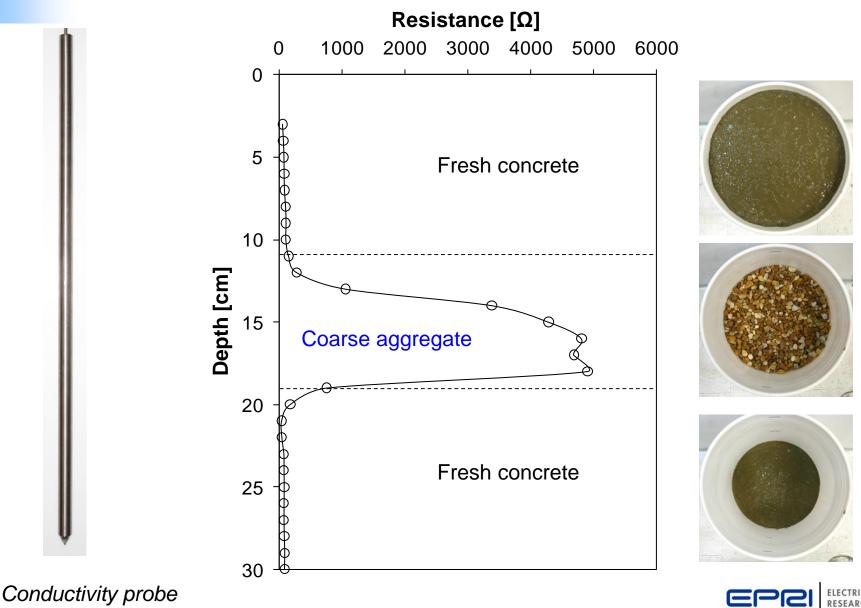
- **Time-domain reflectometry** (TDR) Permittivity can measure a discontinuity in homogenous substances by observing reflected waveforms.
- P-wave velocity Ultrasonic longitudinal waves propagate in gases, liquids or solids. P-wave velocity measurements are very different between fresh concrete and air. Therefore, they have a potential to have large signal to noise ratio.
- Electrical Conductivity of curing cement changes over time and is directly dependent on temperature. The presence of a void is distinctly discernable.
- Gamma Density methods are based on selective absorption. Global absorption depends on the elemental absorption and mass fraction with amplitude decaying exponentially with distance <sup>137</sup>Cs is preferred for concreterelated applications.
- Permeability Gas Flow The injection pressure ideally approaches zero in honeycombs, and closes to the 'hydro-static pressure' of fresh concrete in paste-saturated fresh concrete.



#### **Exploratory Test - Ultrasonic**



#### **Exploratory tests - Electrical conductivity**

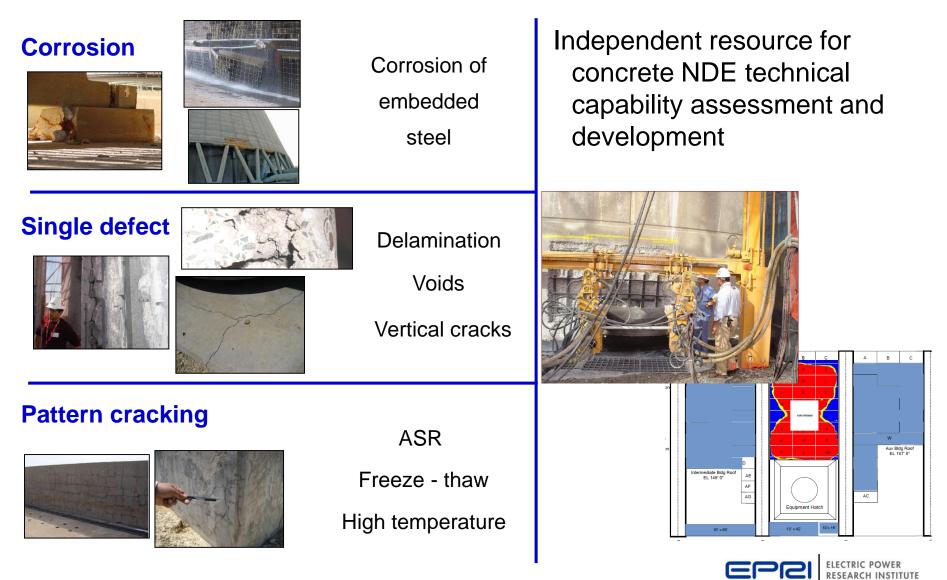


© 2014 Electric Power Research Institute, Inc. All rights reserved.



## **Other Projects**

## **NDE capabilities for concrete**

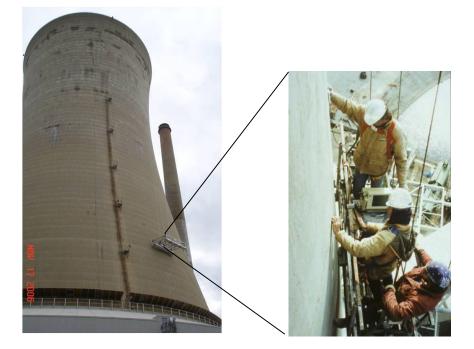


© 2014 Electric Power Research Institute, Inc. All rights reserved.

## **Automation of concrete inspection**

The availability of automated concrete inspections will translate into faster and less costly inspections of vertical structures. This will allow for easier and more frequent inspections of the aging nuclear fleet.







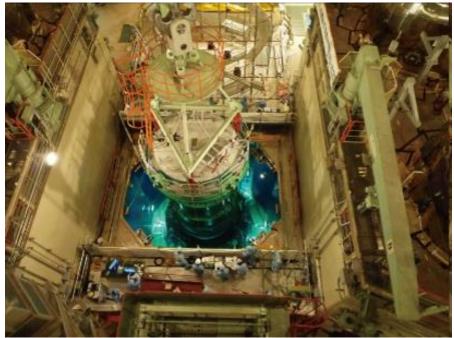
http://www.youtube.com/EPRIvideos

## **Radiation damage in concrete**



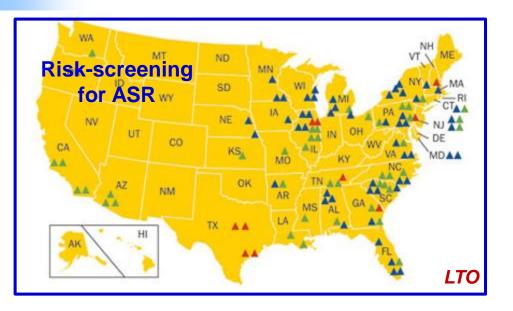
EPRI is working on a new report with updated data on irradiated concrete samples.

In parallel, research in fundamental understanding on radiation in concrete will be pursued Reactor cavity concrete may see > 10<sup>20</sup> n/cm<sup>2</sup> during the period of Long Term Operation, which is beyond the design basis.



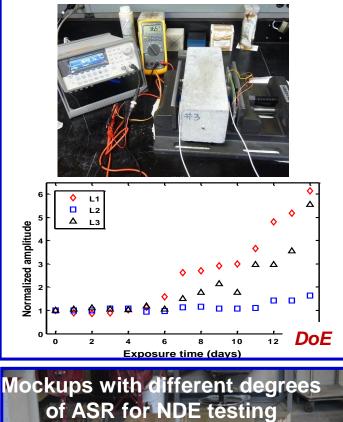


## **EPRI 's projects on ASR**





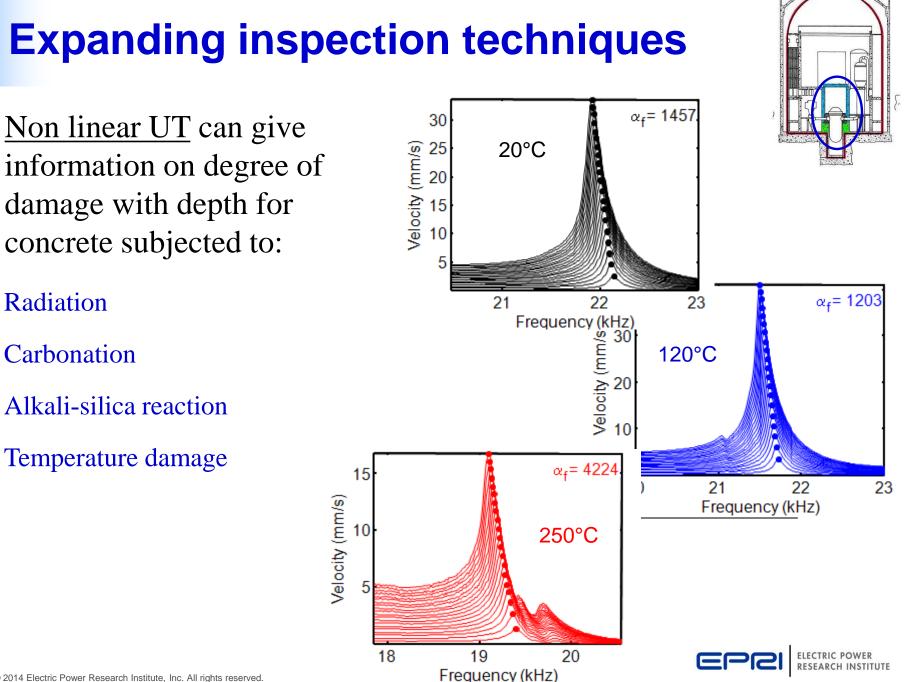
#### Non-linear UT to detect ASR





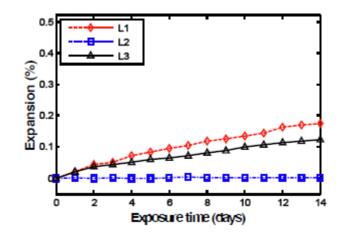


ELECTRIC POWER RESEARCH INSTITUTE

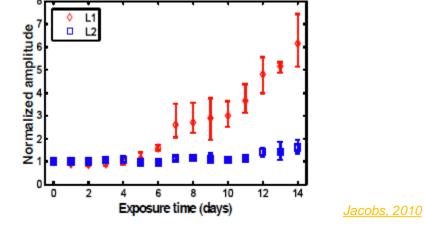


## **Non-linear Ultrasound**

<u>Non linear UT</u> can give information on degree of damage with depth for concrete subjected to ASR.



% expansion of concrete bars with different degrees of ASR



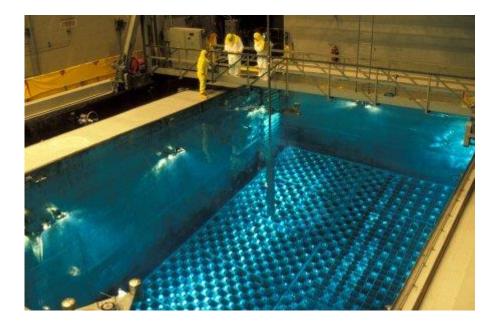
Normalized amplitude (non linear parameter) in the same concrete bars with different degrees of ASR

Note the sensitivity of the acoustic non linear parameter in detecting the degree of damage caused by ASR



## **Concrete degradation in Spent Fuel Pool**

Concrete in spent fuel pools is degrading due to leakage beneath the liner. The spent fuel pool water exits through welds in the liner and begins to attack the concrete substructure.





1 in. = 25.4 mm

EPRI is engaged in studying the effects of water containing boric acid on the structural integrity of spent fuel pools. A project on modeling the degradation rate due to boric acid being performed in 2013-2014.



# Chloride attack in concrete – cooling towers



Cooling towers and water intakes are subjected to corrosion related degradation due to aggressive water used in the cooling system.



A project on determining the extent of degradation and the structural bearing capacity margin in severely damaged cooling towers is being performed at EPRI.



© 2014 Electric Power Research Institute, Inc. All rights reserved.





### **Together...Shaping the Future of Electricity**