



Combined effects of fiber reinforcement and layer orientation on properties of 3D printed concrete

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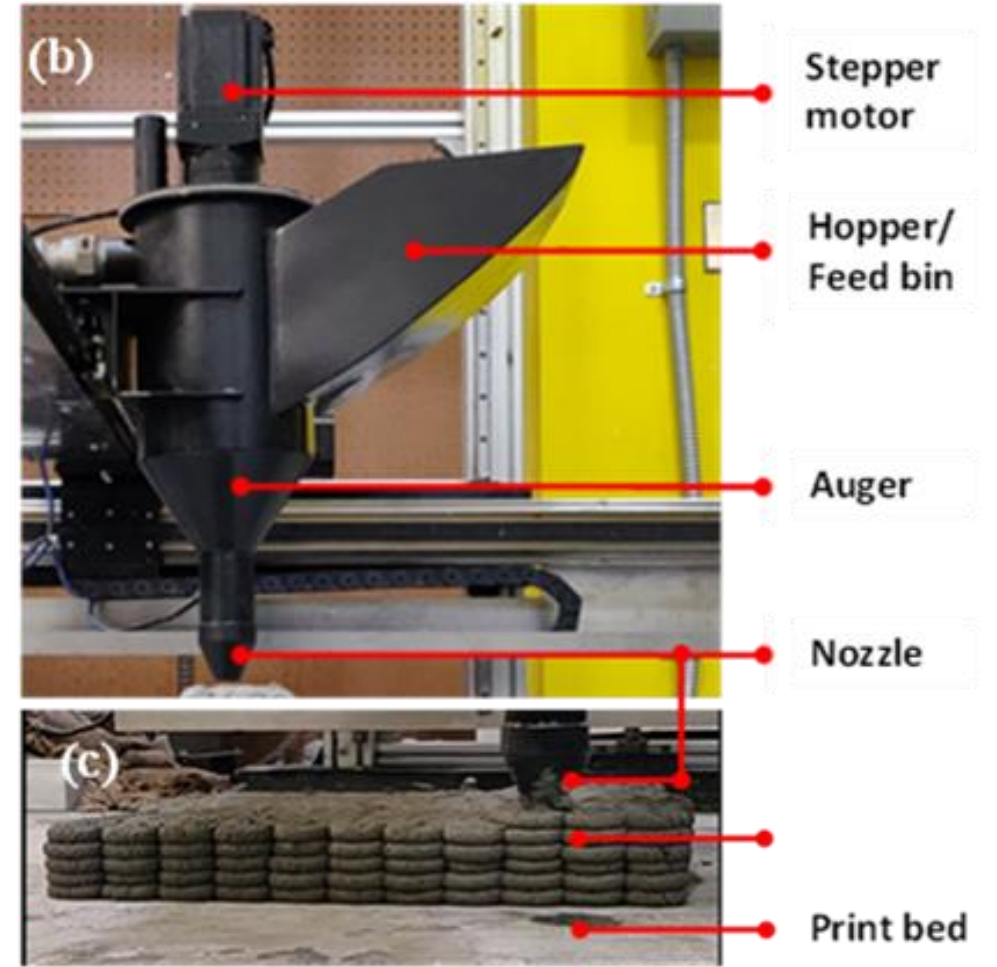
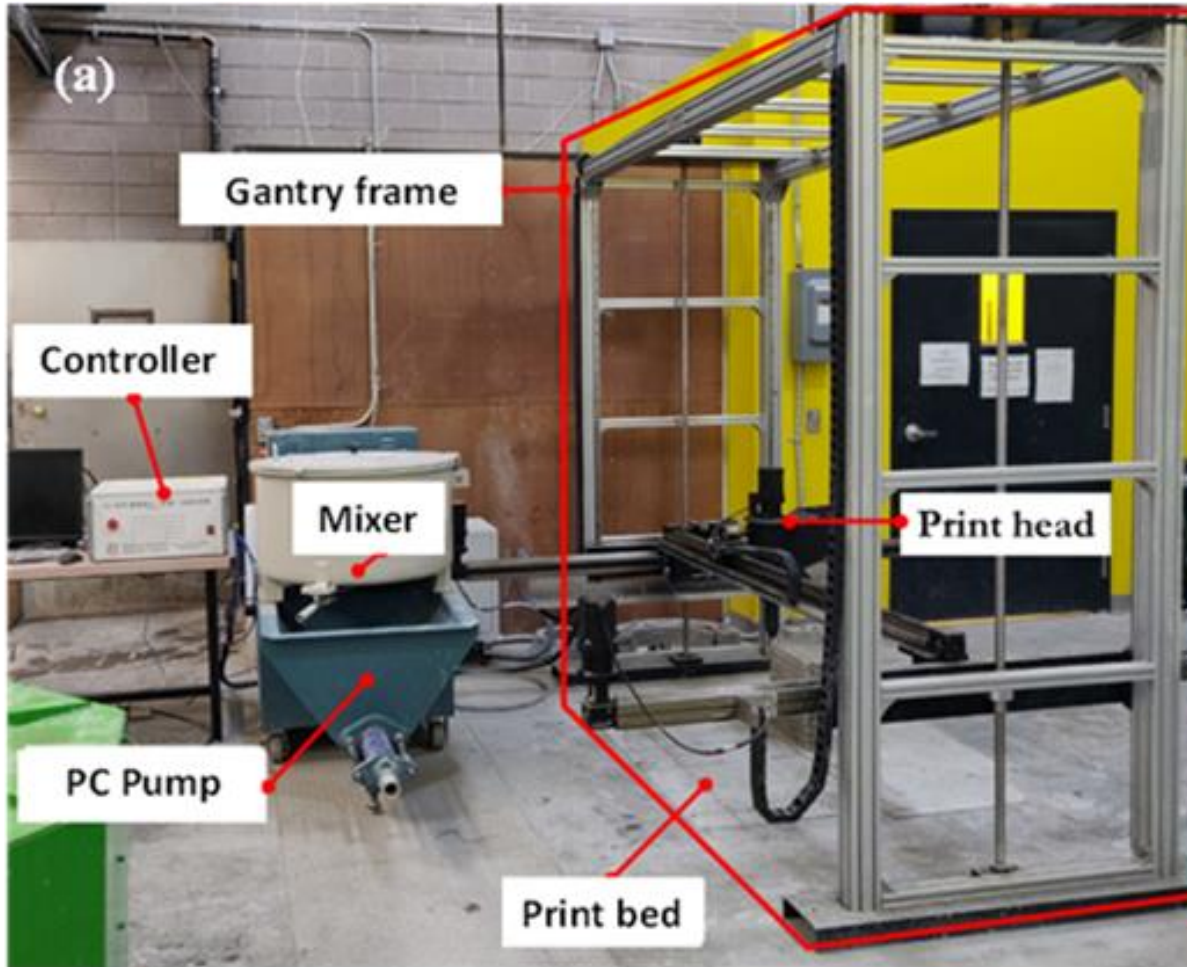
<http://neithalath.engineering.asu.edu>; <http://3dconcrete.asu.edu>



Concrete 3D Printing



Concrete printer

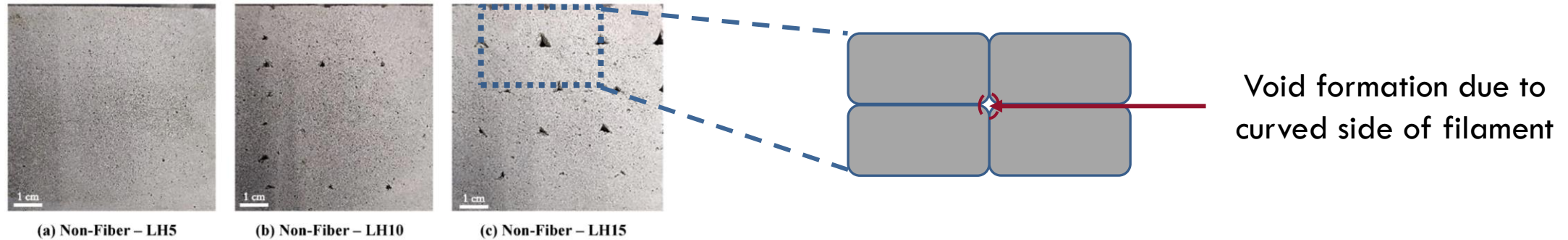




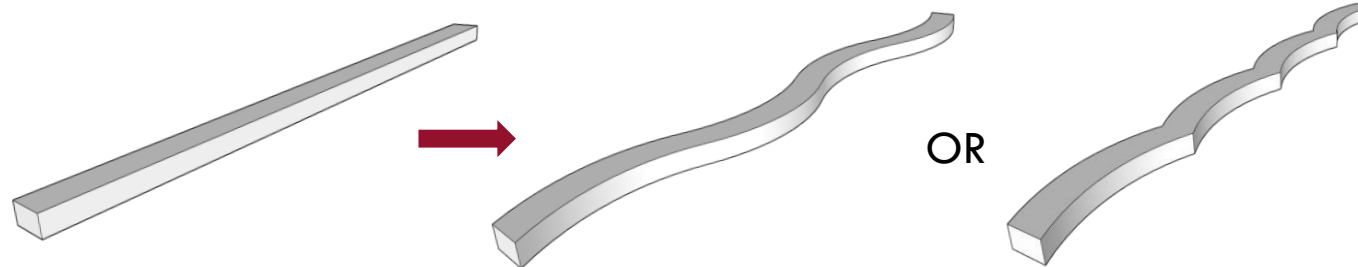
CONCRETE

Conventional Printing

- Lack of compaction results in weak bonding, sometimes formation of gap/voids mainly when using larger layer height

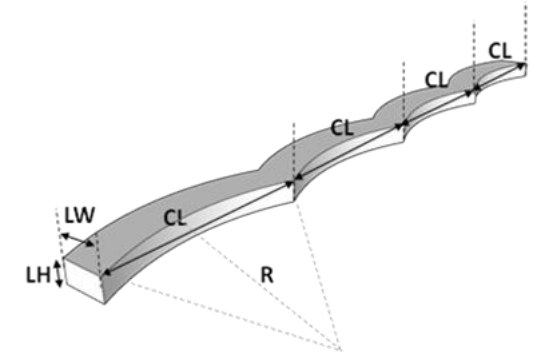
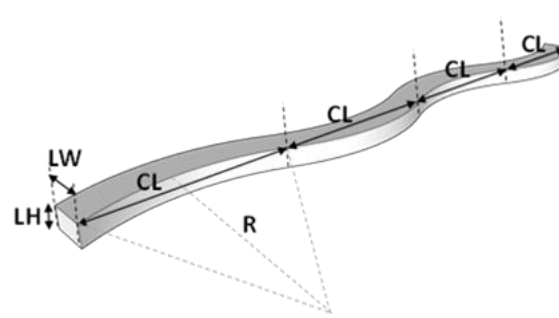
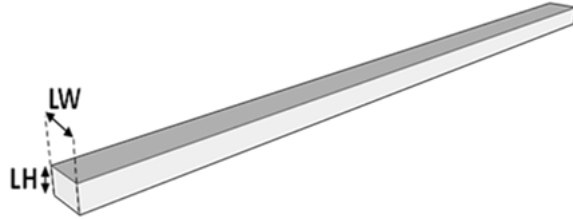


- Usually linear extrudate printed in practice, why not curve them?



- Staggering layer could help reduce chances of void formation
- Use of fiber can help bridge crack once they initiate

Filament dimensions



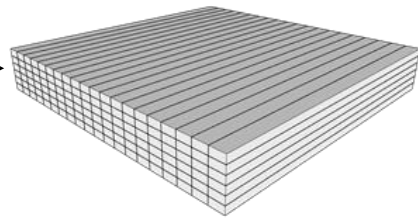
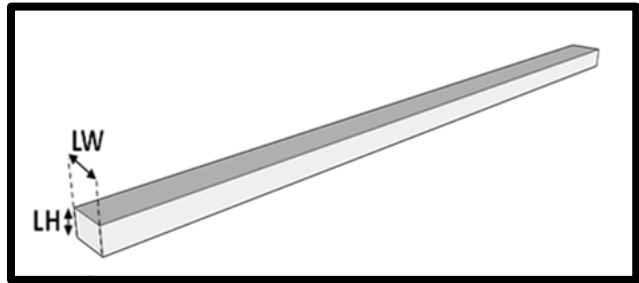
Layer Height (LH) = 10 mm;

Layer Width (LW) = 20 mm

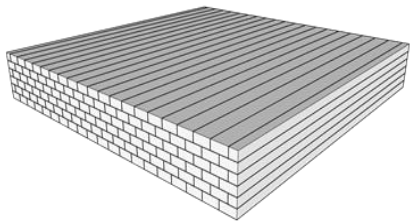
Chord Length (CL) = 100 mm

Radius (R) = 120 mm

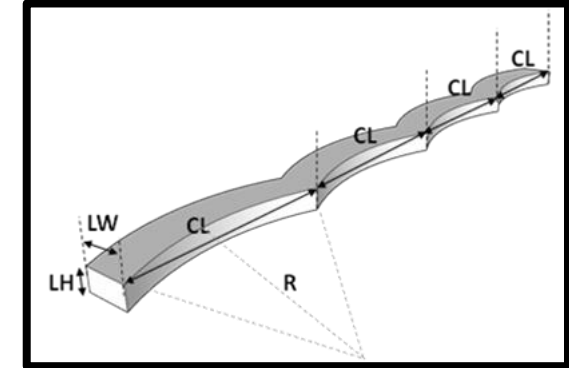
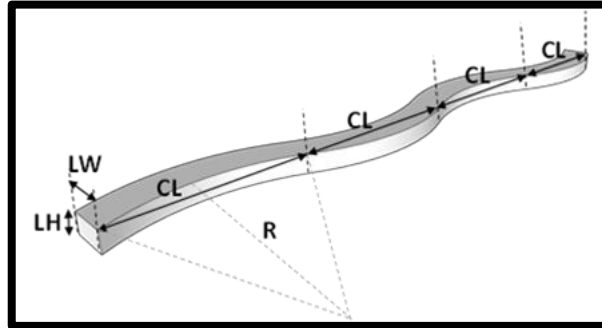
Layering type



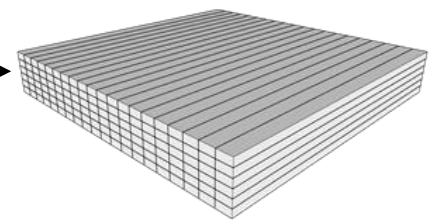
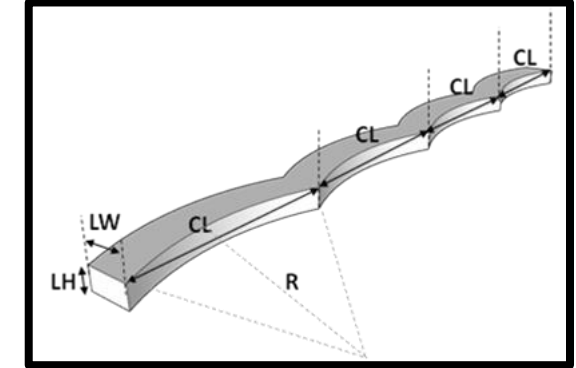
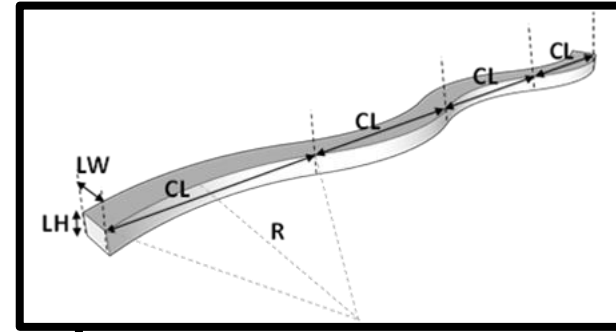
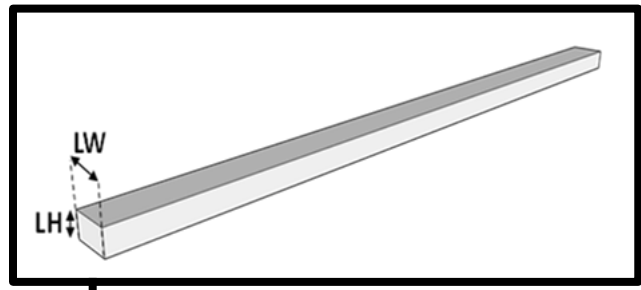
Linear Conventional (L-C)



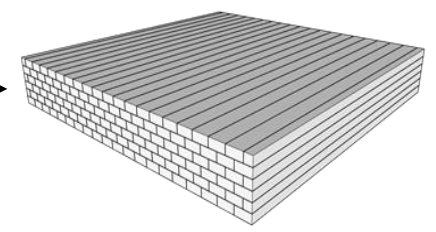
Linear Staggered (L-S)



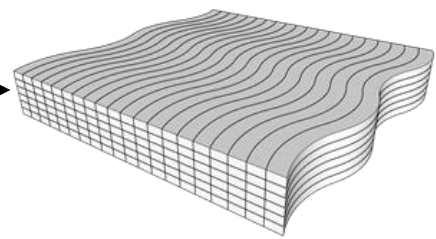
Layering type



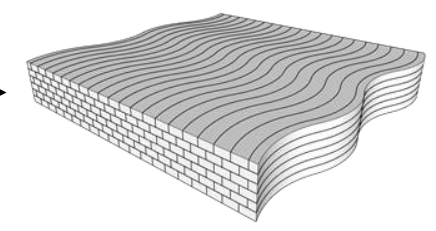
Linear Conventional (L-C)



Linear Staggered (L-S)

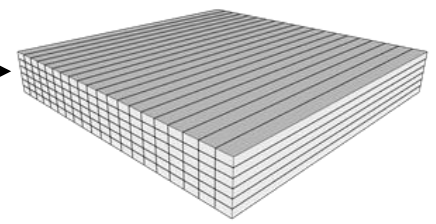
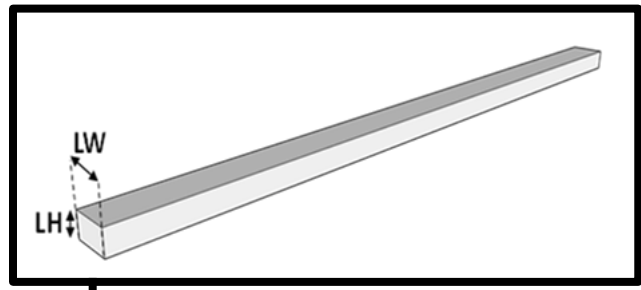


S-shaped Conventional (S-C)

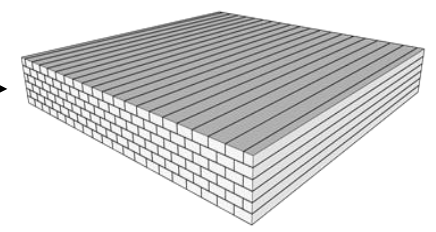


S-shaped Staggered (S-S)

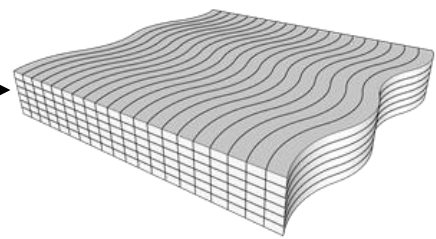
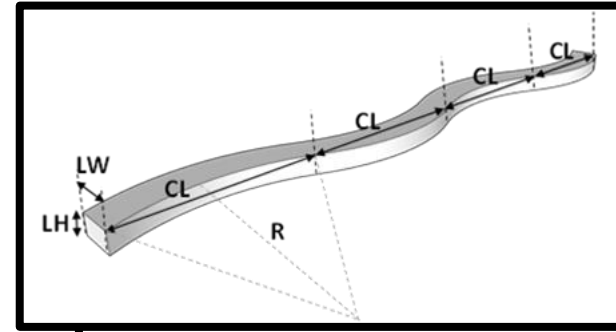
Layering type



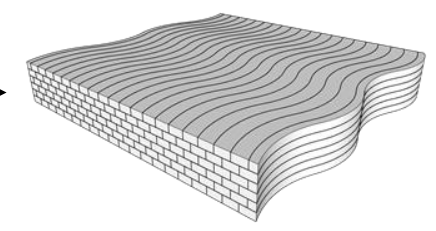
Linear Conventional (L-C)



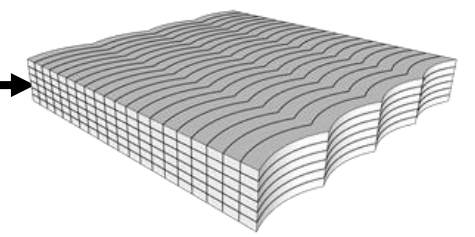
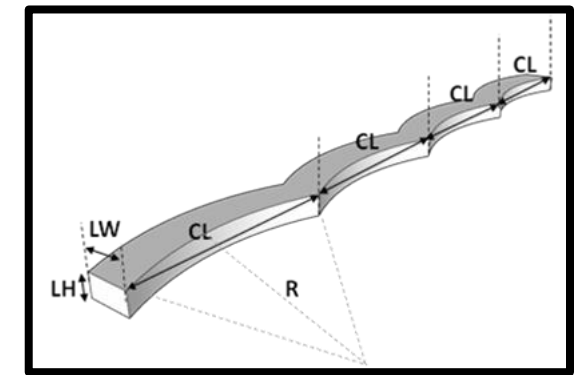
Linear Staggered (L-S)



S-shaped Conventional (S-C)

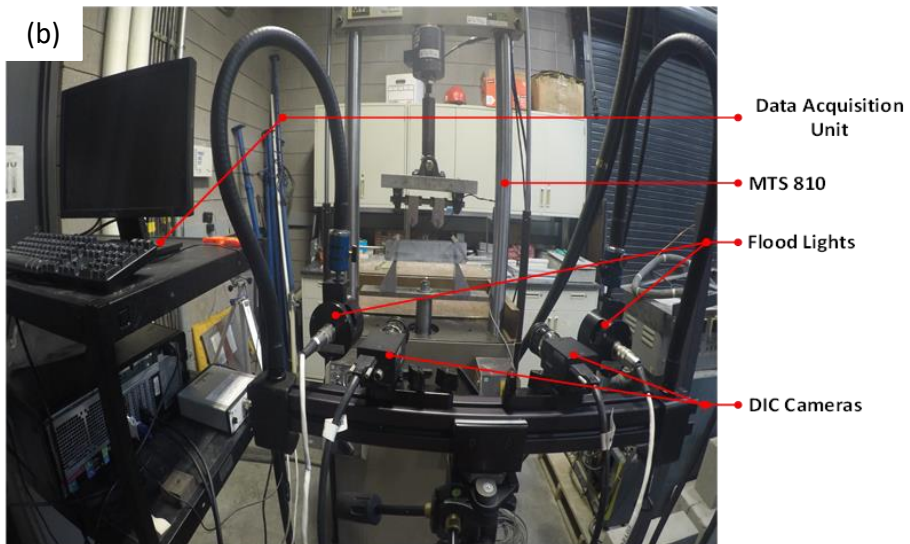
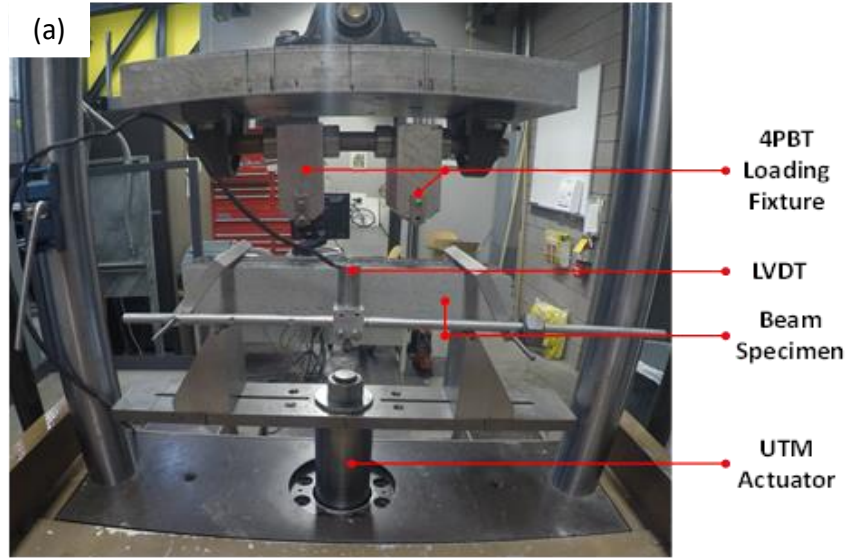


S-shaped Staggered (S-S)



3-shaped Conventional (3-C)

Geometry modification effect



Mixture ID	Mass Fraction of Ingredients			Chopped Steel Fiber (SF) ⁺	Chopped Basalt Fiber (BF) ⁺	Water-to-binder ratio (w/b) by mass	SP solid to binder ratio (SP%) by mass of the binder
	OPC	Limestone (L)	Sand (M)				
L ₃₀	0.35	0.15	0.5	-	-	0.35	0.05
L _{30-SF}	0.35	0.15	0.5	0.28	-	0.35	0.07
L _{30-BF}	0.35	0.15	0.5	-	0.28	0.35	0.07

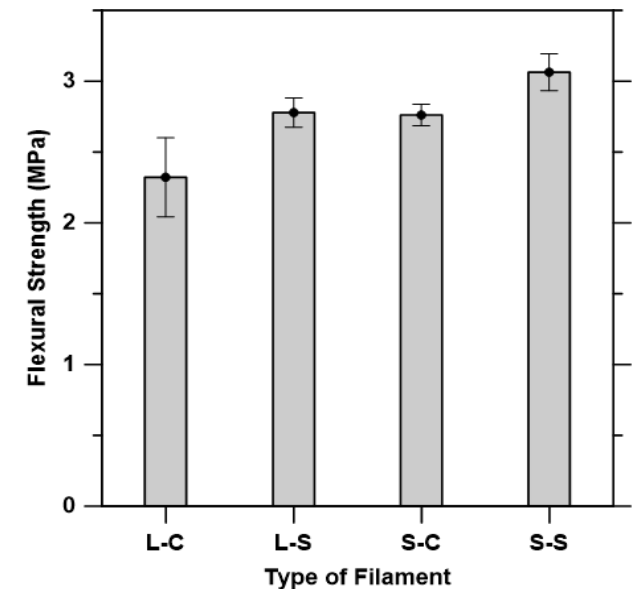
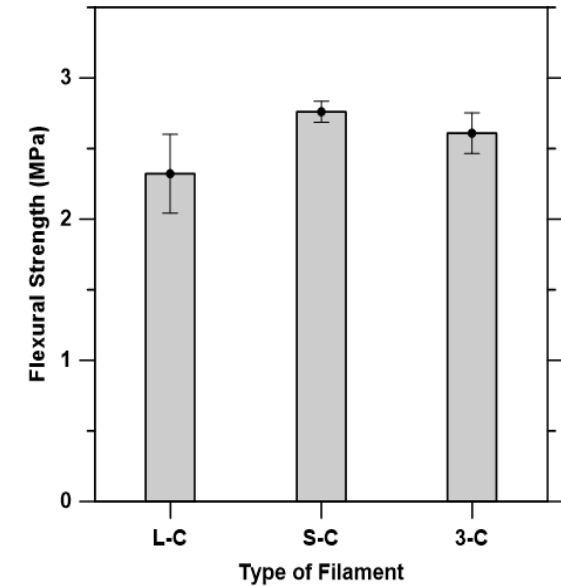
⁺Percentage by volume of the mixture.



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Flexural Strength

- Beam tested (60 x 60 x 300 mm).
- For L-C, inter filament joint runs parallel to the length direction.
- For S-C and 3-C, inter filament joints do not align completely to the length of the beam.
- Curved nature ensuring that the stress required to failure is higher due to the tortuosity introduce.
- Staggering of the filament ensures reduction of voids which could be formed between four filaments sitting side by side between two layers.

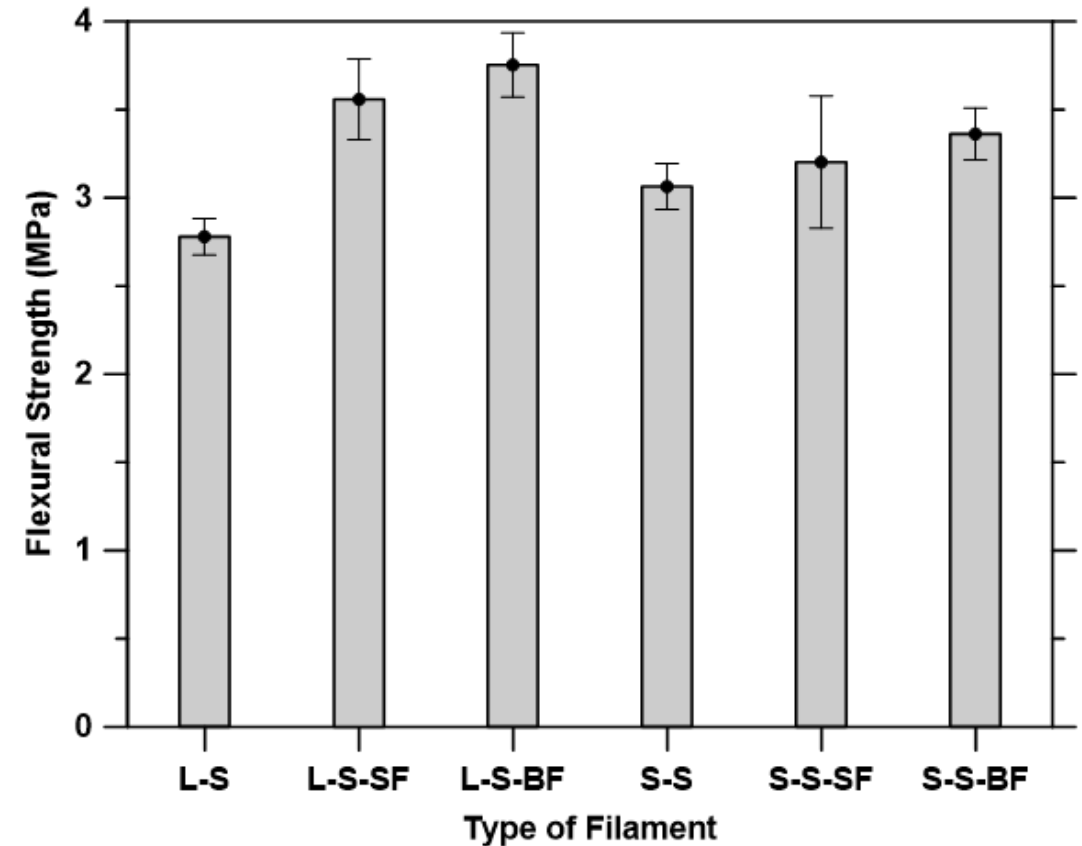




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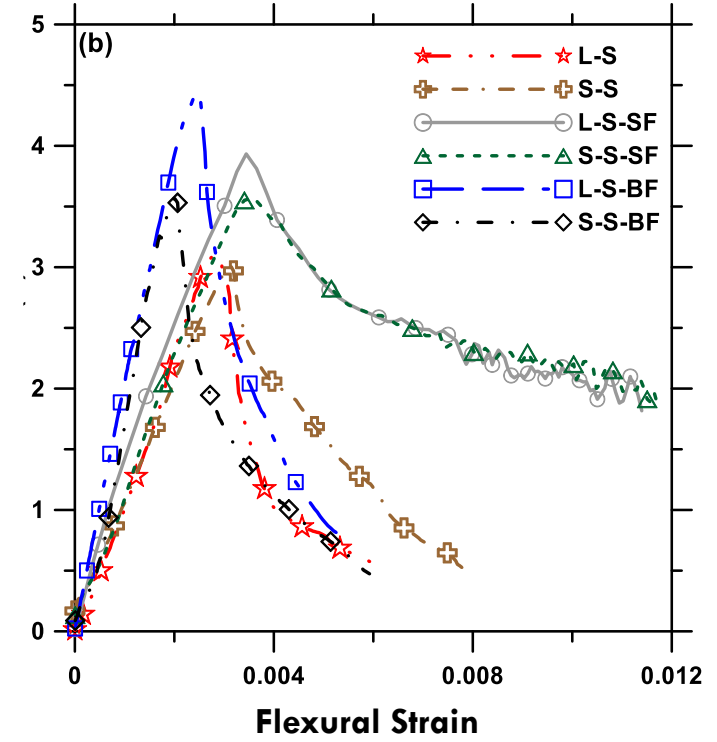
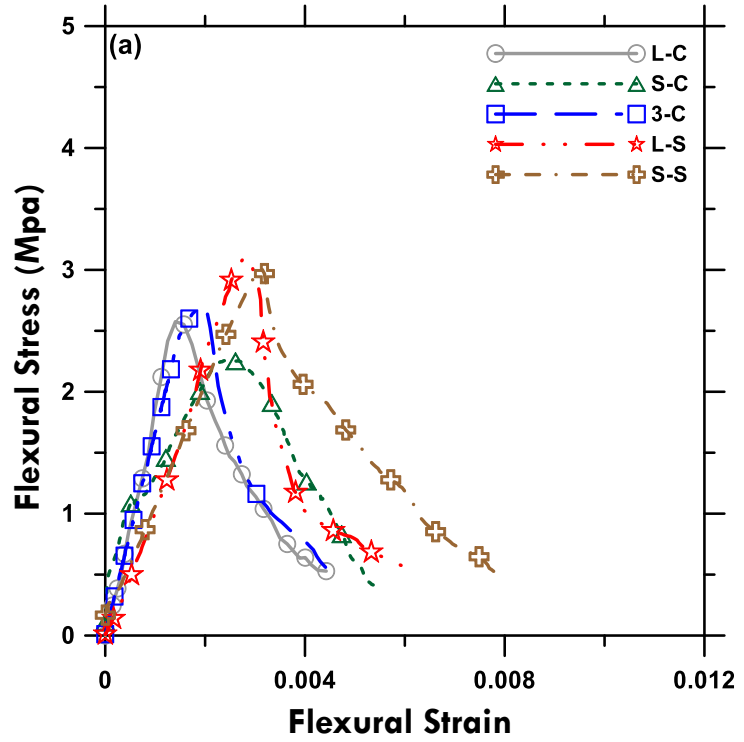
Fiber effect (at low dosage)

- Near 10-30% enhancement when fibers are used.
- Alignment of fiber along the print path meant reduced efficiency of the S-shaped filament.
- At lower percentage, use of basalt fiber resulting in higher increase in the flexural strength than using steel fiber.
- For the same volume percentage content, 13 times the number of basal fibers in the mixture as compared to steel fibers.



Flexural response

- Increase in flexural strain for S- and 3- shaped prints
- Basalt fiber, despite providing better flexural strength, did not provide ductility to the beams.
- Steel fiber provides ductility (providing higher toughness than with basalt fiber)
- Similar observation made from digital image correlation

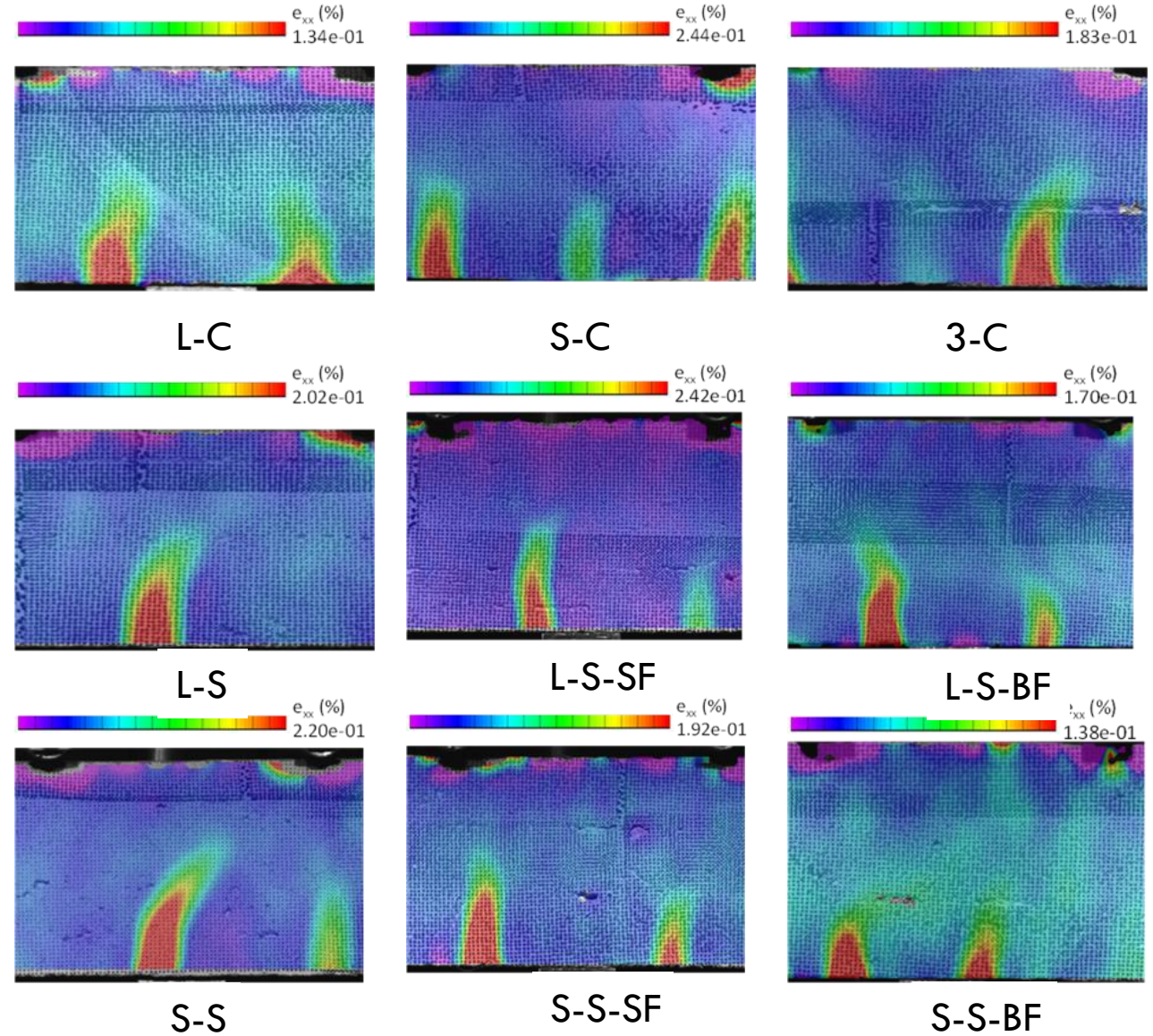




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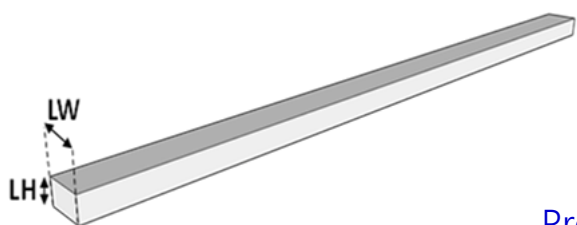
Strain profile at peak

- Strain profile observed through DIC analysis agrees with the flexural response
- Redistribution of strain occurs when a crack forms, hence maximum strain at peak stress are not indicators of average strain across the depth when LVDTs or strain gages are used.
- Multiple strain concentration location observed, finally one dominates and crack initiates from that place



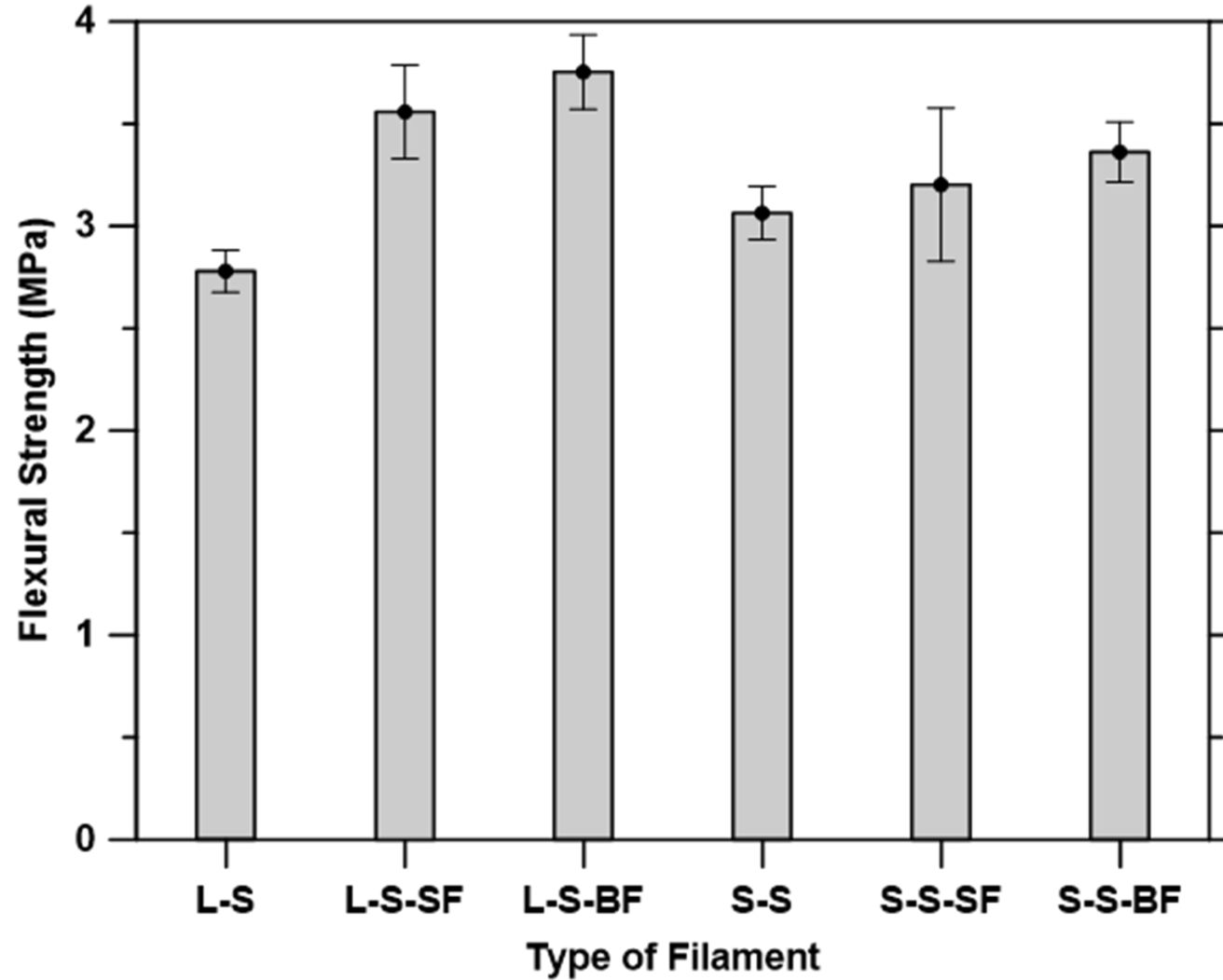
UHPC mixture (high fiber dosage)

Mixture ID	Mass Fraction of Ingredients					Chopped Steel Fiber (SF)*	Chopped Basalt Fiber (BF)*	Water-to-binder ratio (w/b) by mass	SP solid to binder ratio (SP%) by mass of the binder
	OPC	Fly Ash (F)	Limestone ($d_{50}=1.5 \mu\text{m}$) (L_f)	Slag (S)	Sand (M)				
$F_{10}S_{10}(L_f)_{10}$	0.42	0.06	0.06	0.06	0.4	-	-	0.19	0.22
$F_{10}S_{10}(L_f)_{10}-SF_{1\%}$	0.42	0.06	0.06	0.06	0.4	1	-	0.19	0.22
$F_{10}S_{10}(L_f)_{10}-SF_{1.5\%}$	0.42	0.06	0.06	0.06	0.4	1.5	-	0.19	0.22
$F_{10}S_{10}(L_f)_{10}-BF_{1.5\%}$	0.42	0.06	0.06	0.06	0.4	-	1.5	0.19	0.22
* Percentage by volume of the mixture									

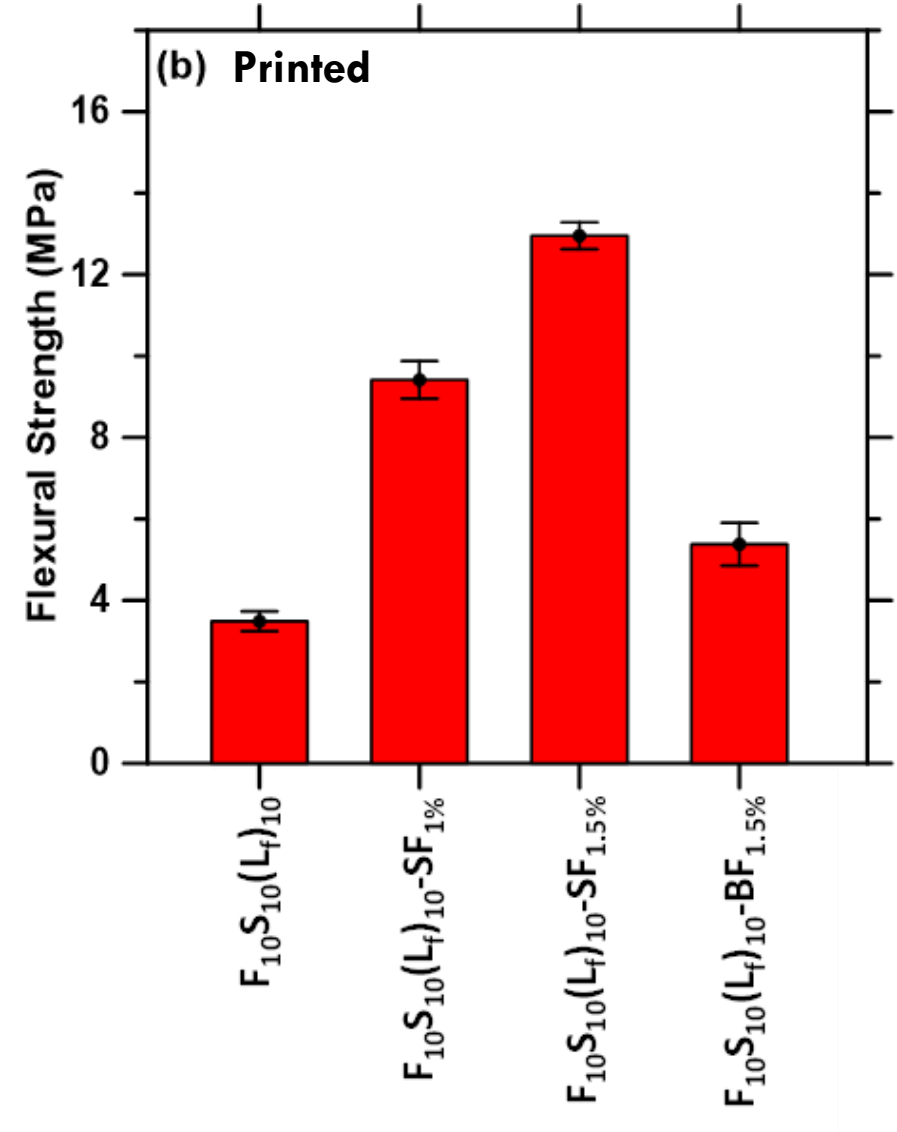
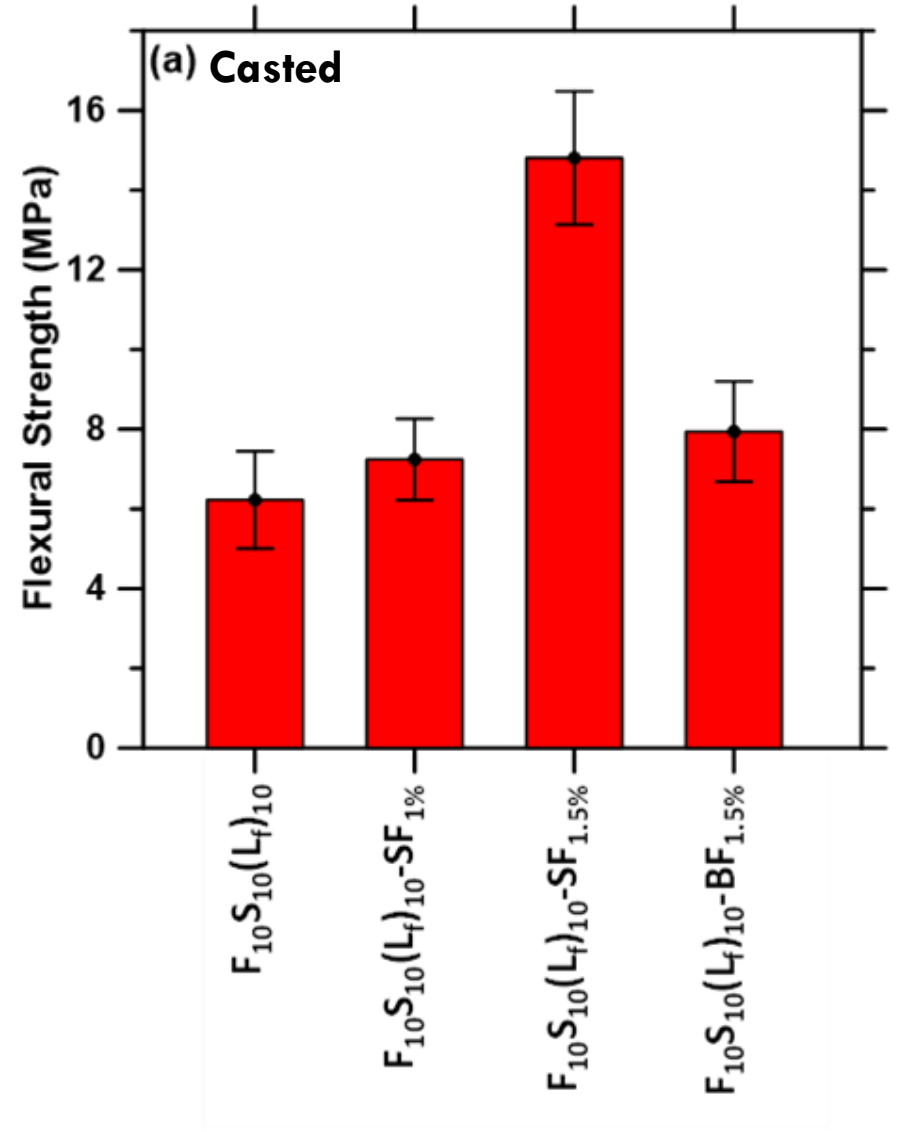




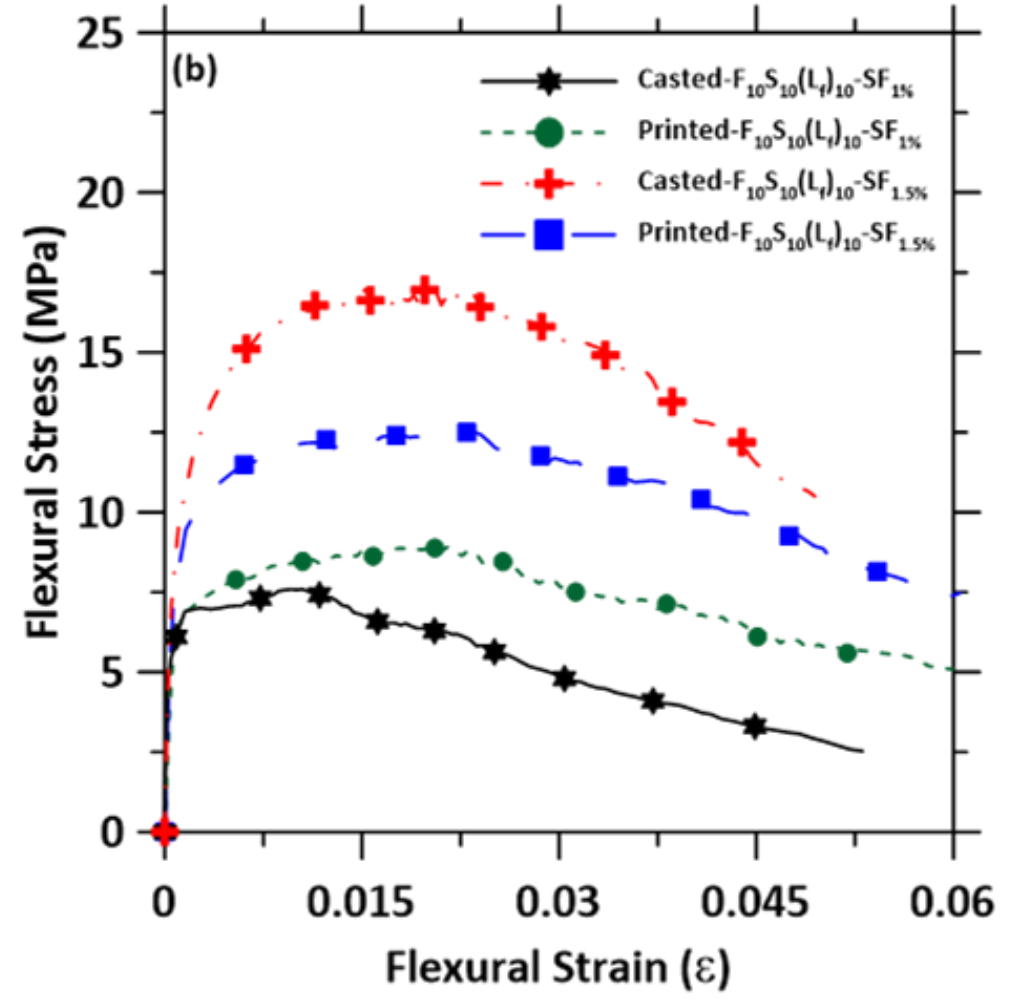
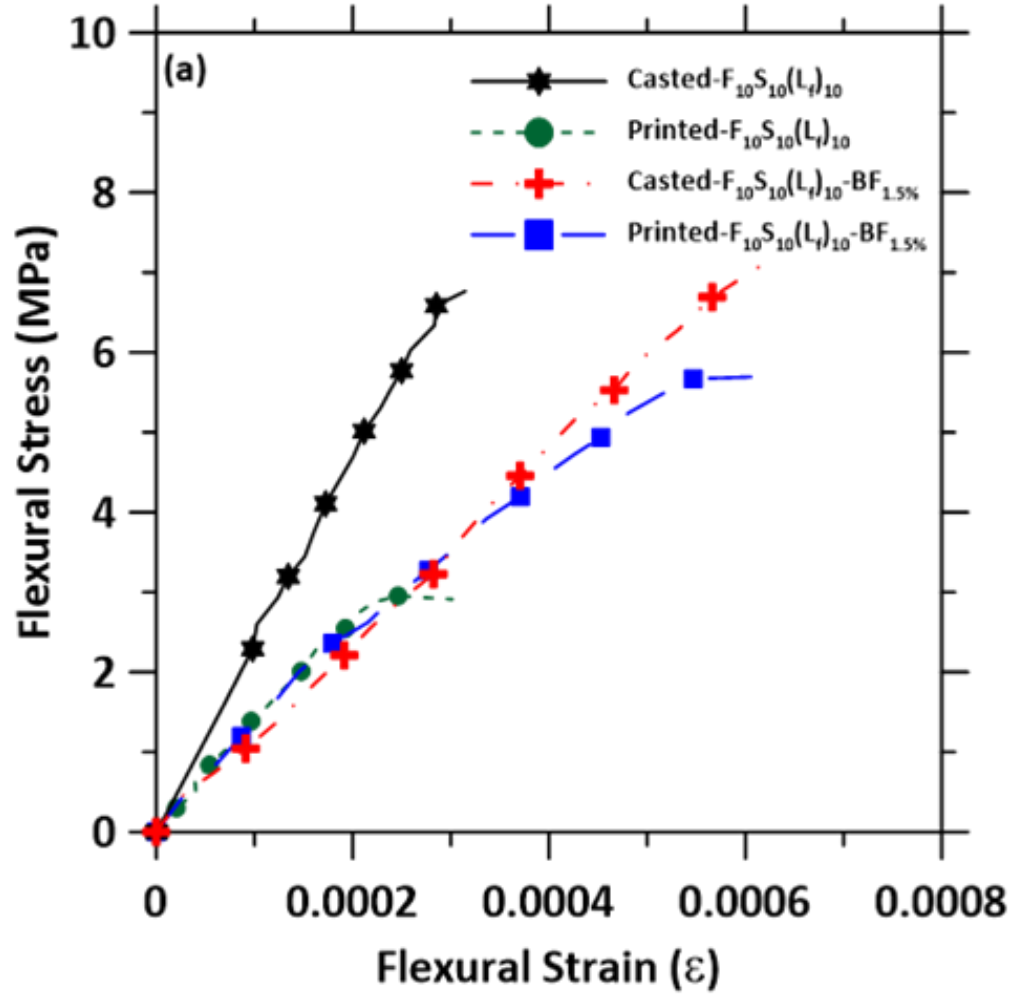
Previous flexural strength (low dosage)



Flexural strength



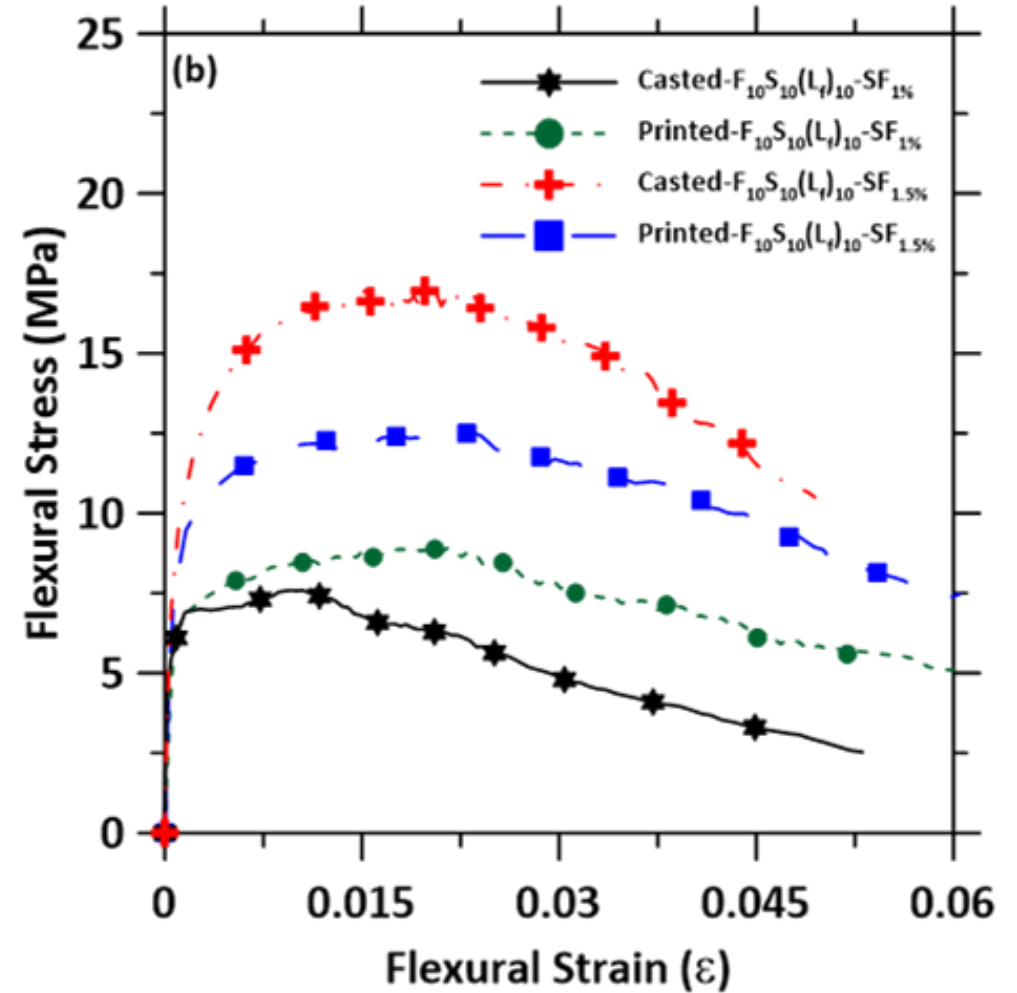
Flexural response





Flexural response

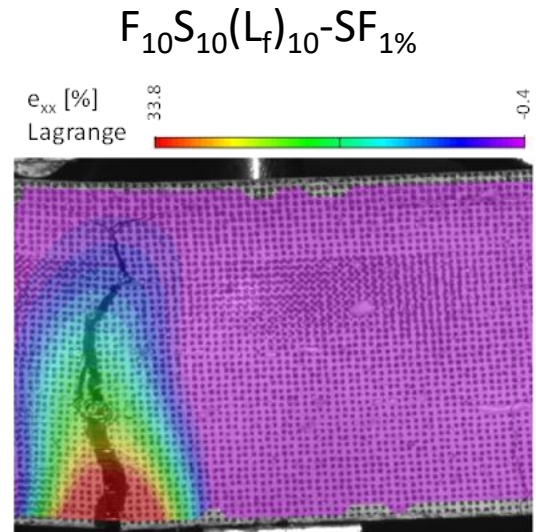
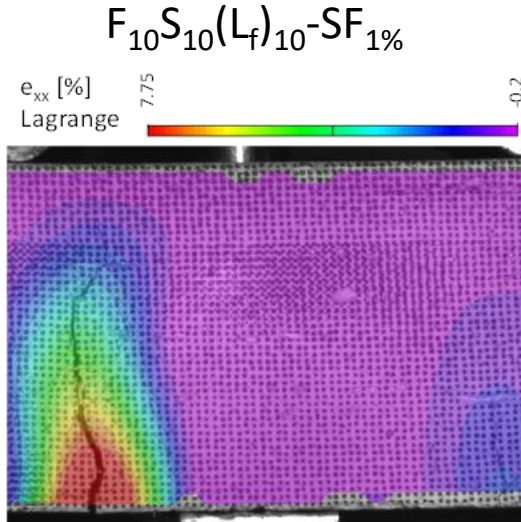
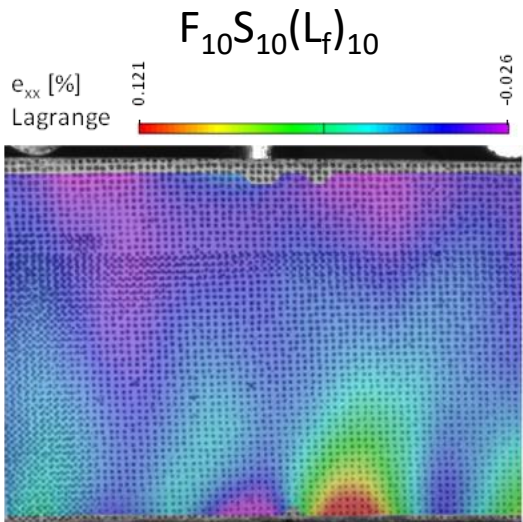
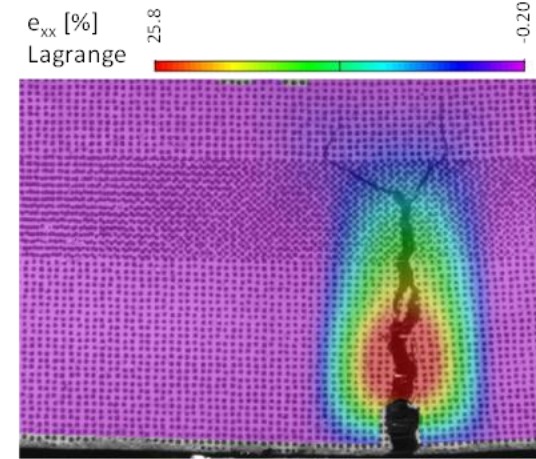
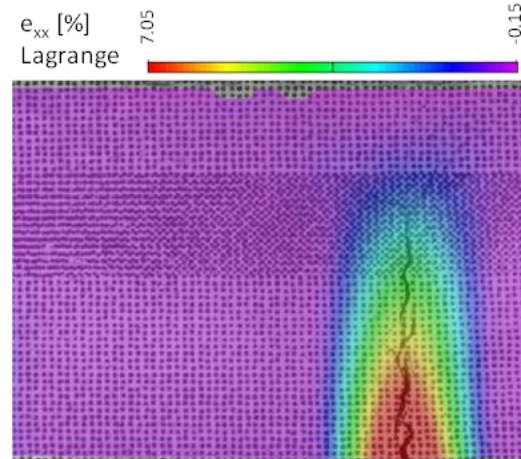
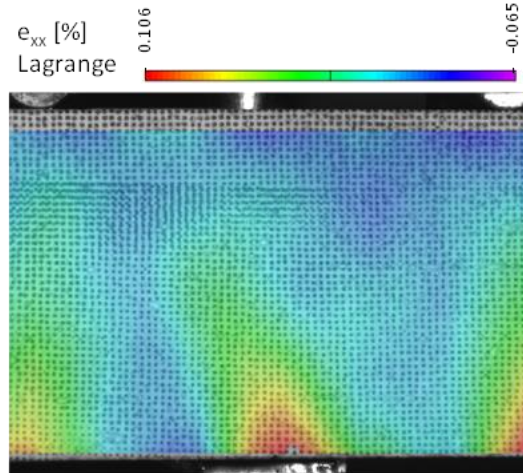
- Presence of basalt fiber resulted in higher flexural strain at failure
- Basalt underperforms at high fiber content (due to less tensile capacity and brittle nature)
- Printed steel fiber at 1% outperformed mold casted specimen with 1% steel fiber (attributed to alignment of fibers along the length resulting in proper crack bridging)
- Steel fiber providing high ductility, load carrying capacity increases still after the mortar matrix cracks



DIC peak and post peak analysis

At peak load

At 4 mm central deflection



$F_{10}S_{10}(L_f)_{10}-BF_{1.5\%}$

$F_{10}S_{10}(L_f)_{10}-SF_{1.5\%}$

$F_{10}S_{10}(L_f)_{10}-SF_{1.5\%}$



Conclusion



- Enhancement of mechanical response of 3D printed element can be achieved through simpler methods
- Chopped fiber in concrete mortar used for printing helps enhance mechanical response*
- Tendency of fiber to orient in print direction could be used to advantage

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An NSF AccelNet
Collaborative Effort





QUESTIONS?