

# UHPC Alternative for the West Wilson Bridge

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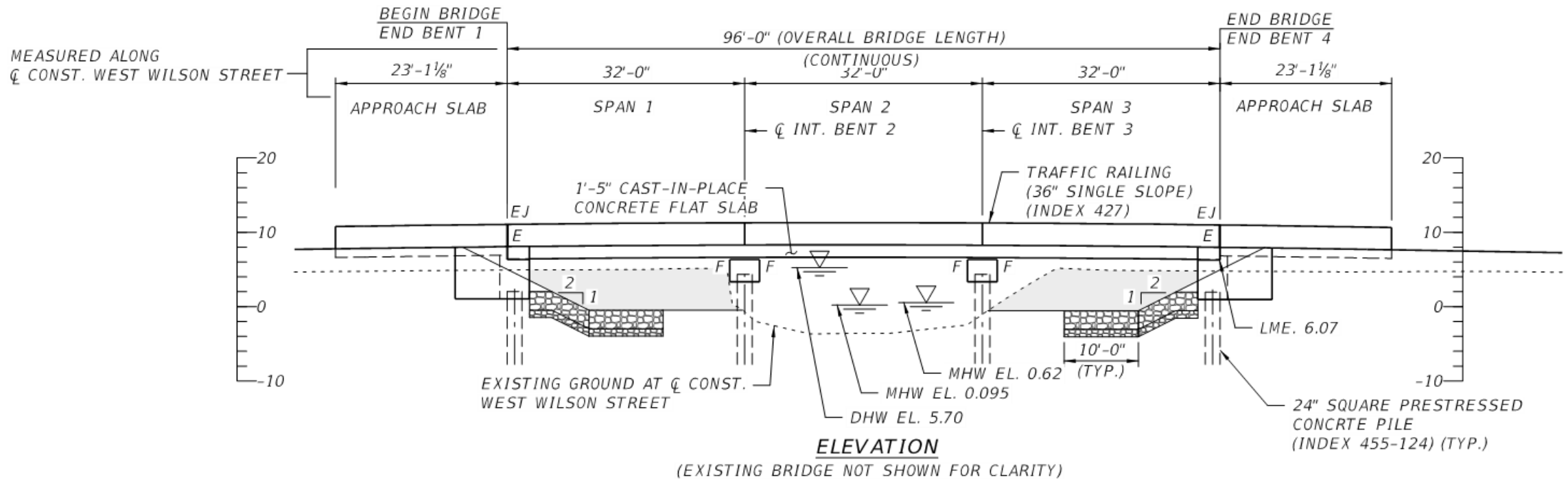


THE WORLD'S GATHERING PLACE FOR ADVANCING CONCRETE



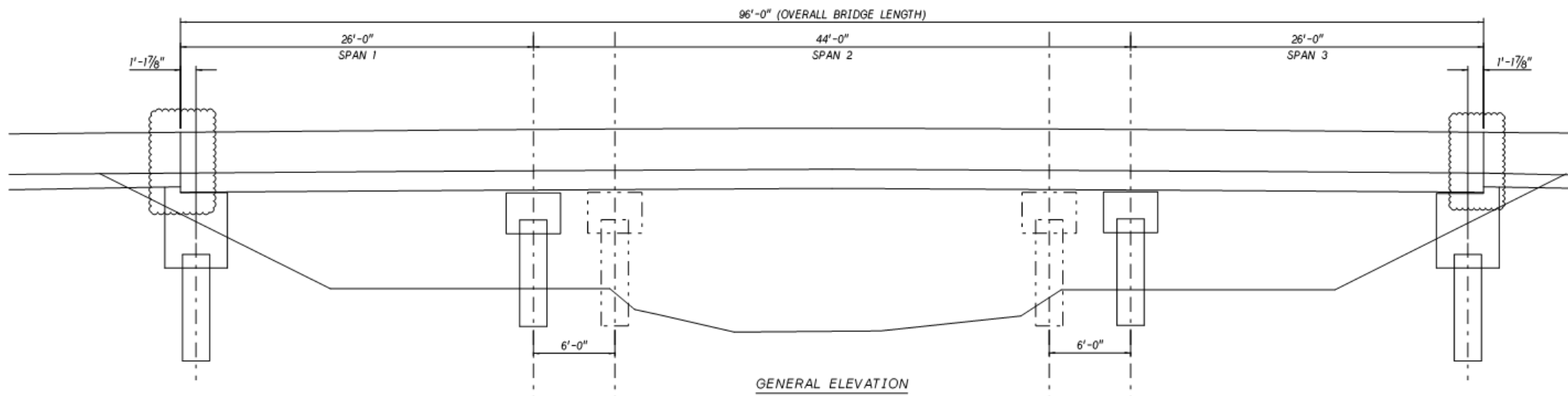
# Original Cast-in-Place Slab Bridge

- 2% superelevation; 30° skew

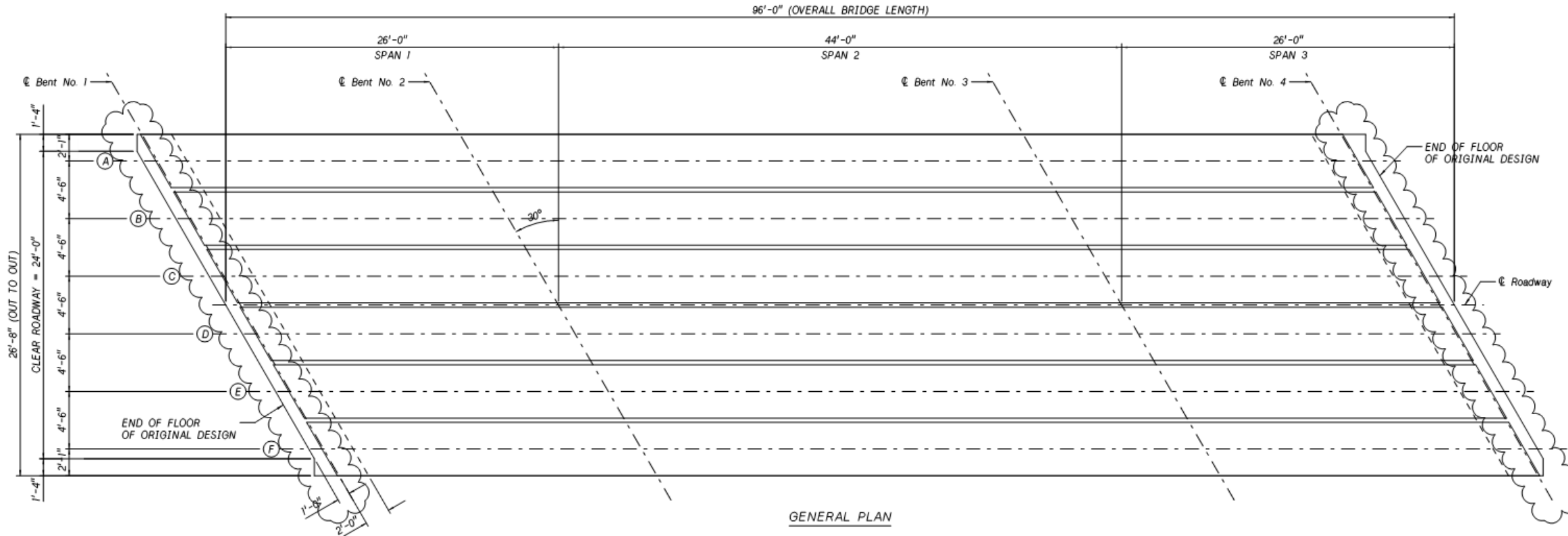


# Proposed UHPC Bridge Elevation

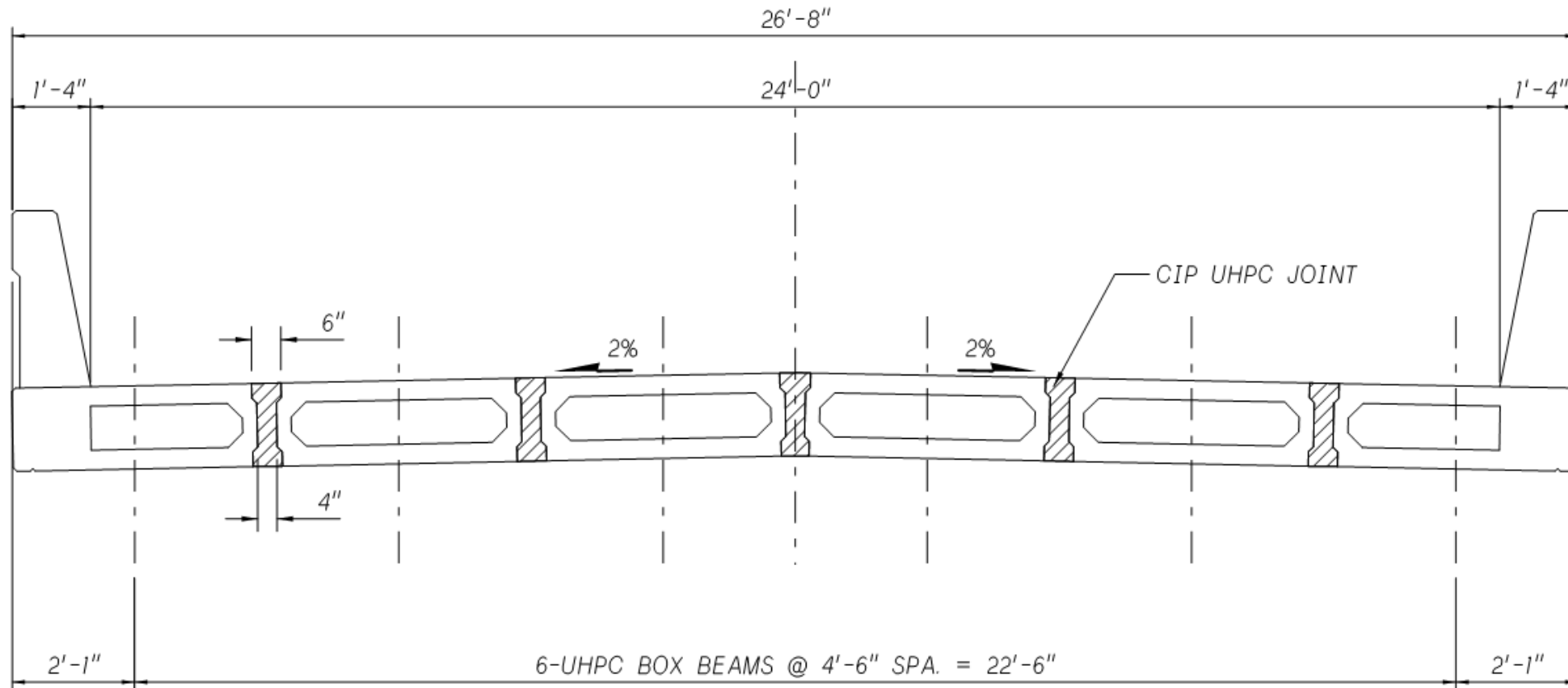
- The piers are moved 6 ft away from the center.
- The box beam length covers the entire bridge length of 96 ft.
- Three spans: 26-44-26 ft



# Proposed UHPC Bridge Plan



# UHPC Bridge Cross Section

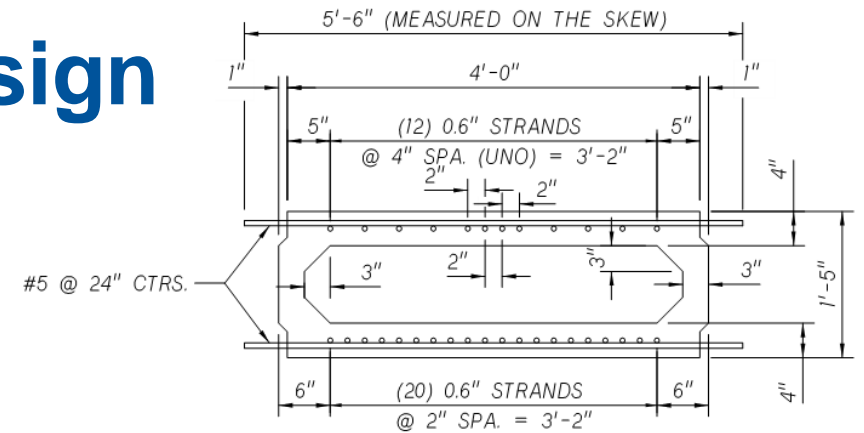


# UHPC Box Beam Design

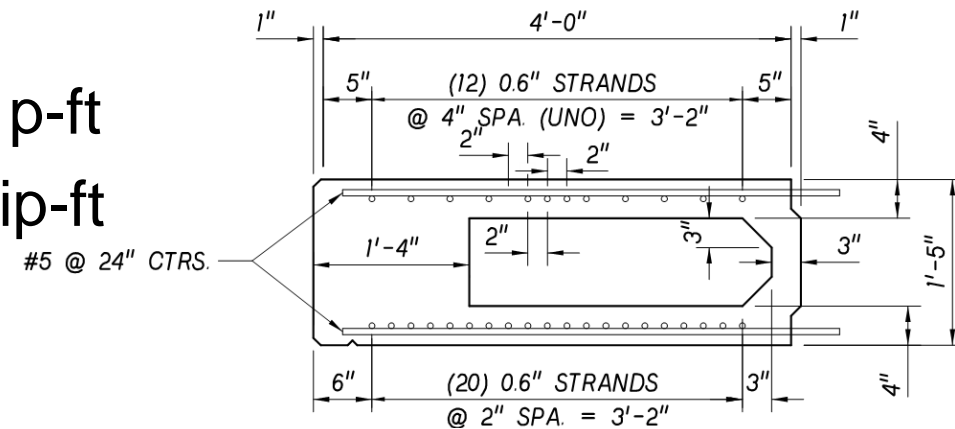
- 20-0.6" bottom strands
- 12-0.6" top strands
- No shear reinforcement!

## Design

- Positive moment :  $\phi M_n = 1,369 \text{ kip-ft} > M_u = 304 \text{ p-ft}$
- Negative moment:  $\phi M_n = 877 \text{ kip-ft} > M_u = 629 \text{ kip-ft}$
- Shear:  $\phi V_n = 179 \text{ kip-ft} > V_u = 138 \text{ kip-ft (at pier)}$



Interior Typical Section



Exterior Typical Section

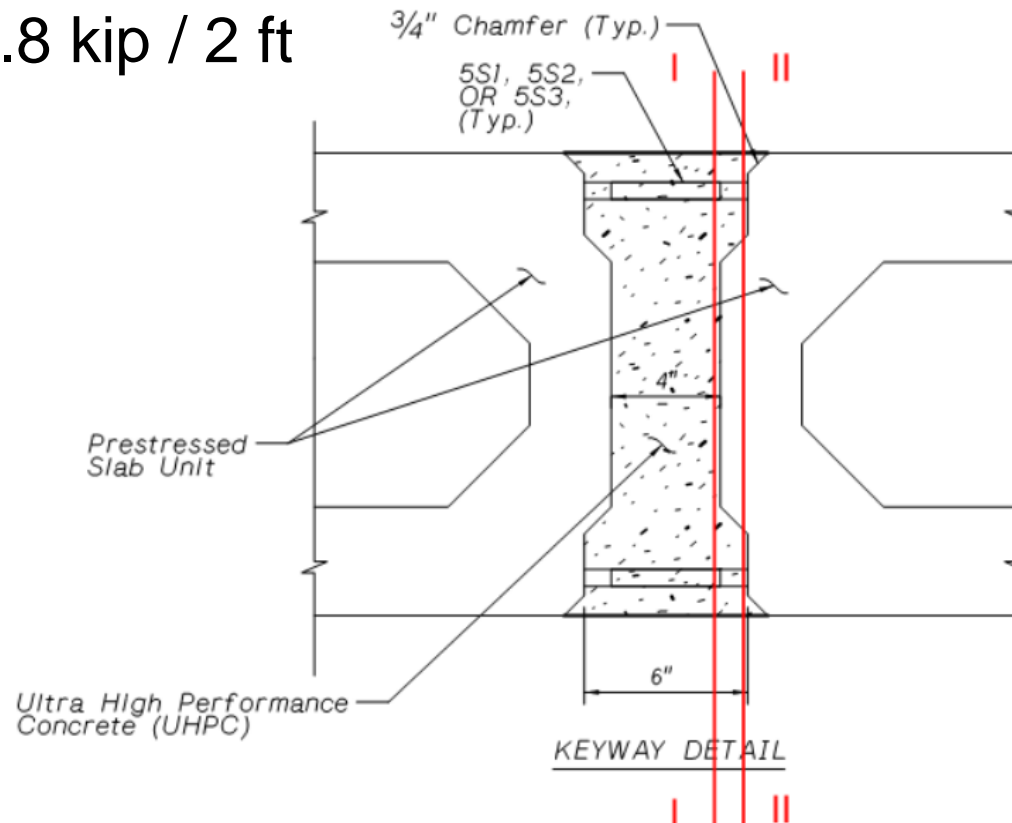
# Longitudinal Joint, Moments

- Finite element modeling was completed to determine ultimate tension forces between adjacent boxes
- Ultimate tension force,  $T_u = 8.84$  kip/ft
- $A_s$  required  $T_u/0.9/f_y = 0.16$  in.<sup>2</sup>/ft
- Provided #5 @ 2 ft =  $0.31/2 = 0.16$  in.<sup>2</sup>/ft OK



# Longitudinal Joint, Vertical Shear

- Ultimate interface shear = 22.8 kip / 2 ft
- At Section I-I:
  - $V_{ni} = 364$  kip / 2 ft (controls)
- At Section II-II:
  - $V_{ni} = 423$  kip / 2 ft





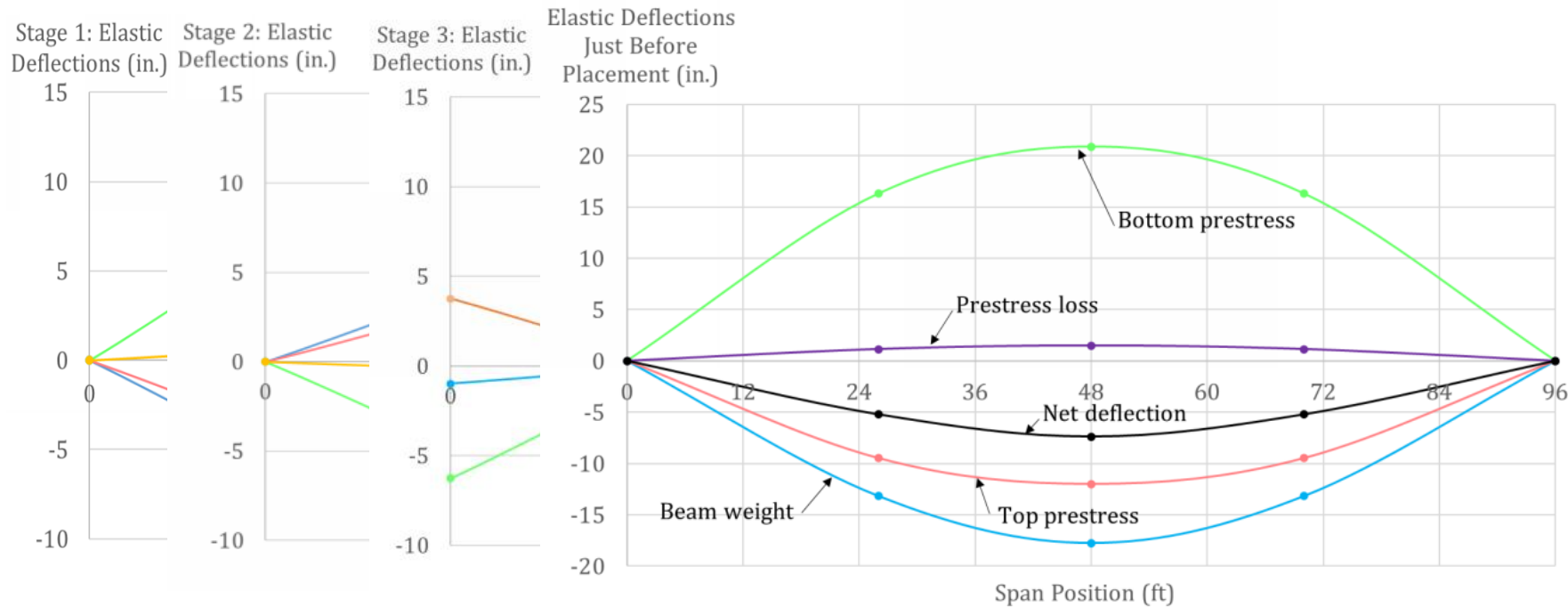
# Assumed Construction Schedule

- Establishing the construction sequence was important to determine deflection and camber at each stage
- Targeted camber = 4 in.

Step	Concrete Age (days)	Location	Support conditions	Event
1	1	Yard	2, 91.94 ft	Right after release, set in the yard on dunnage
2	120	Shipping	2, 91.94 ft	Ship to bridge site
4	120	Jobsite	24.49, 68.49 ft	The beam is set on the pier supports, and does not touch the end bent
5	141	Jobsite	0.48, 24.49, 68.49, 93.46 ft	Cast end bent
6	148	Jobsite	0.48, 24.49, 68.49, 93.46 ft	Joint and barrier concrete are poured/attached
7	20,000	Service	0.48, 24.49, 68.49, 93.46 ft	Final condition



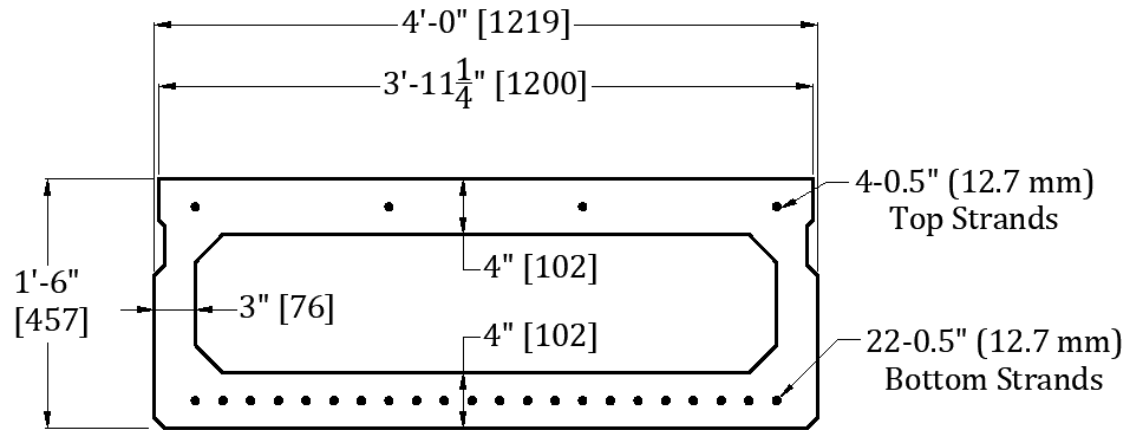
# Camber and Deflection Analysis



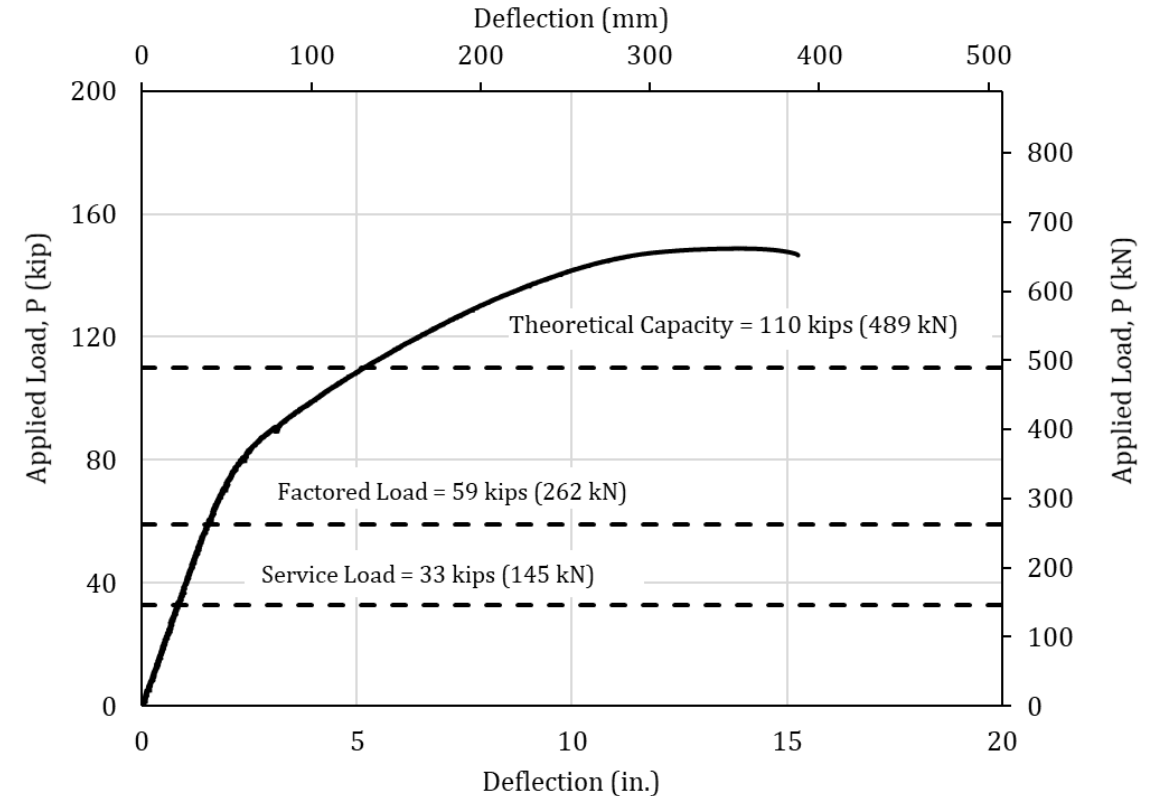
- At final time, net midspan camber = 5.4 in.
- To bring this down to 4 in., an upward load can be applied near the ends of the beams



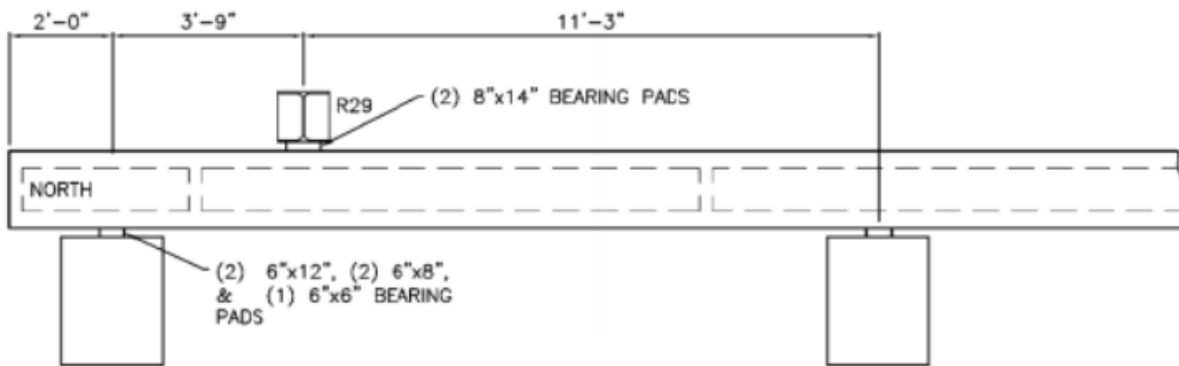
# Experimental Verification - Flexure



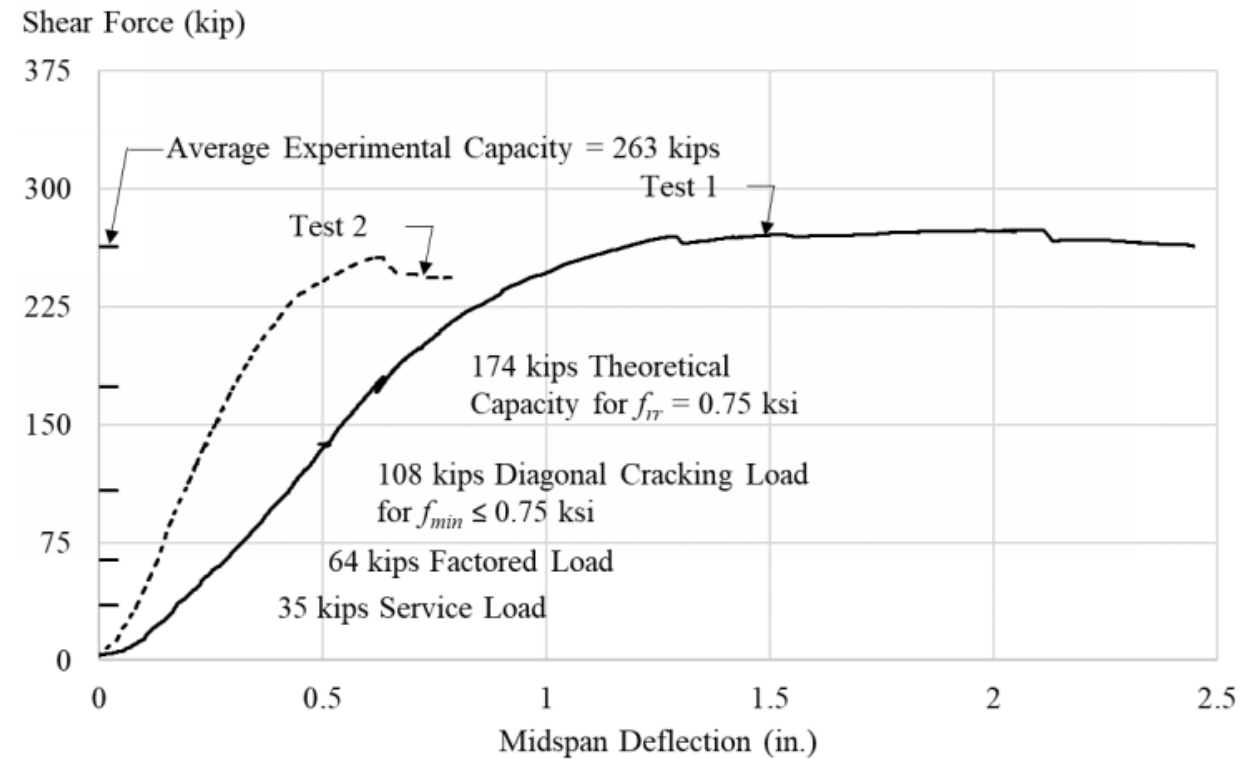
- Experimental/Theoretical = 1.35
- Experimental/Demand = 2.52
- Experimental/Service Load = 4.51



# Experimental Verification - Shear

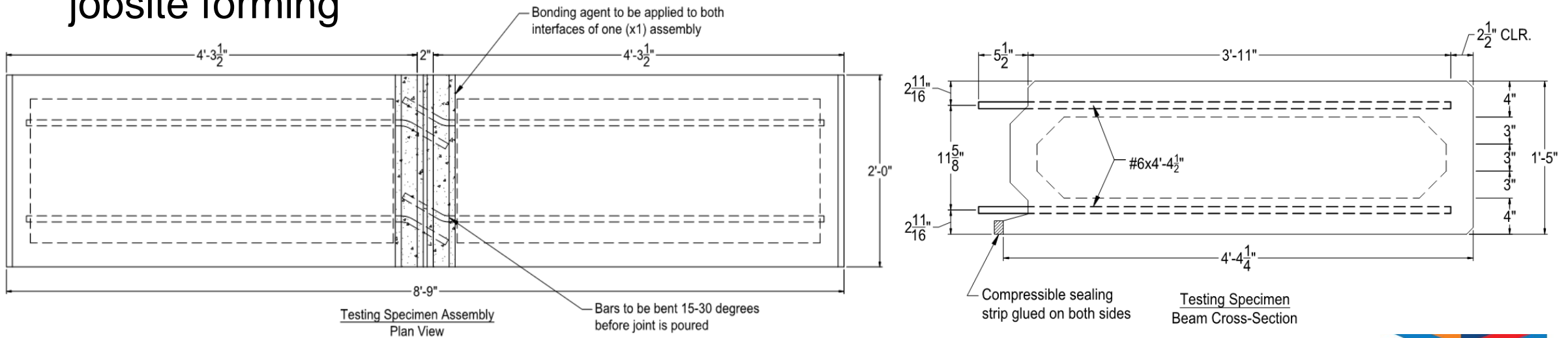


- Experimental/Theoretical = 1.51
- Experimental/Demand = 4.11
- Experimental/Service Load = 7.51



# Experimental Verification – Longitudinal Joint

- Tests were conducted to assess the joint
  - One specimen had a smooth interface, one had a roughened interface
- Note the modified bottom flange, which decreases the amount of required jobsite forming



# Joint Test Results

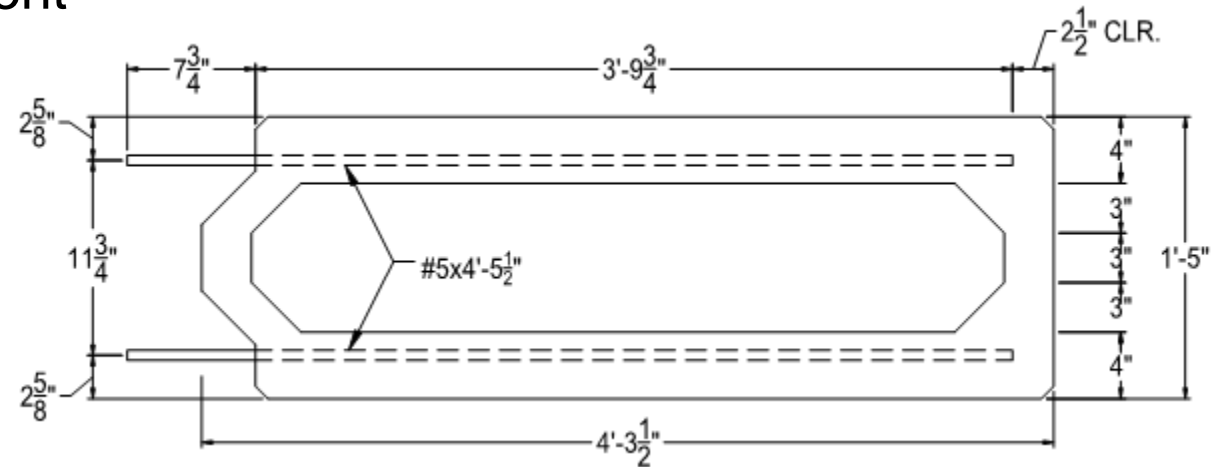
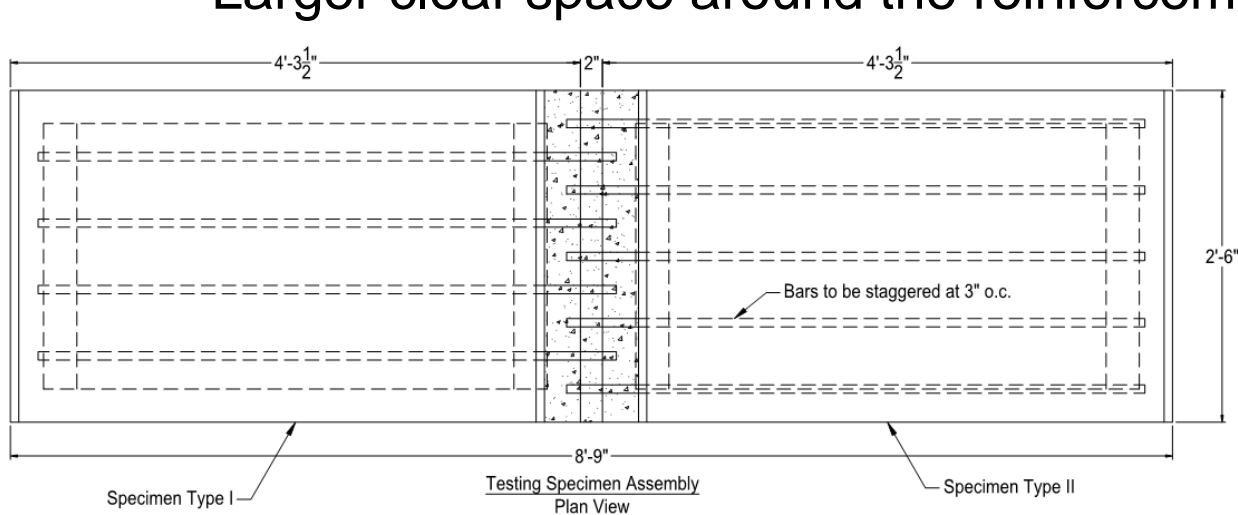
- Specimen failed at the joint
- Bars pulled out, indicating lack of development
- Assumed to be due to both the bending and the lack of clear space around the bars

- Demand = 14.8 kip
- Smooth face capacity = 13.7 kip
- Rough face capacity = 18.4 kip



# Future Testing

- Two more sets of specimens have been produced and await testing
  - Straight bars instead of bent
  - Longer embedment length
  - Larger clear space around the reinforcement



# Thank you!

## Questions?

Feel free to email questions at:  
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