

# The Influence of Slag on Reducing Concrete Pavement Joint Deterioration

Jason Weiss and Burkan Isgor  
Oregon State University

October 26<sup>th</sup>, 2020; 7:00-8:00 AM

# Description of the Talk

Presenter: Jason Weiss and Burkan Isgor



Oregon State University  
College of Engineering

Distress has recently been observed in the joints of some concrete pavements, primarily in the wet-freeze states. This distress often begins in longitudinal joints, followed by transverse joints and results in the significant loss of material from the joint area. Although it may only affect approximately 10% of the concrete pavements system-wide, it greatly reduces the service life and increases maintenance costs of the pavements it effects. Primary issues that emerged from studies on this phenomenon include the importance of the timing of joint sawing, the width of the joint opening, degree of concrete or joint sealing, drainage and degree of saturation of the concrete at the joint, quality of the air void system, role of deicing chemicals, quality of curing, and the degree of restraint at the joint. This work will discuss the role of slag and its role in the reduction or mitigation of joint damage.

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Happy Halloween



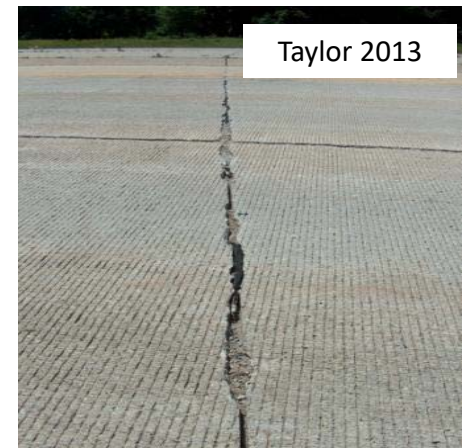
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# Pavement Joints



- The majority of concrete pavement performs well; however some joints are failing/ need repair
- A problem for an otherwise healthy pavement
- The cost is approximately \$1 million dollar per mile



# A Road Map for PRS and PEM Tools & Concerns



TARGET: Improve Long-Term Durability

- Freeze-Thaw
- Salt Damage
- Transport/ Chloride Ingress
- ASR
  
- Shrinkage & Cracking



PRS has focused on the models for performance

Recently we developed many tests that can be standardized (after a year AASTHO SOM has these to move on with through a committee/webinars)

We also have quality control/quality acceptance approaches

Weiss et al. 2015

# A Road Map for PRS and PEM Tools & Concerns



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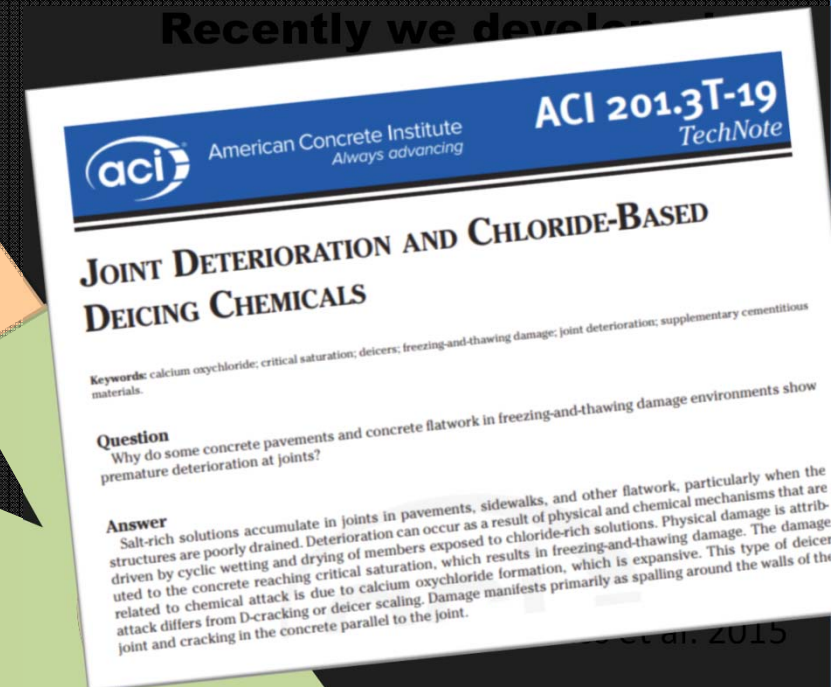
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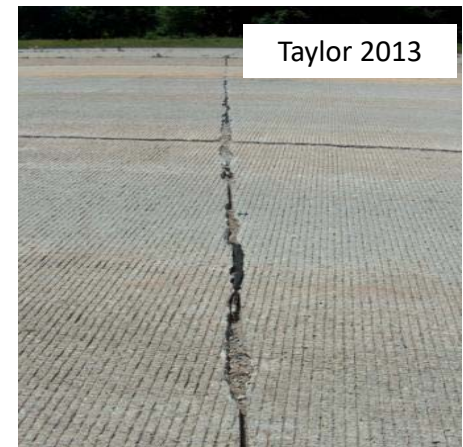
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# Pavement Joints



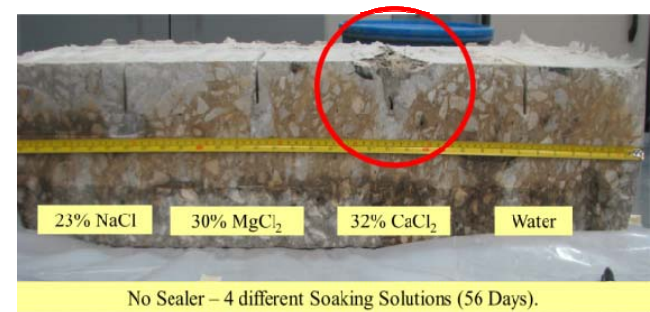
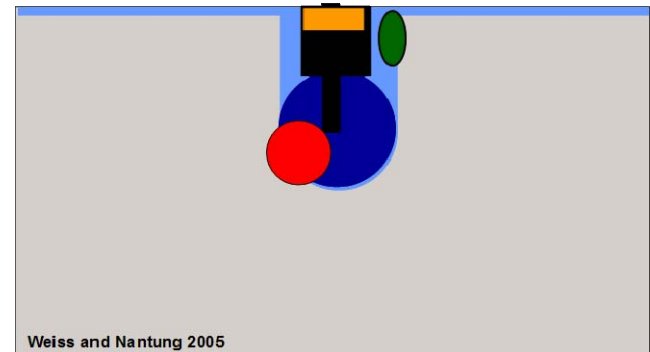
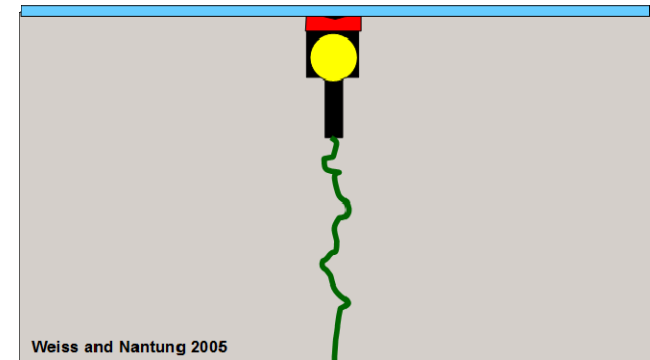
- The majority of concrete pavement performs well; however some joints are failing/ need repair
- A problem for an otherwise healthy pavement
- The cost is approximately \$1 million dollar per mile





# Toward a Working Mechanism

- Examined saw cutting and curing at joints
- Fluid enters joint is trapped
- Saw cut joints not opening to drain (higher early strength, thicker, increased tie bars)
- As a result, fluid can not drain out easily to drainable subbase under the PCCP
- Silicone sealant & backer rod limit drying of trapped fluid which can increase saturation and potentially lead to crystal growth, chemical reaction or pressure



Weiss et al. 2005

# Potential Blame



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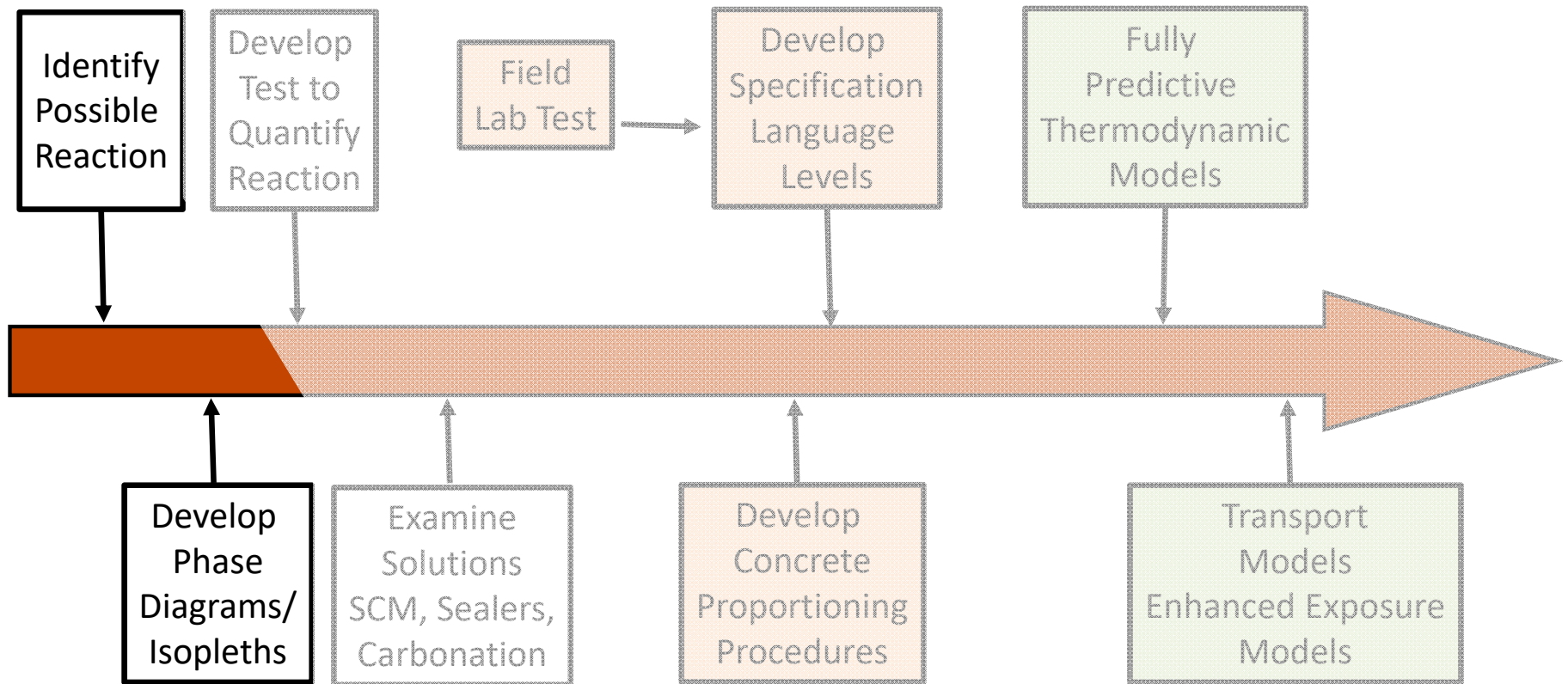
- Contractor/Construction – Overvibration, poor mixture designs, insufficient air
- Pavement Design – too much steel, poor drainage, too thick a pavement
- Deicer supplier – ‘super salts’ ‘eat’ pavements
- Admixture supplier – Bad air systems, ‘new air’
- Hand placement vs machine placement
- Sulfates and ettringite
- Anti-icing deicing practice
- D Cracking, aggregates etc..
- Saw cutting crews/techniques
- Saw cutting vs forming



# Salt Damage

- For approximately 15 years concrete pavements have been observed to show damage at the joints
- Much speculation has been made to the cause of this damage however it seems to now be due in large part of fluid induced freeze-thaw damage and  $\text{CaCl}_2$ ,  $\text{MgCl}_2$  damage
- We have come a long way but have some solutions

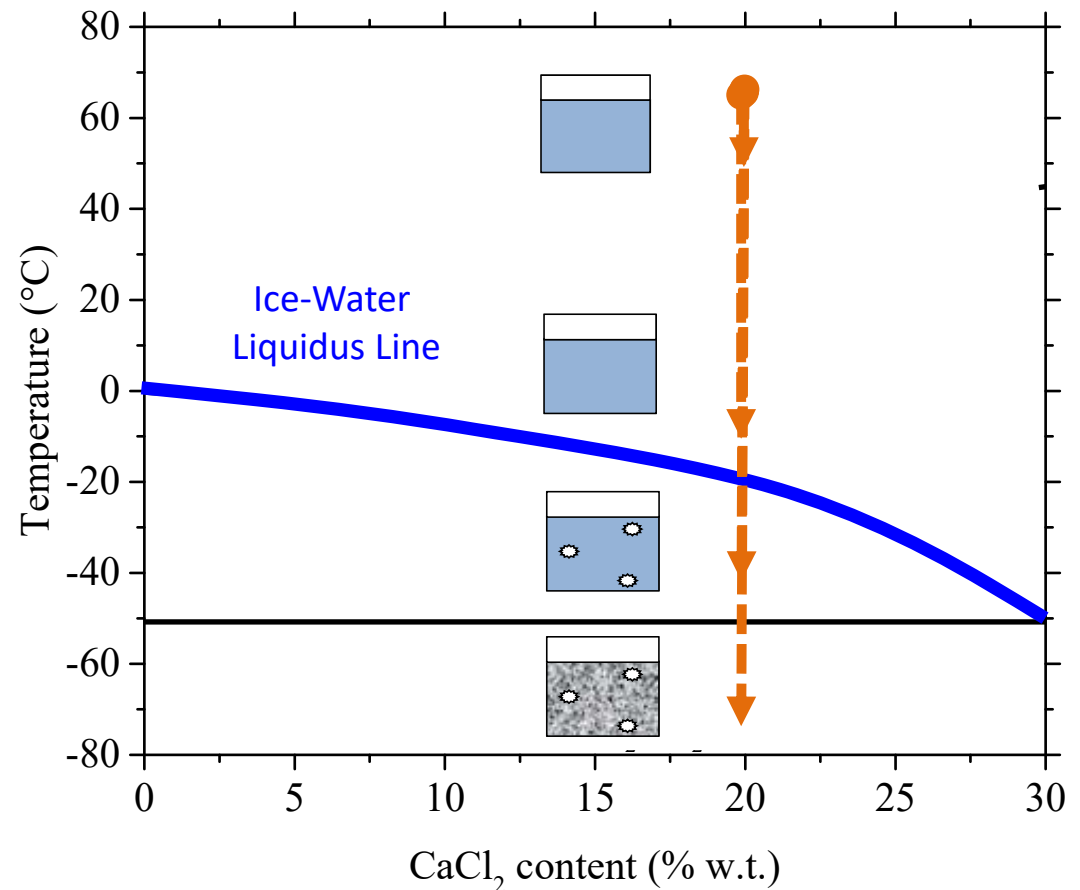
# Overall Timeline



# Phase Diagram For $\text{CaCl}_2\text{-H}_2\text{O}$ Solution



- NaCl salt most common deicers used in practice
- Many times it is blended with  $\text{CaCl}_2$  or  $\text{MgCl}_2$
- We will discuss blends later however for now lets focus on  $\text{CaCl}_2$
- Ice forms as we cross the liquidus line
- All solution solidifies below the eutectic temperature

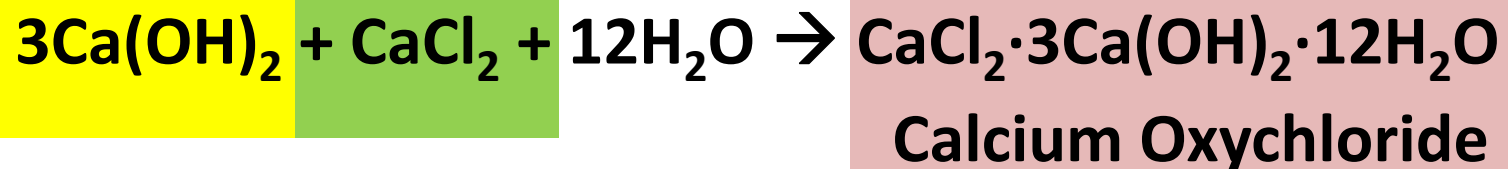


# What Causes the Calcium Oxychloride to Form



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- NaCl salt most common deicer used in practice; many times it is blended with  $\text{CaCl}_2$  or  $\text{MgCl}_2$
- For each system the results are a little different but lets focus on  $\text{CaCl}_2$  as the salt: Reactions occur with  $\text{C}_3\text{A}$ ,  $\text{Afm}$ ,  $\text{Aft}$ ,  $\text{Ca(OH)}_2$
- Kuzel Salt and Friedel Salt – They occur; likely not issue
- Calcium oxychloride forms due to reaction with  $\text{Ca(OH)}_2$

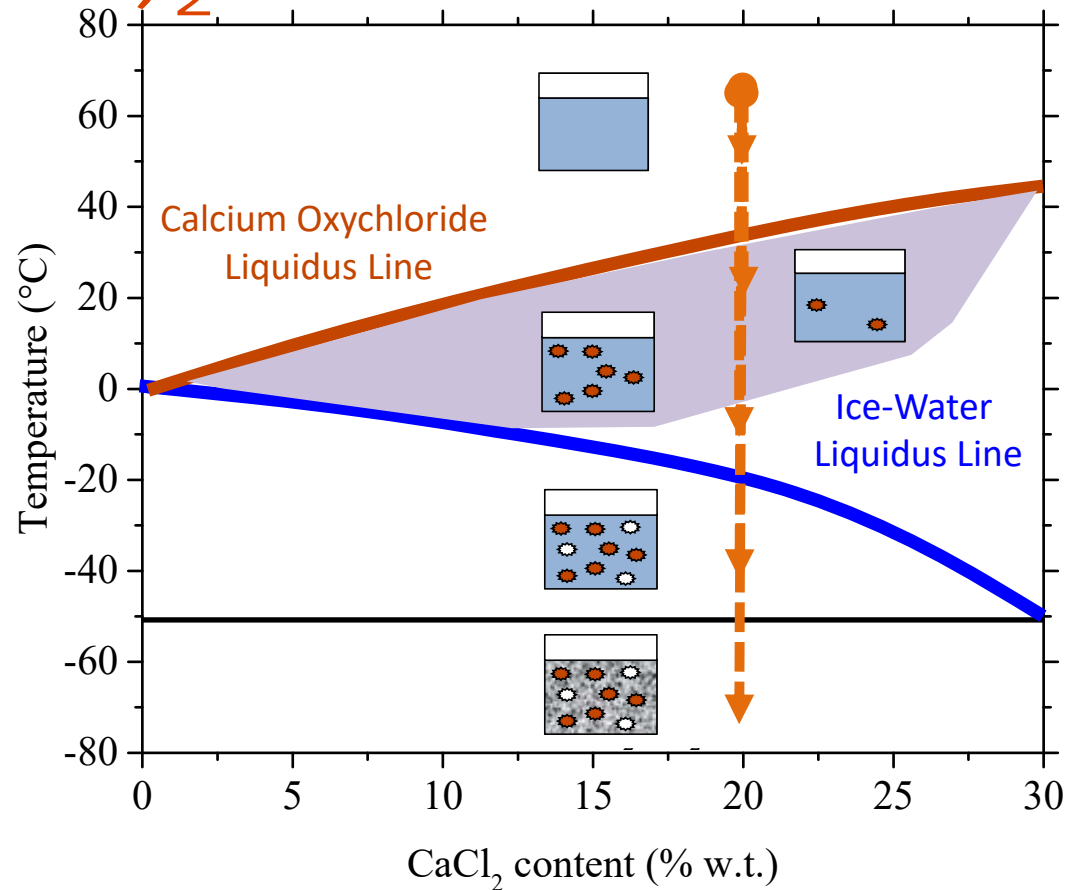


# Phase Isopleth For $\text{CaCl}_2\text{-H}_2\text{O-Ca(OH)}_2$



- However in cement paste there are other species in the pore solution
- Here we see that when the solution contains calcium hydroxide an additional phase forms
- This phase has some implications on the performance of the system

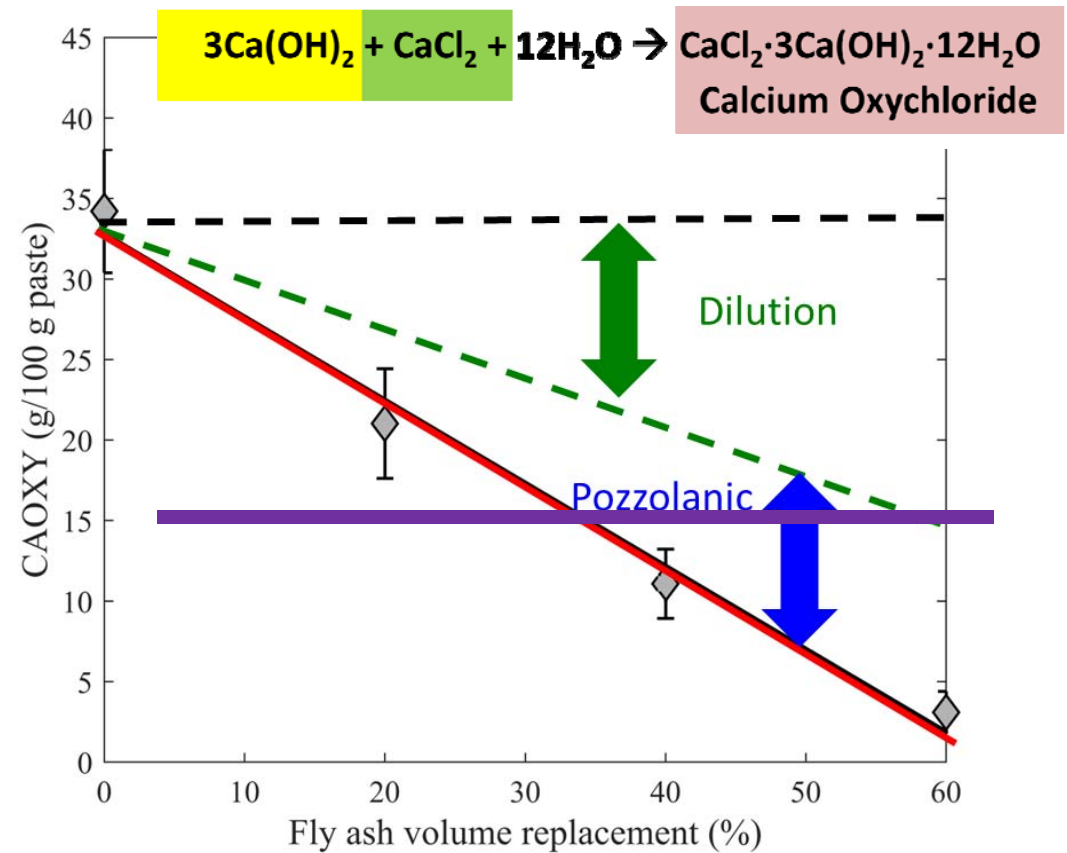
Qiao et al. 2017



# The Role of SCM

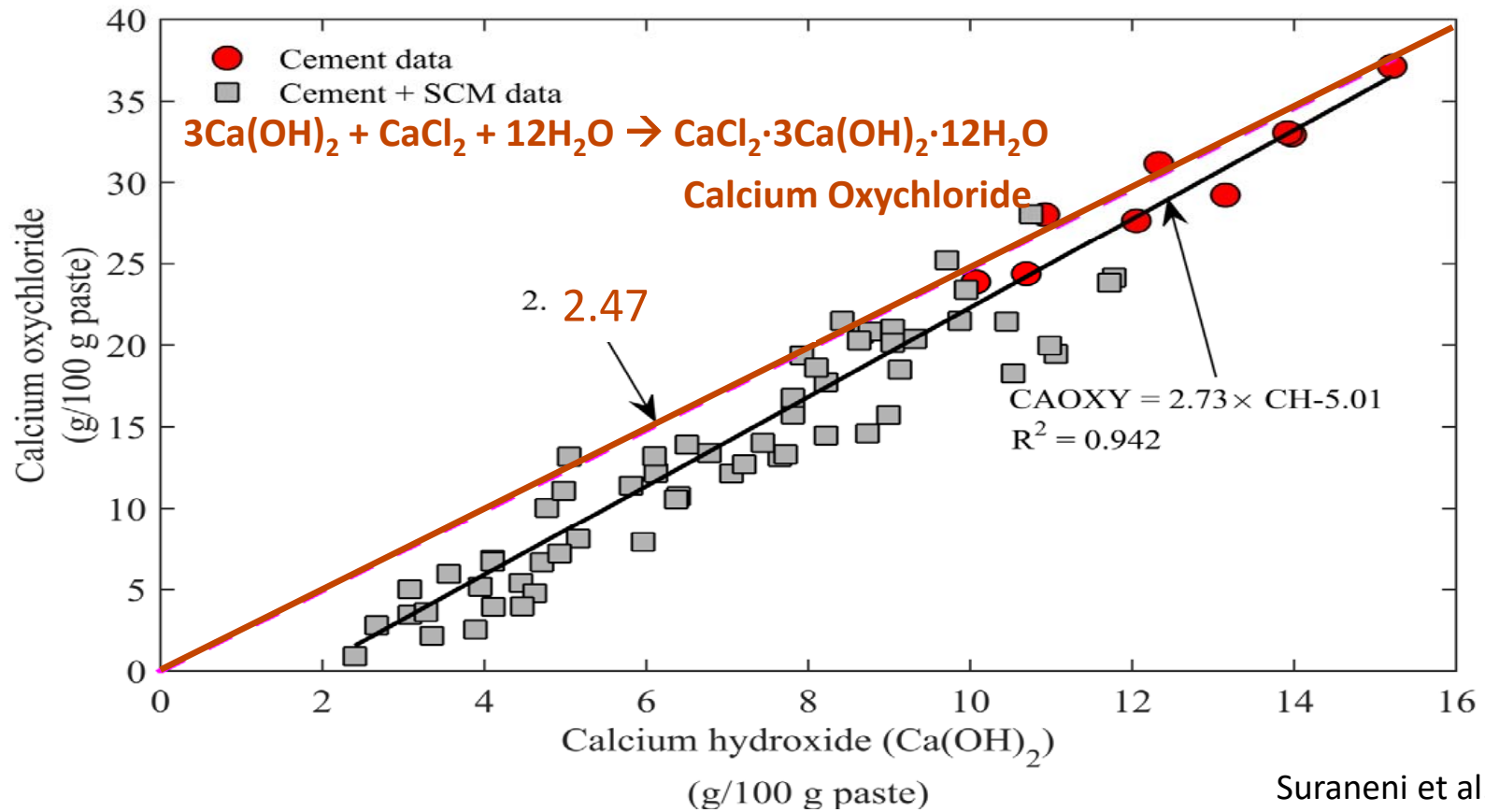


- Effect of Dilution  
(Less CH)
- Pozzolanic Reaction  
(Less CH)
- Limiting Factor
- Mixture Design



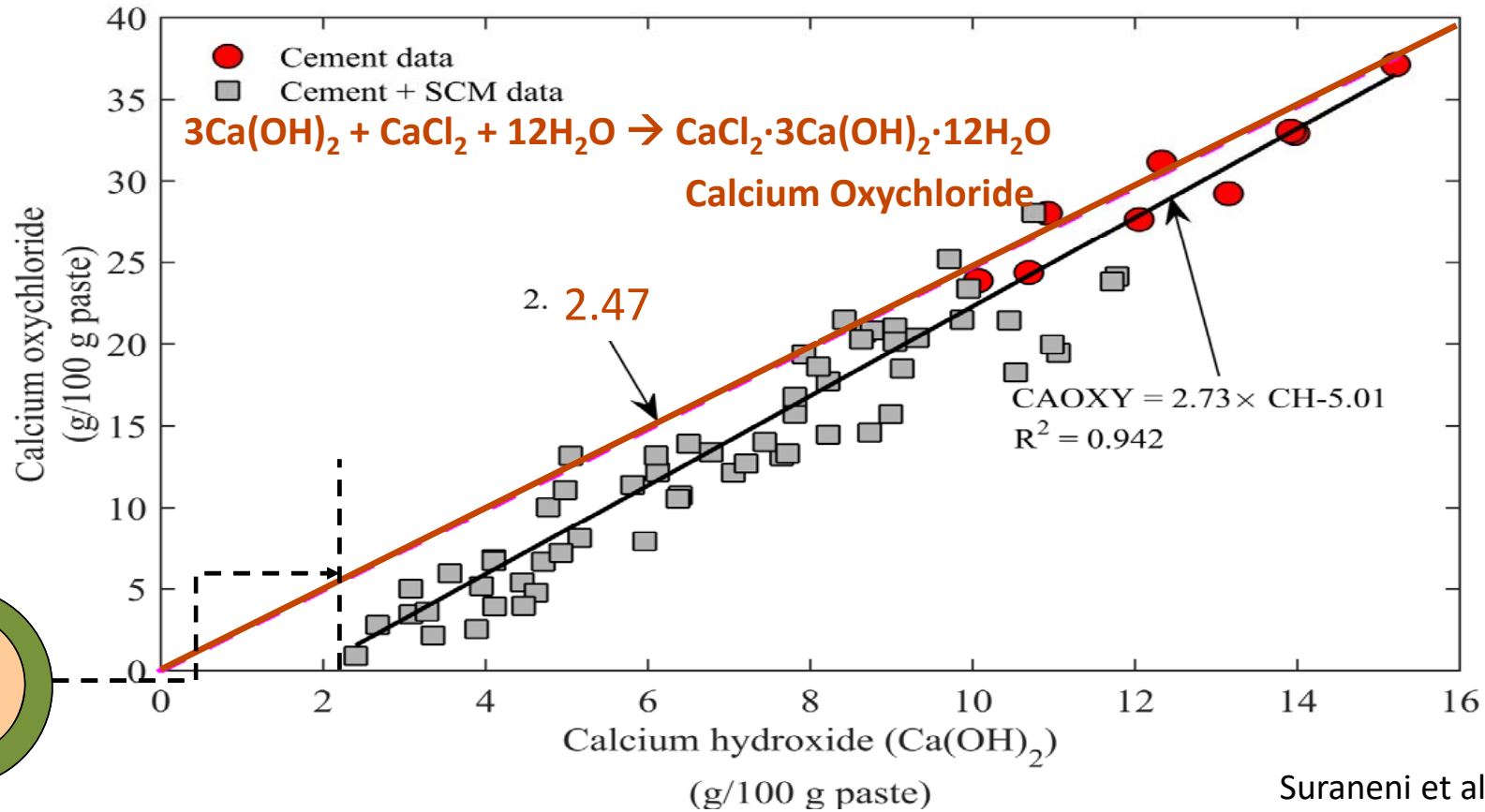


# Relating CH and CAOXY



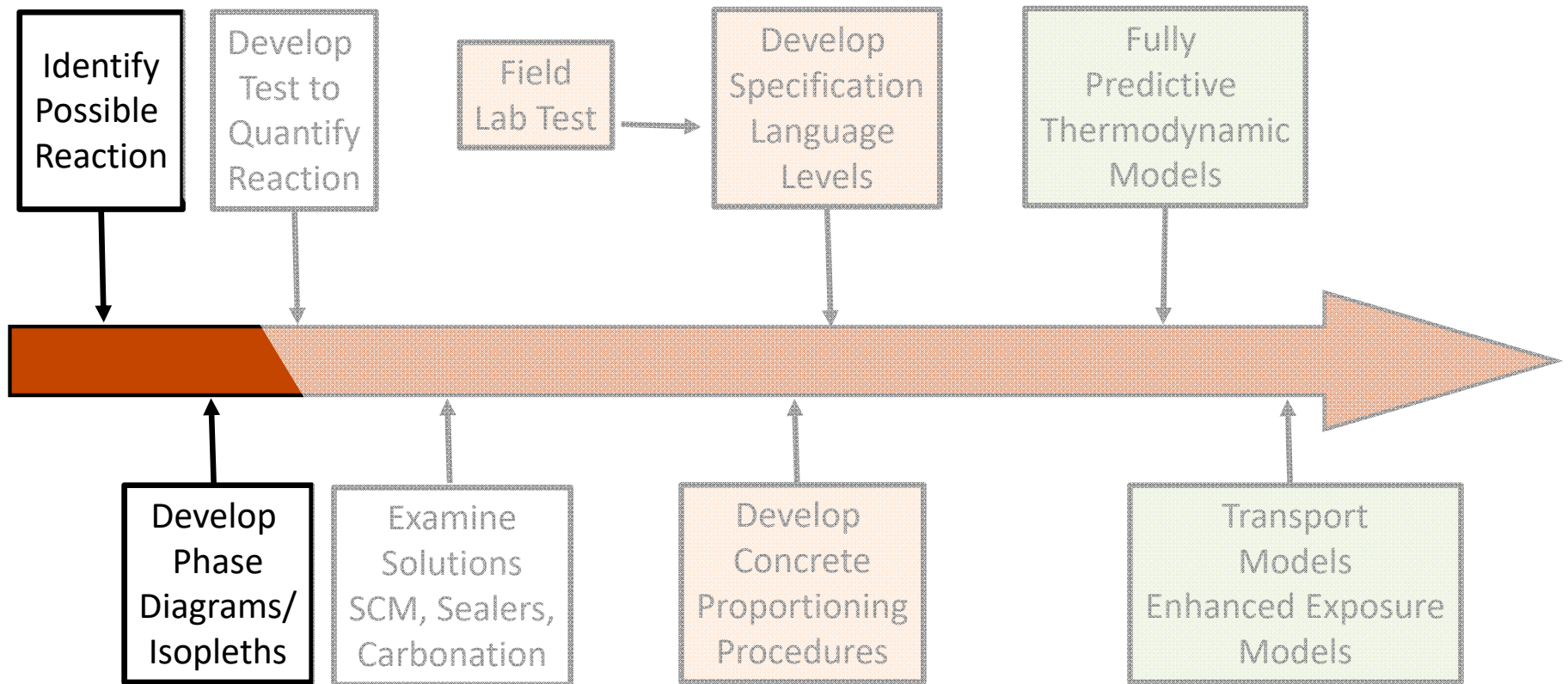
Suraneni et al. 2016d

# Relating CH and CAOXY



Suraneni et al. 2016d

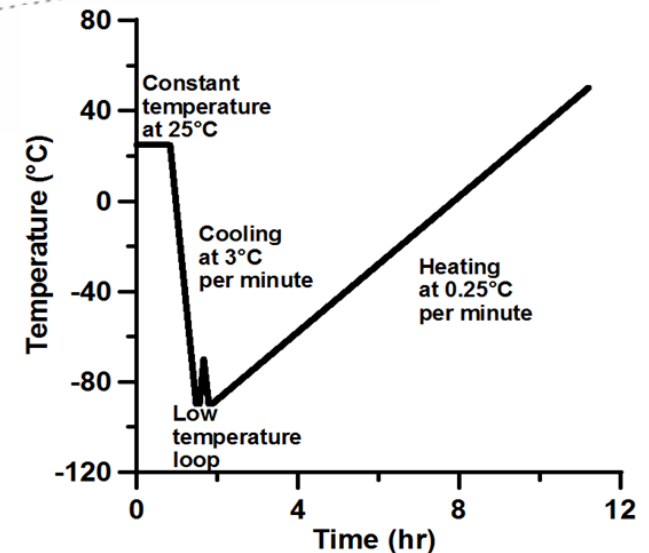
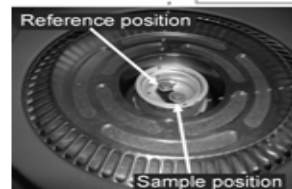
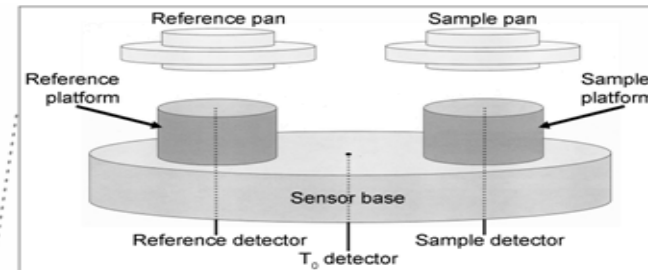
# Overall Timeline



# Test - AASHTO T365



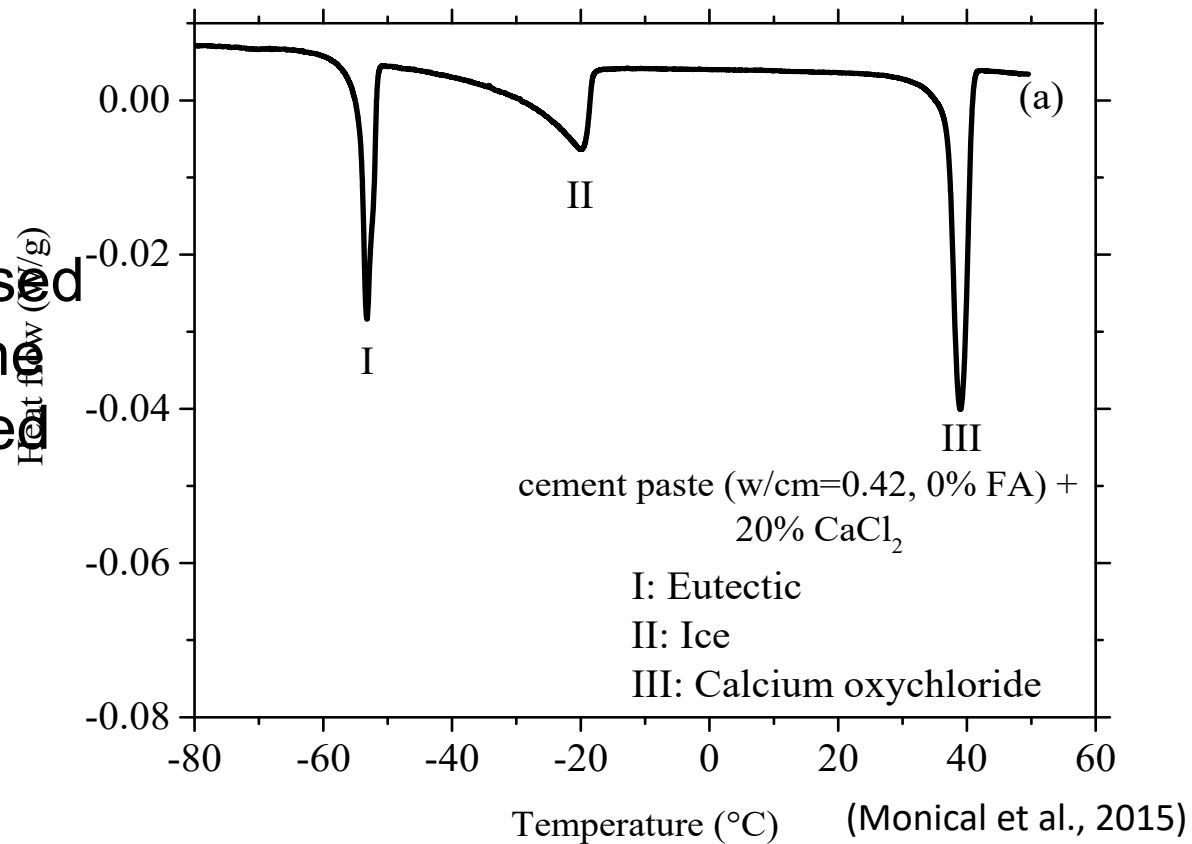
- Cement paste is ground and placed in a salt solution.
- Pan is moved into the cell.
- Thermal Cycle to cause CaOxy to form and we can quantify using heat



# A Test to Quantify Damage (LT-DSC)



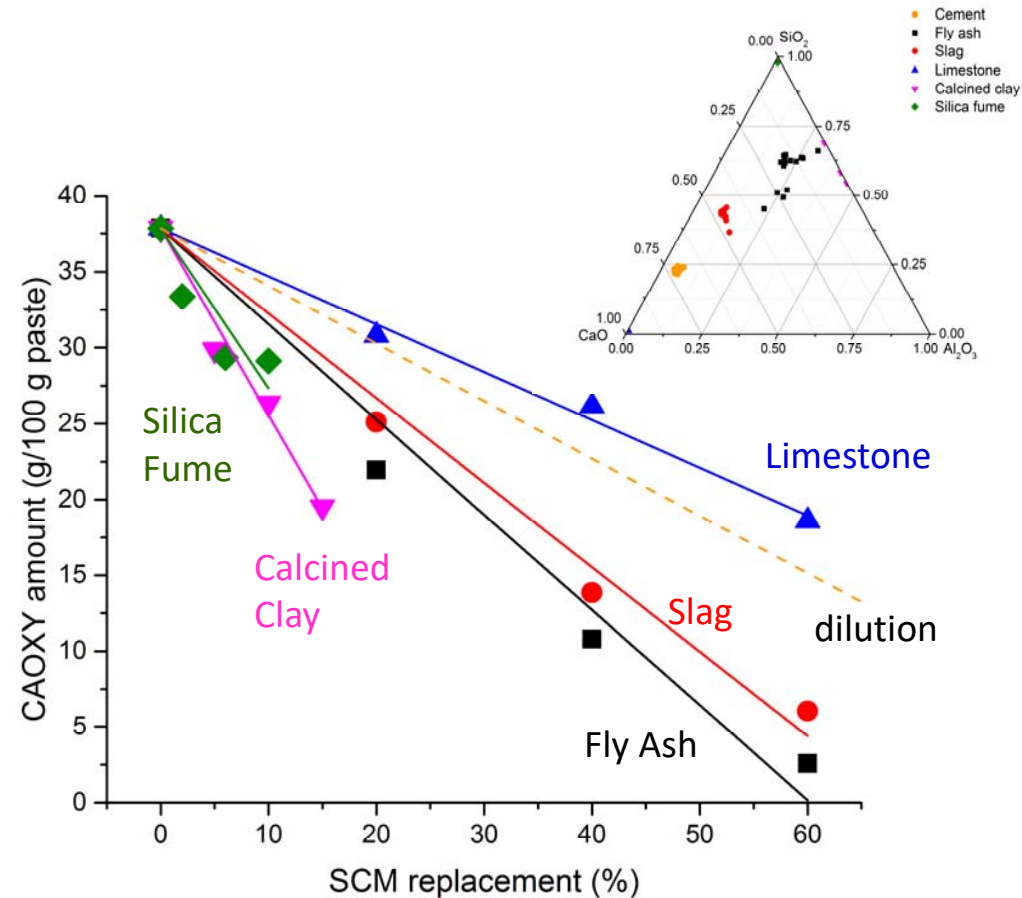
- Low Temperature – Differential Scanning Calorimeter (LT-DSC)
- Temperature is decreased from 50 °C to -80 °C, the sample is then re-heated
- Uses powder with  $\text{CaCl}_2$
- Notice heat flow peaks at various phase formations



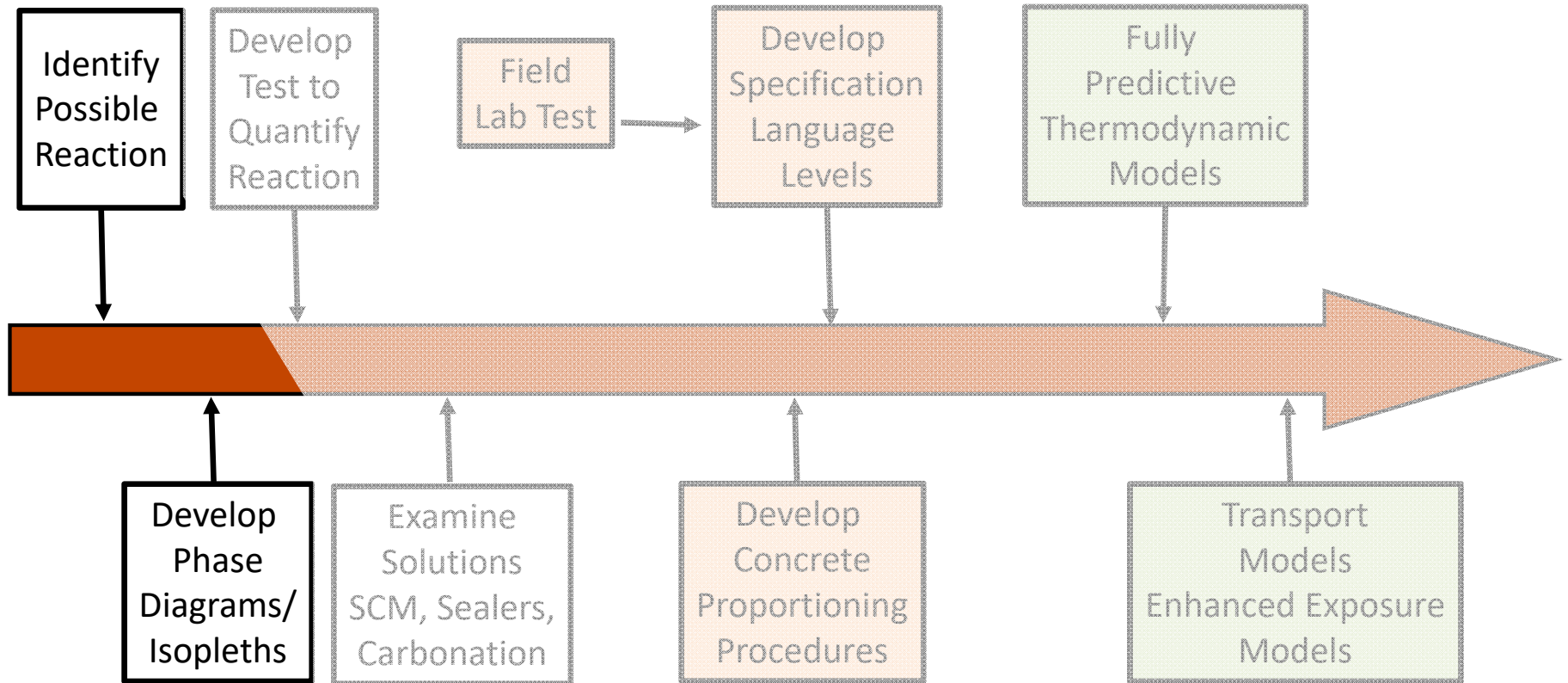
# CH Reduces with Slag



- Its interesting to note that the use of slag reduces CH
- As a result the CaOxy is expected to be reduced
- This is interesting as slag is not a pozzolan



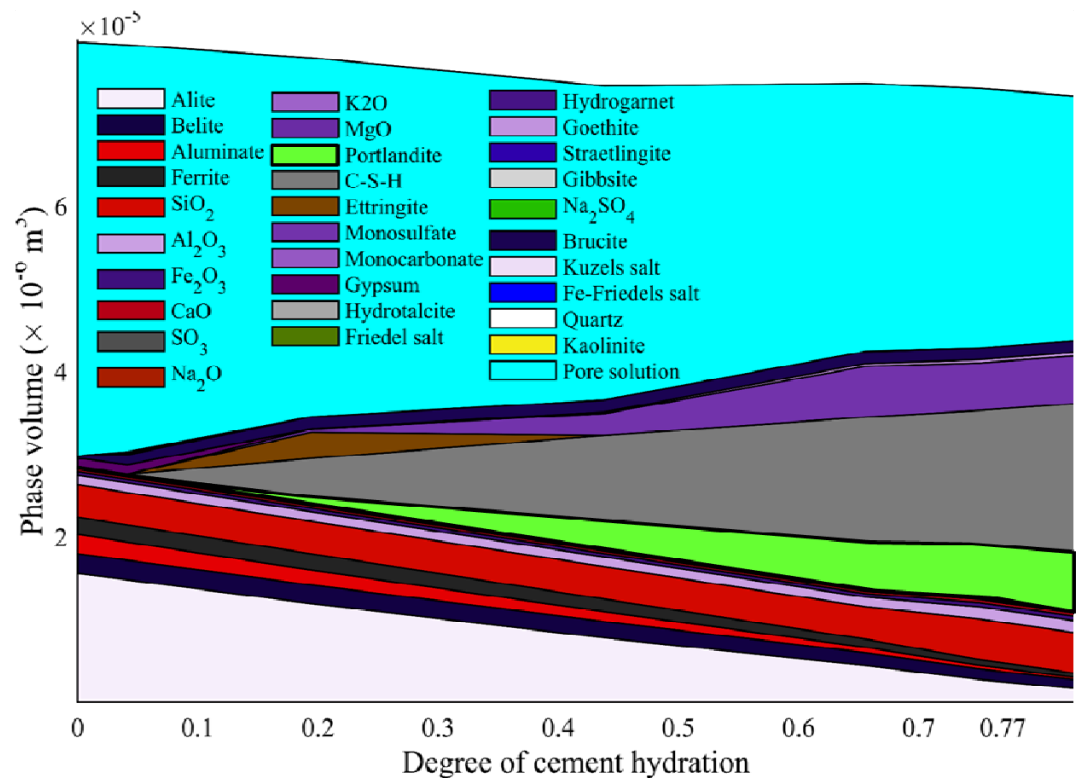
# Overall Timeline



# Thermodynamic Model



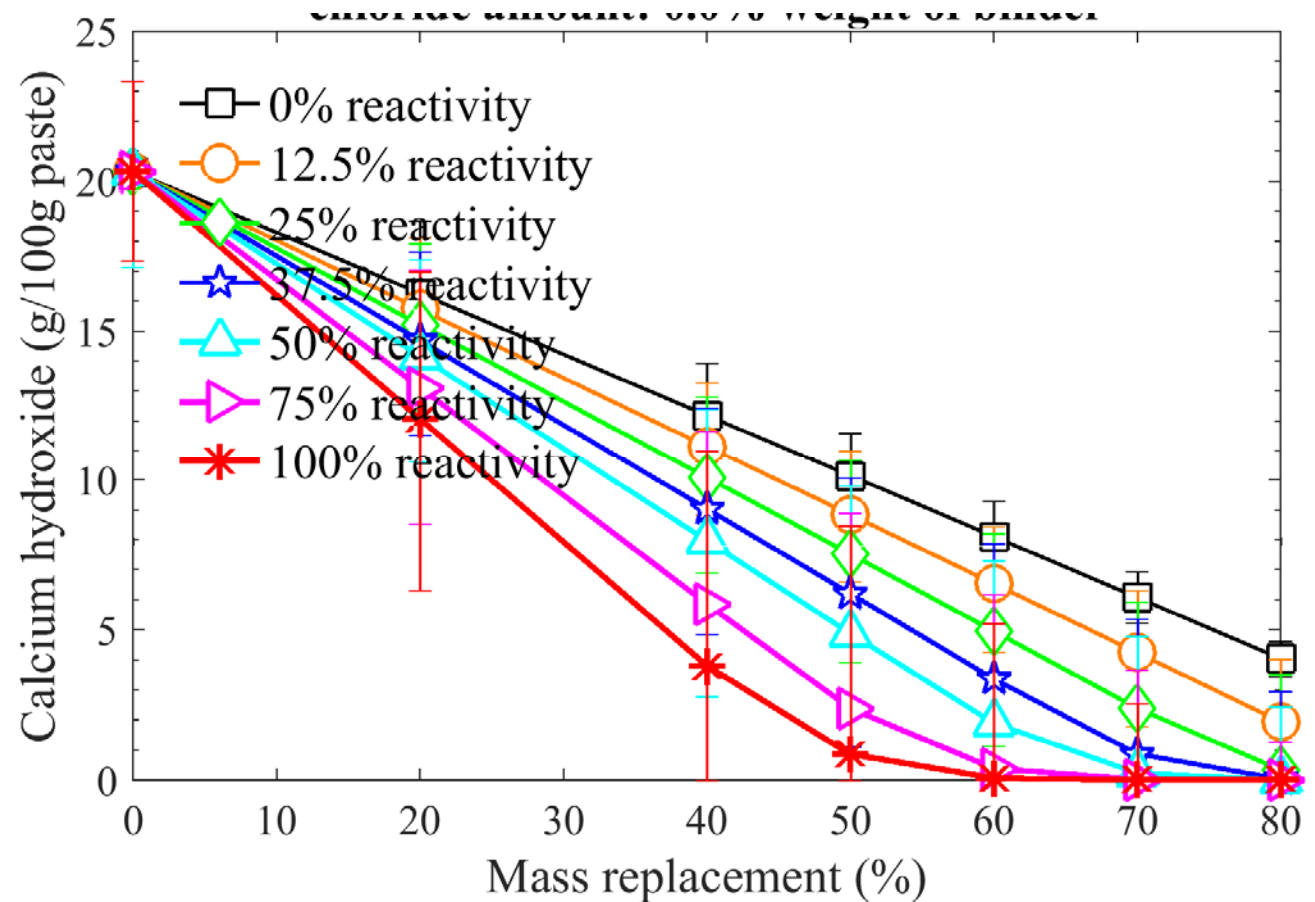
- Using GEMS to predict the reacted products
- Specifically examining the CH production





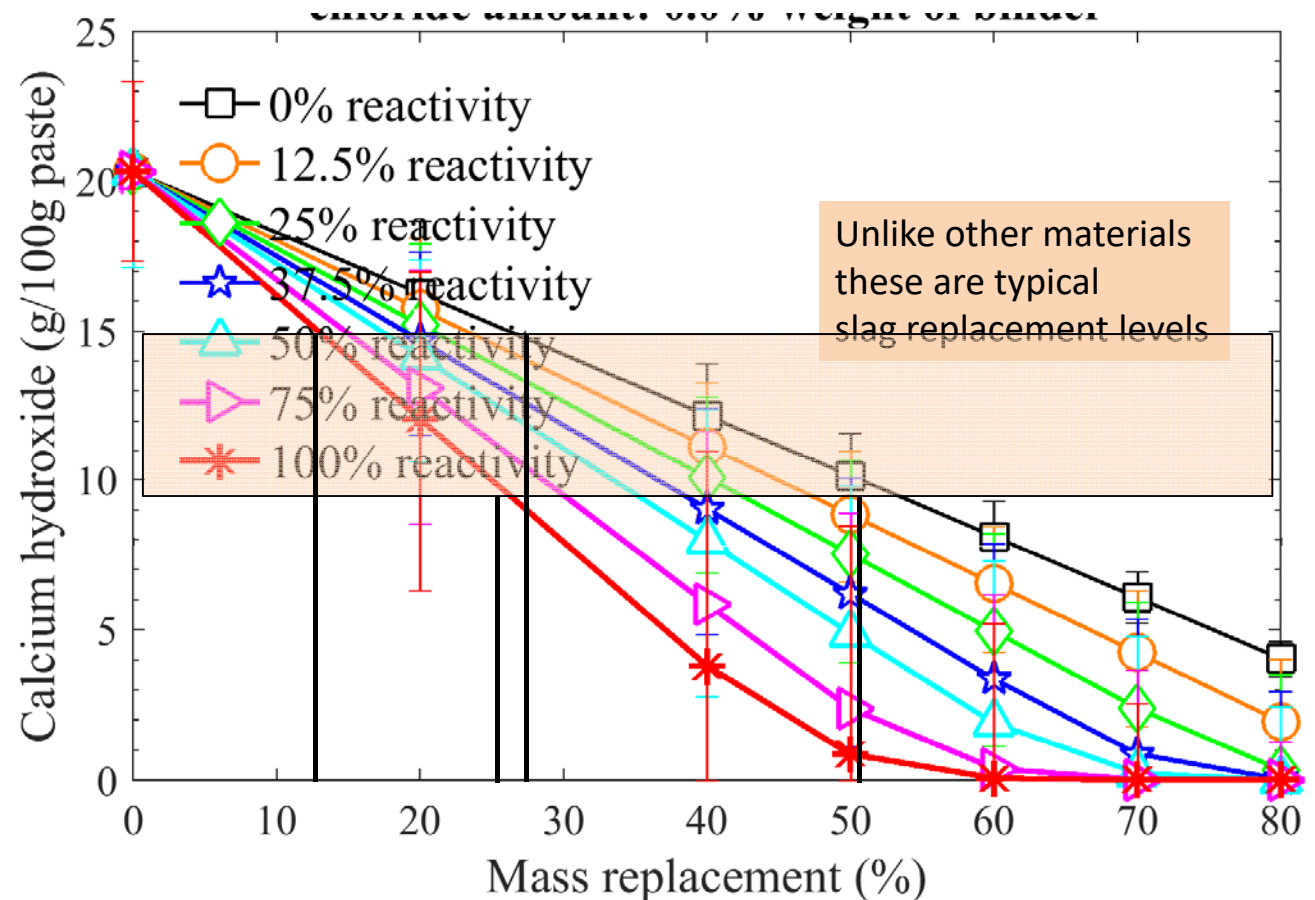
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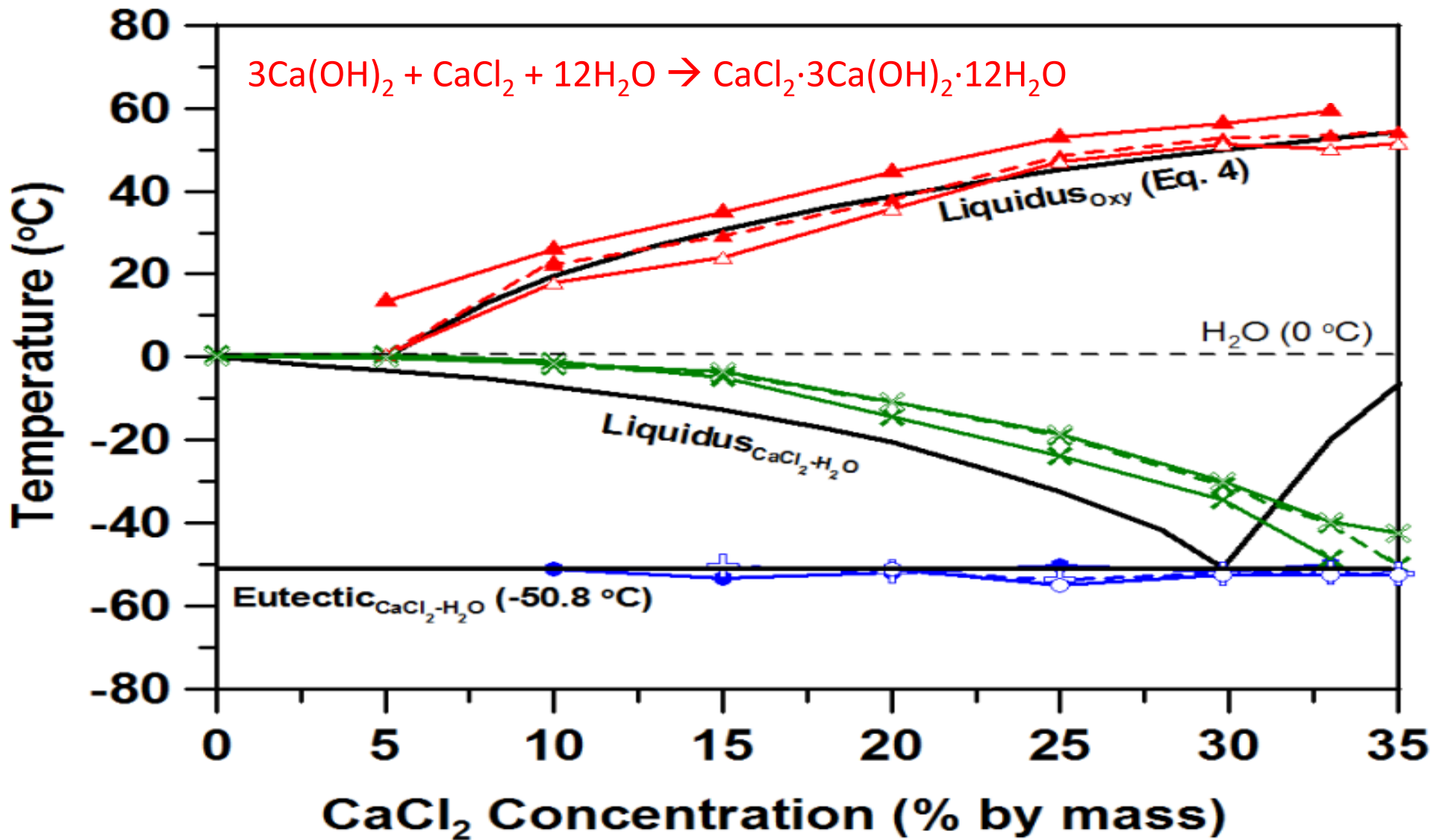
- As slag is added the CH value decreases
- Here we see simulations that assume different extents of rxn



# CH Reduces with Slag

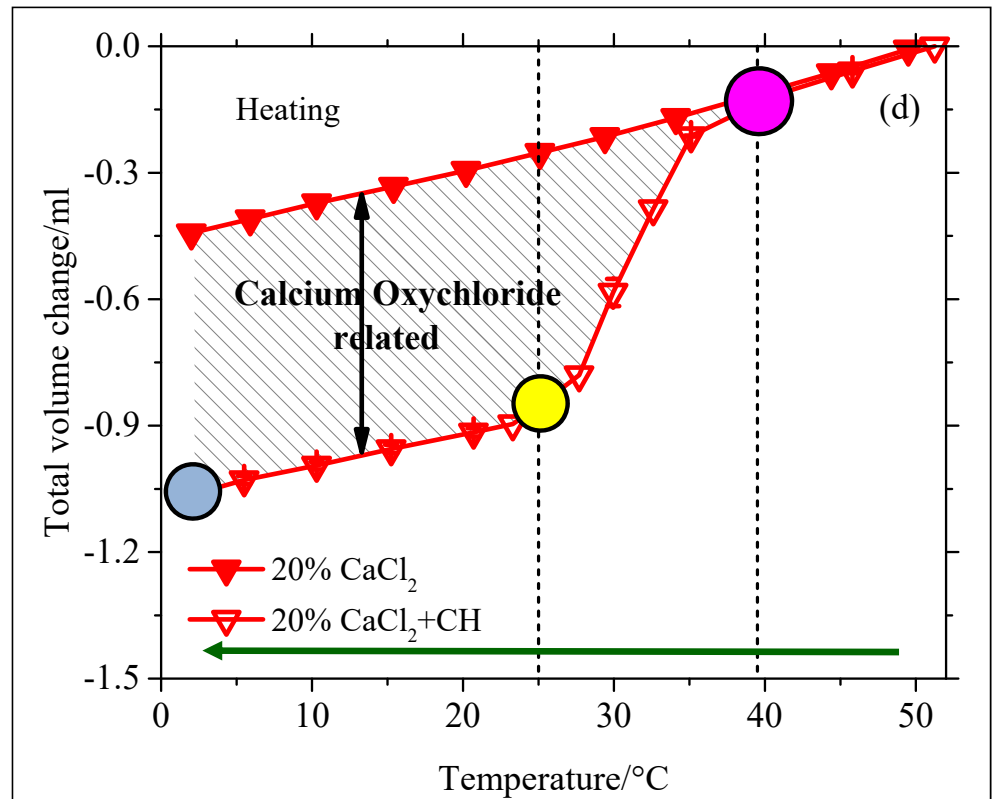
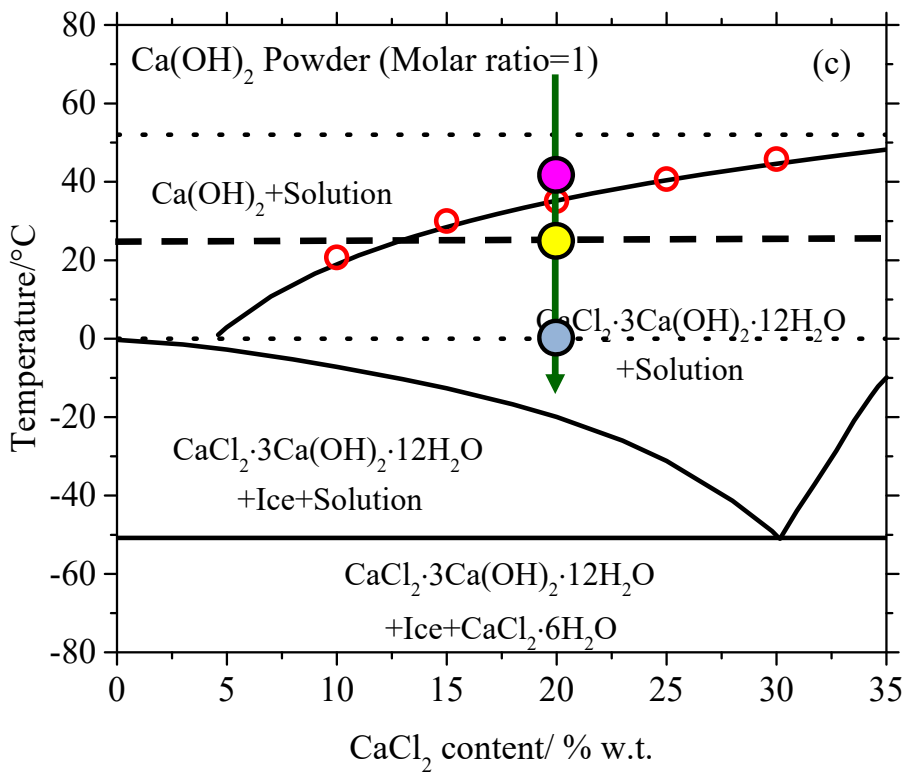
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- Here we see simulations that assume different extents of rxn





Farnam et al. 2013

# Volume Change

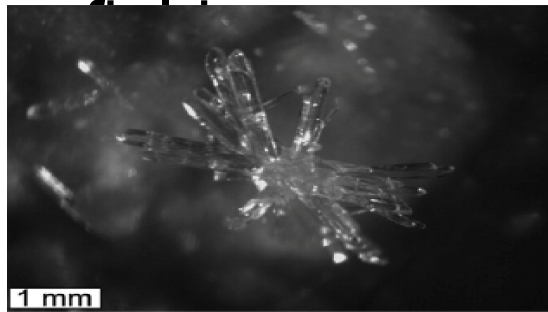


Qiao et al. 2017

# Calcium Oxychloride



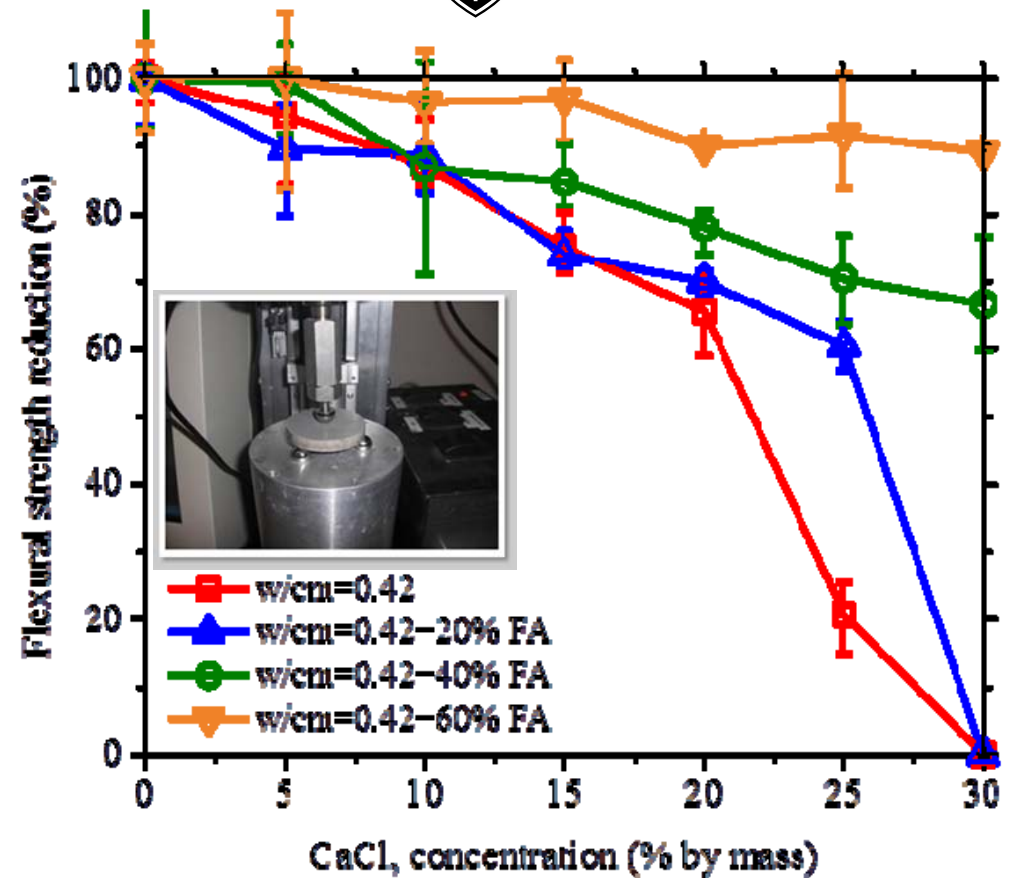
- Ca-oxychloride transforms from liquid to solid
- Damage manifests as paste flaking that is observed in the



Peterson et al. 2013



Qiao et al. in 2017

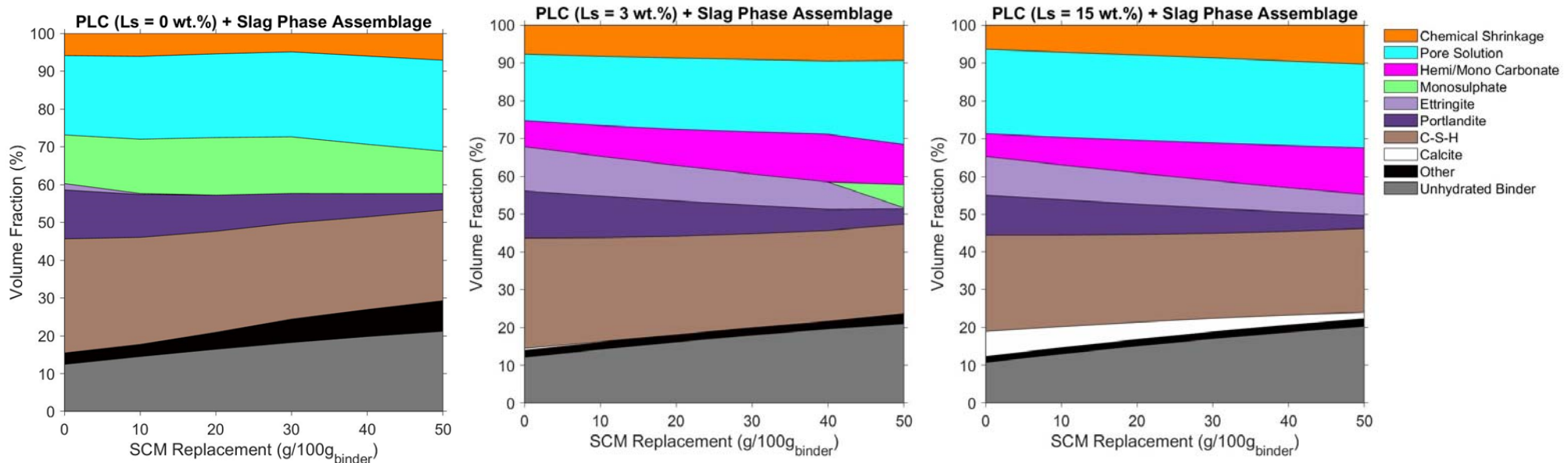


Qiao et al. in 2017

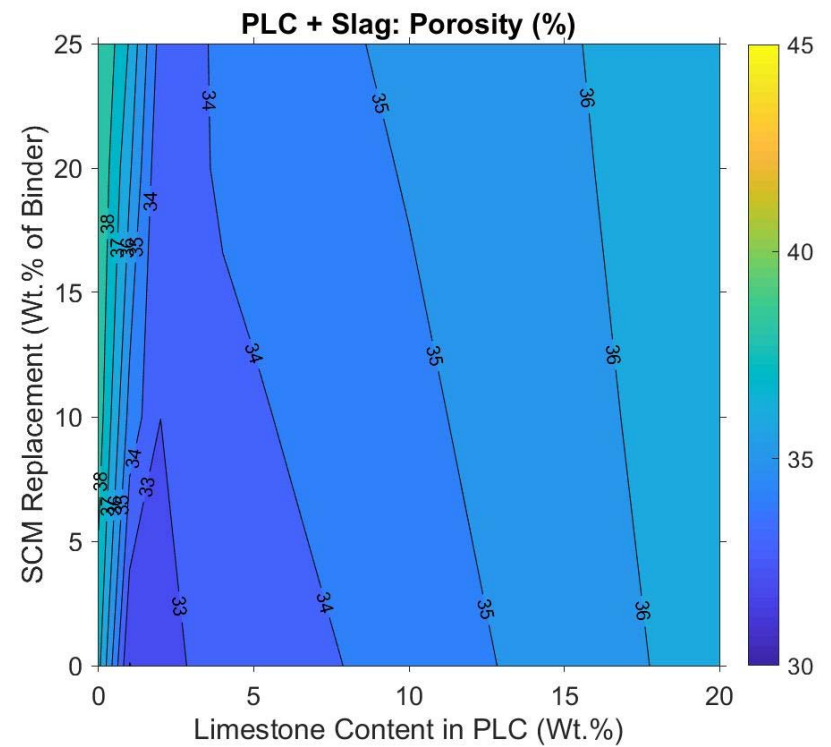
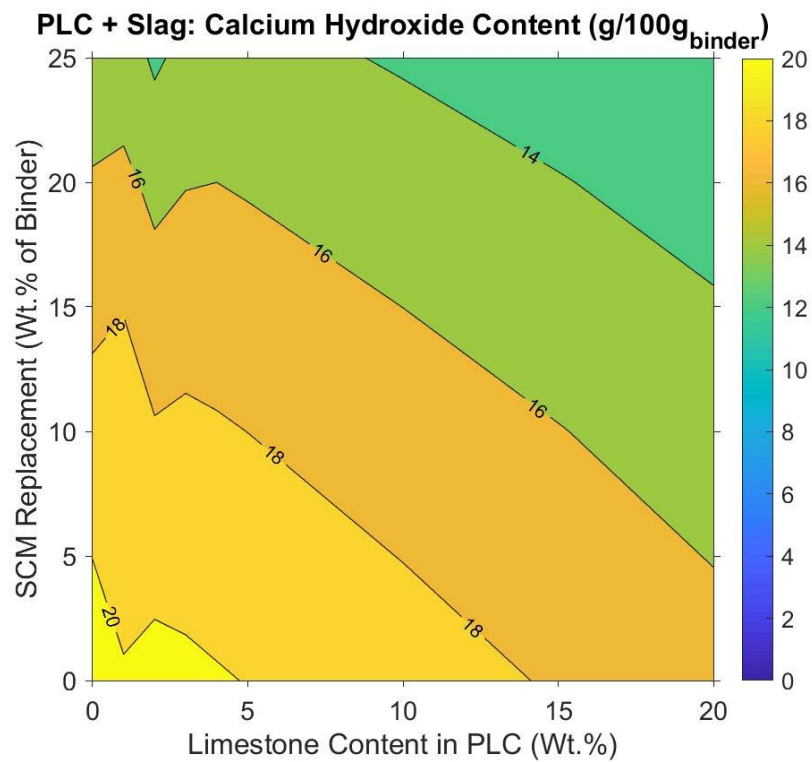
# Thermodynamic Model



- As limestone is increased, the chemical shrinkage increases and the monosulfate converts to ettringite and hemi/mono carbonate



# PLC + Slag



# Numerical case studies

## Cement:

C<sub>3</sub>S: 52.2%  
C<sub>2</sub>S: 21.6%  
C<sub>3</sub>A: 8.1%  
C<sub>4</sub>AF: 7.6%  
SO<sub>3</sub>: 3.0%  
Na<sub>2</sub>O<sub>eq</sub>: 0.2%  
MgO: 2.3%

## Slag:

SiO<sub>2</sub>: 35.0%  
Al<sub>2</sub>O<sub>3</sub>: 12.0%  
Fe<sub>2</sub>O<sub>3</sub>: 1.0%  
CaO: 40.0%  
SO<sub>3</sub>: 9.0%  
Na<sub>2</sub>O<sub>eq</sub>: 0.6%

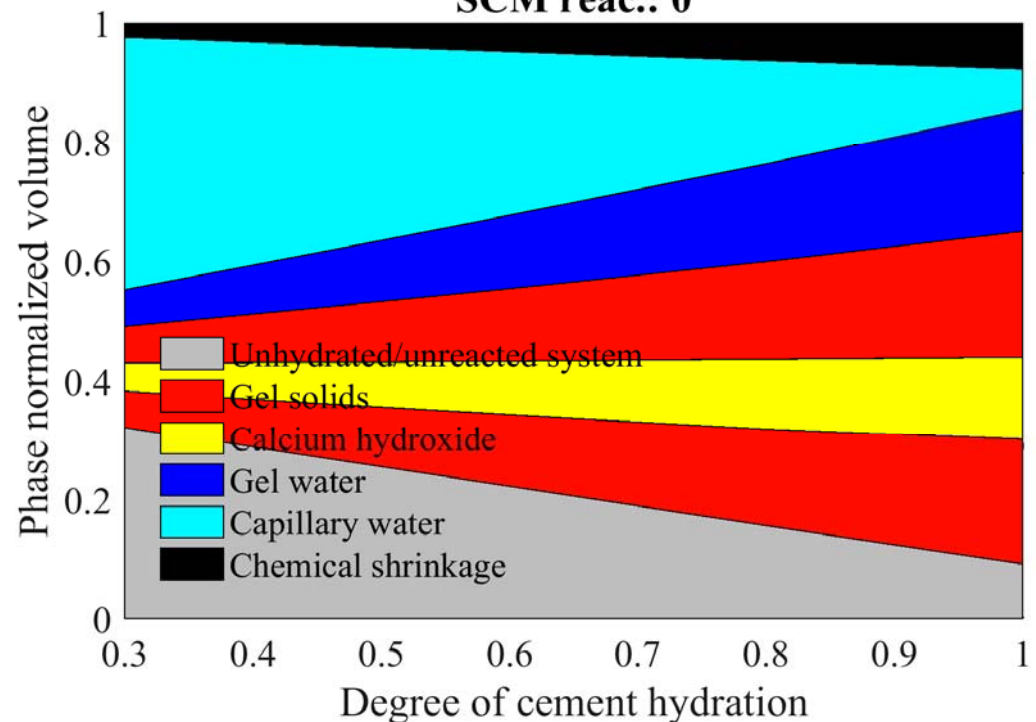
w/b = 0.42  
T = 23 °C

- Mass replacement: 0-80%
- SCM reactivity: 0-60%

<sup>1</sup> Shehata, Thomas 2000

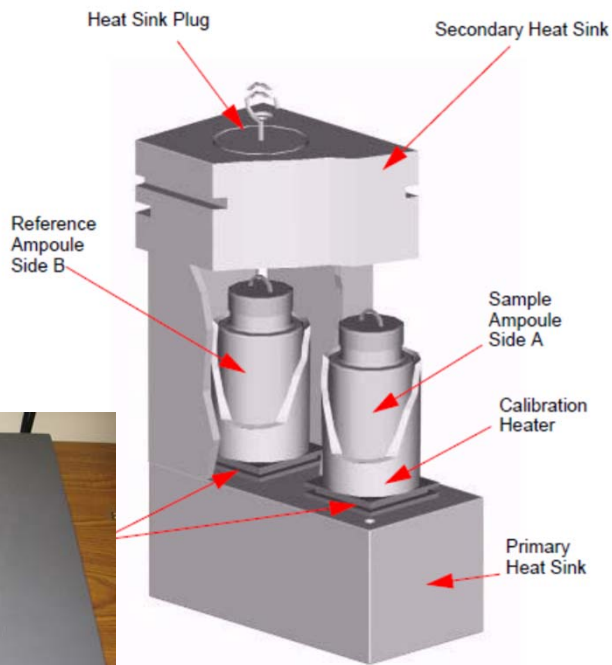
<sup>2</sup> PCA bulletin 15<sup>th</sup> edition, 2011

SL system with wb=0.42 T=296.15 °K,  
SCM repl.: 0.2  
SCM reac.: 0

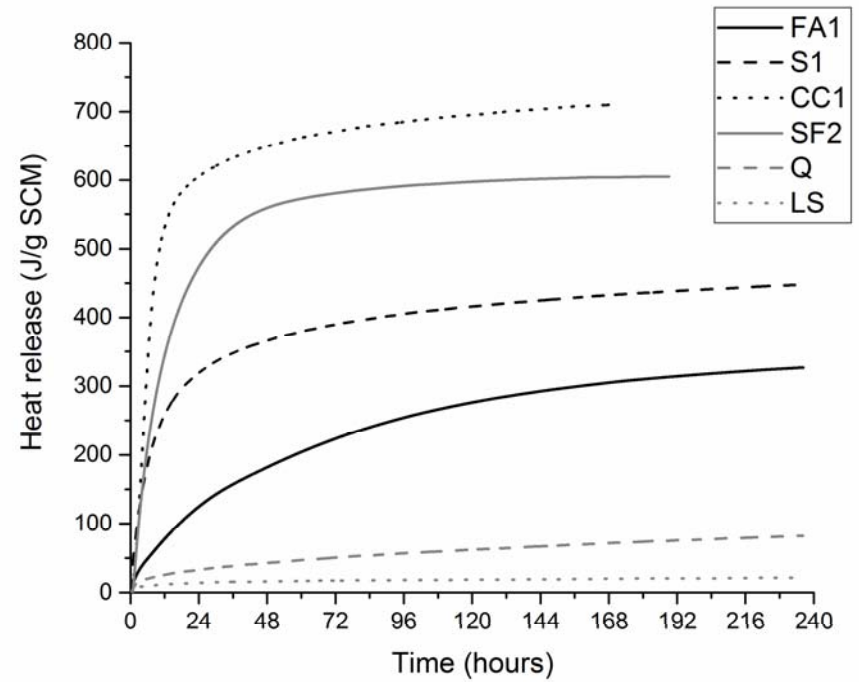




# Isothermal Calorimetry



Cutaway View  
Twin Configuration  
One of Eight Calorimetric Channels

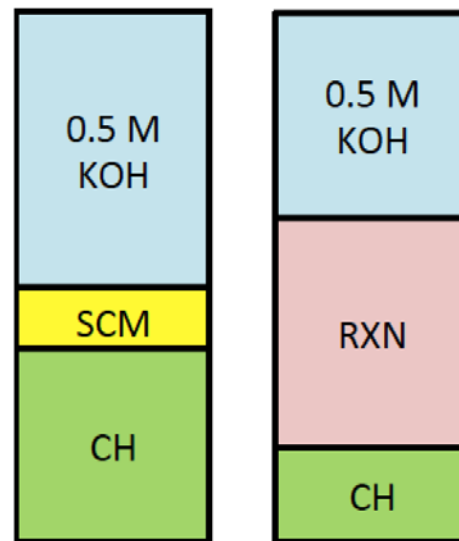


Suraneni et al., 2016b

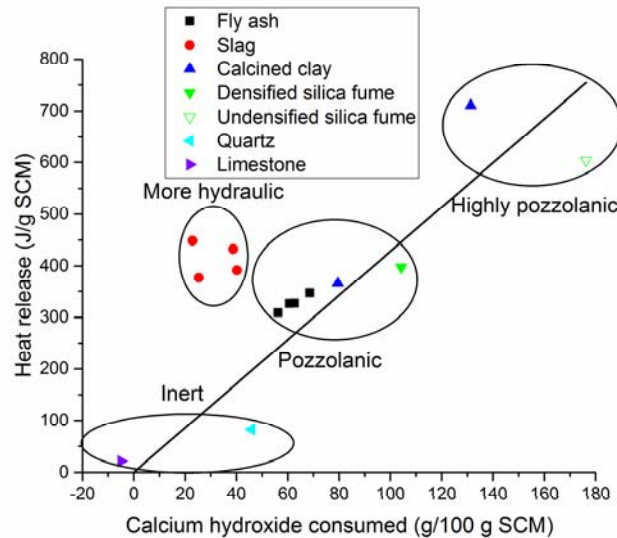
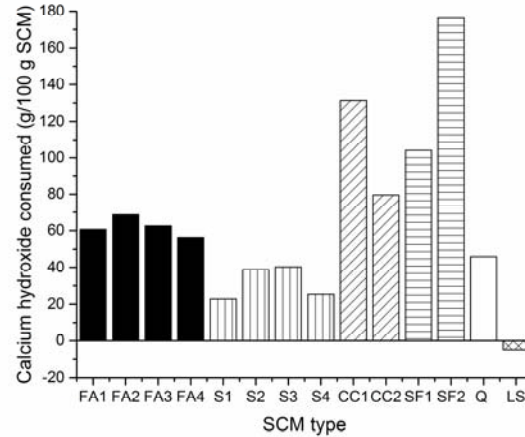
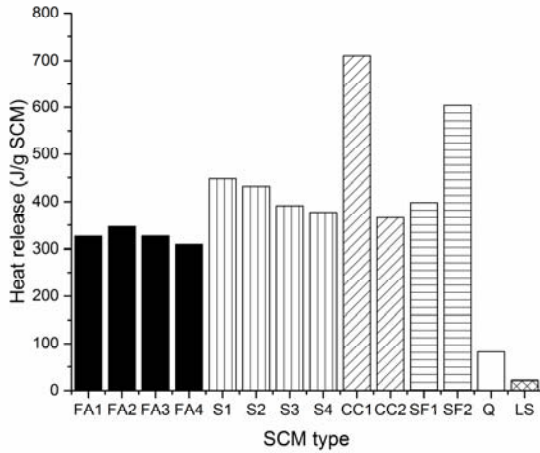
# New pozzolanic test (Being Incorrectly Applied to Slag)



- Measurement of heat release, CH consumption, and bound water for SCM-CH systems



- CH/SCM = 3: 1 (by mass)
- 0.5 M KOH solution
- $w/s = 0.9$
- Temperature = 50 °C
- Measure heat release by IC and CH consumption by TGA for various SCMs
- Adapting interpretation for Slag (Ongoing work DOE)



- Sixteen fly ashes
- Four slags
- Two calcined clays
- Two silica fumes
- Limestone
- Quartz
- Ground LWA
- Other non-traditional SCMs

# Sustainability in Construction a Look at Portland Limestone Cement



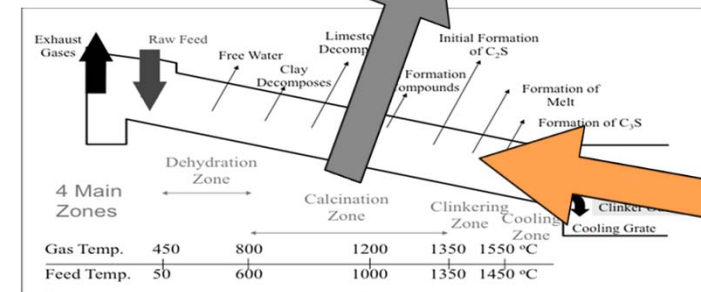
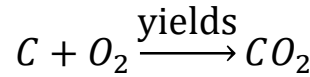
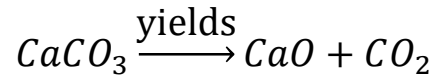
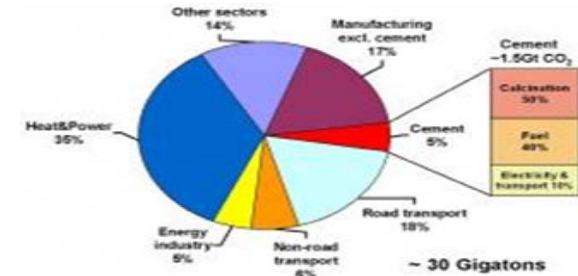
Jason Weiss, [jason.weiss@oregonstate.edu](mailto:jason.weiss@oregonstate.edu), Originally developed 2011  
Head School of Civil and Construction Engineering, Edwards Distinguished Professor



# Cement and CO<sub>2</sub> Production



- You will hear cement accounts for 7-8% of global CO<sub>2</sub> (Mehta 1998)
- What/Where is the CO<sub>2</sub> coming from
  - Calcination
  - **Combustion**
  - **Transportation**
- Concrete has relatively low carbon emission per unit; however widespread use of concrete makes it a major contributor to manmade CO<sub>2</sub> emissions



# Concrete Sustainability



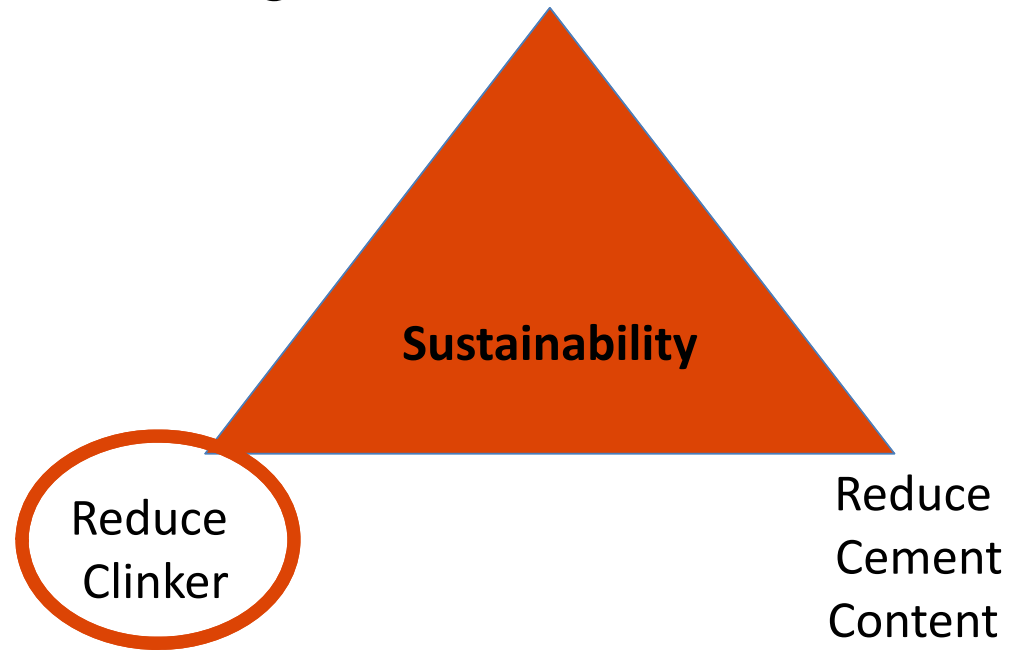
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- I will suggest that change is needed
- I will suggest that the time for change is



- Three Prong approach

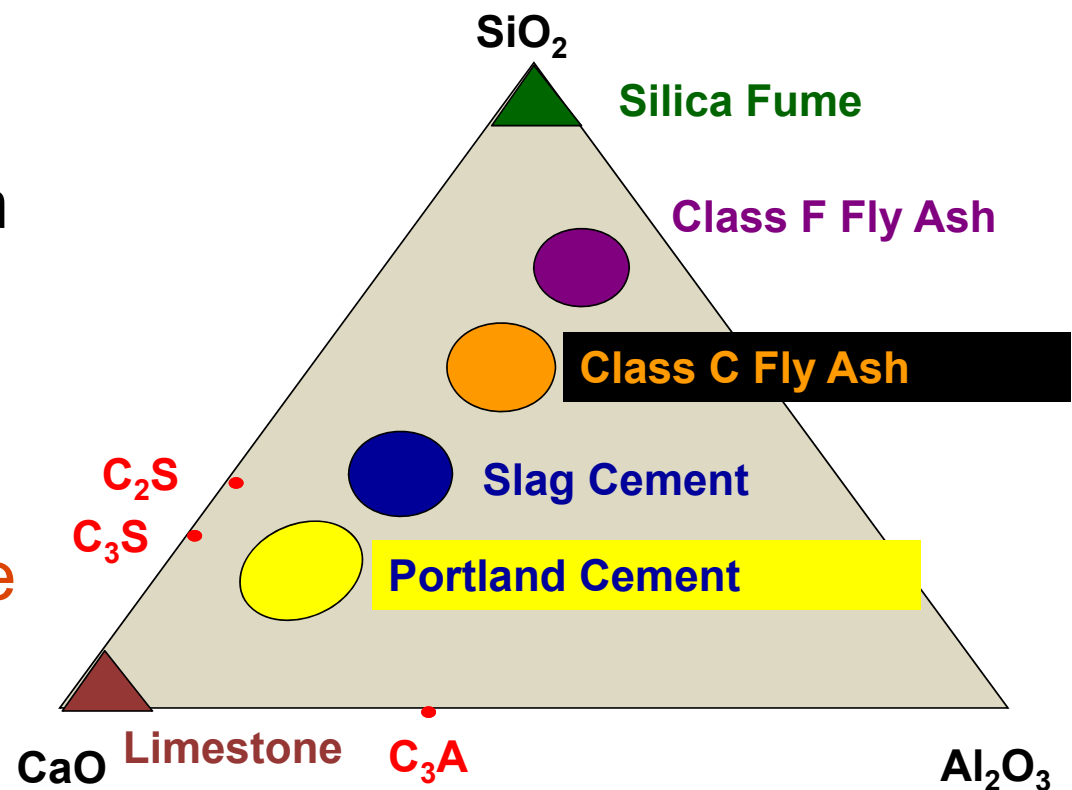
Life Cycle  
Performance



# Approaches to Reduce Clinker Content



- OPC is one of many compositions in the  $\text{CaO-SiO}_2\text{-Al}_2\text{O}_3$  system
- 'by-product materials' from other industries
- **Clinker substitutes: fly ash, slag and limestone**
- Reactivity and size

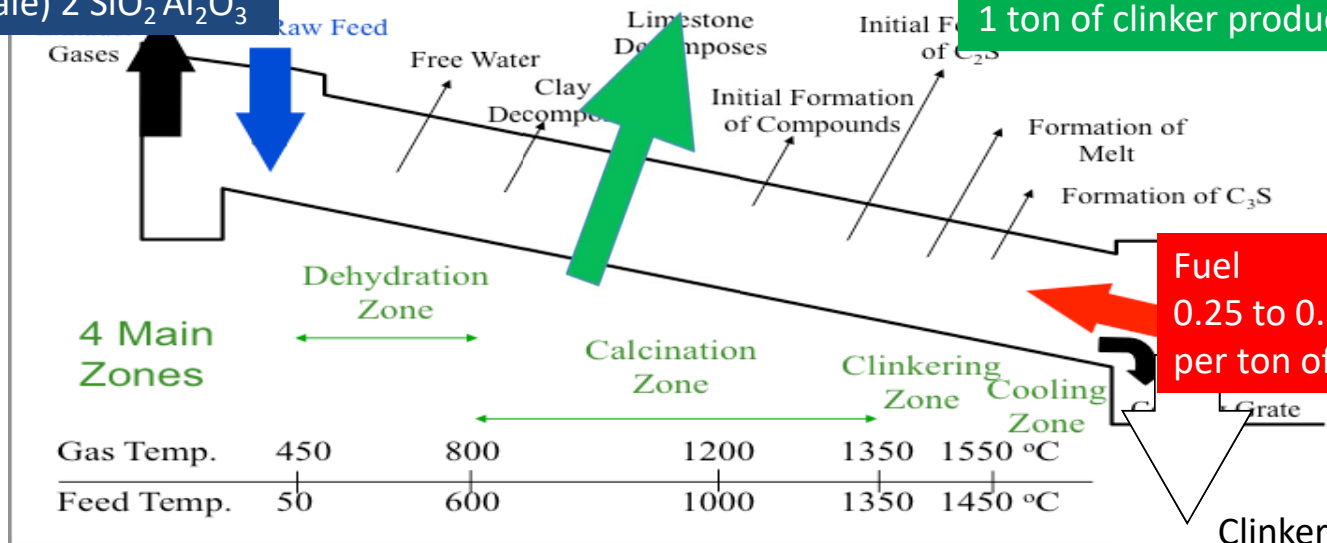


# Ordinary Portland Cement



Limestone ( $\text{CaCO}_3$ )  
Iron Oxide ( $\text{Fe}_2\text{O}_3$ )  
Silica  $\text{SiO}_2$   
Aluminate (Clay, Shale)  $2 \text{SiO}_2 \text{Al}_2\text{O}_3$

Calcination  
 $\text{CaCO}_3 \xrightarrow{\text{yields}} \text{CaO} + \text{CO}_2$   
1 ton of clinker produces 0.5 ton  $\text{CO}_2$



Fuel  
0.25 to 0.65 ton  $\text{CO}_2$   
per ton of clinker

Clinker  
3  $\text{CaO SiO}_2$   
2  $\text{CaO SiO}_2$   
3  $\text{CaO Al}_2\text{O}_3$   
4  $\text{CaO Al}_2\text{O}_3 \text{Fe}_2\text{O}_3$

Ordinary Portland Cement

Intergrind  
Gypsum + Clinker  
 $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$

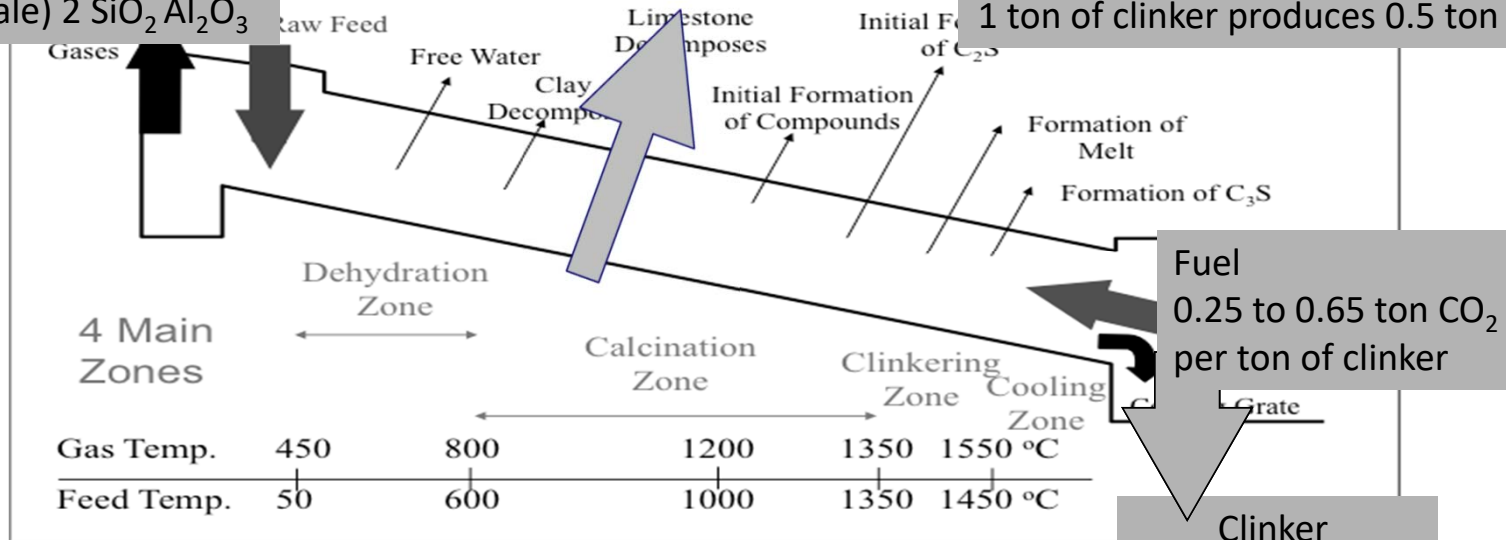


# Portland Limestone Cement



Limestone ( $\text{CaCO}_3$ )  
Iron Oxide ( $\text{Fe}_2\text{O}_3$ )  
Silica  $\text{SiO}_2$   
Aluminate (Clay, Shale)  $2 \text{SiO}_2 \text{Al}_2\text{O}_3$

Calcination  
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1 ton of clinker produces 0.5 ton  $\text{CO}_2$



Portland Limestone Cement

**Intergrind**  
Gypsum + Clinker + Limestone  
 $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$       $\text{CaCO}_3$

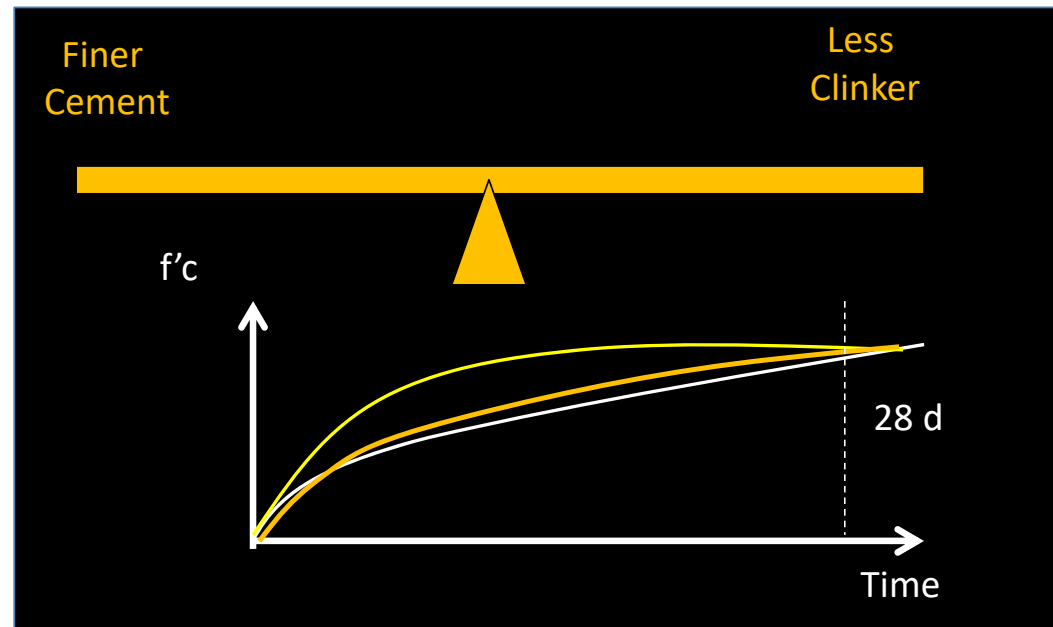
**Clinker**  
3  $\text{CaO SiO}_2$   
2  $\text{CaO SiO}_2$   
3  $\text{CaO Al}_2\text{O}_3$   
4  $\text{CaO Al}_2\text{O}_3 \text{Fe}_2\text{O}_3$

# Approach for Manufacture of Portland Limestone Cement



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- Similar performance is targeted
- PLC is generally ground finer than OPC
  - PLC requires more grinding
  - Higher fineness may act as a nucleating agent to increase early age strengths
- Higher reaction rates may show benefits of blending with other supplementary materials
- Finer cements can show higher shrinkage & cracking potential

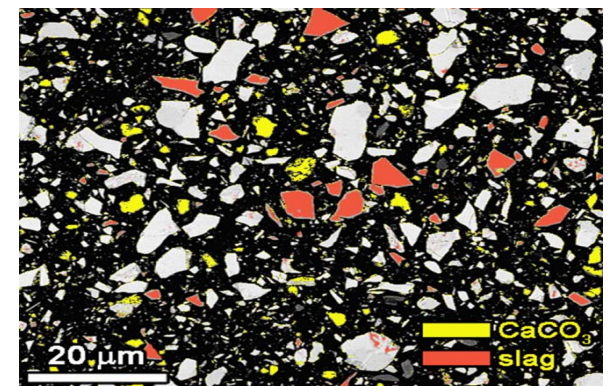
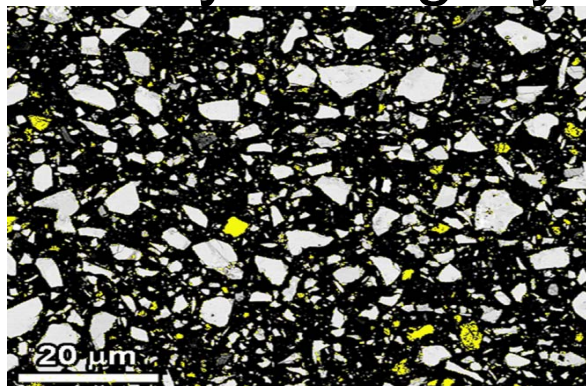
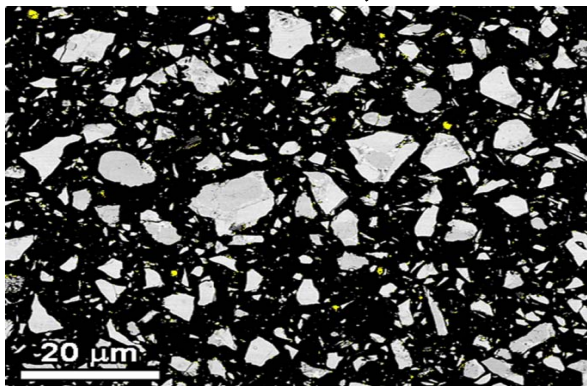


# A Comment on Grinding

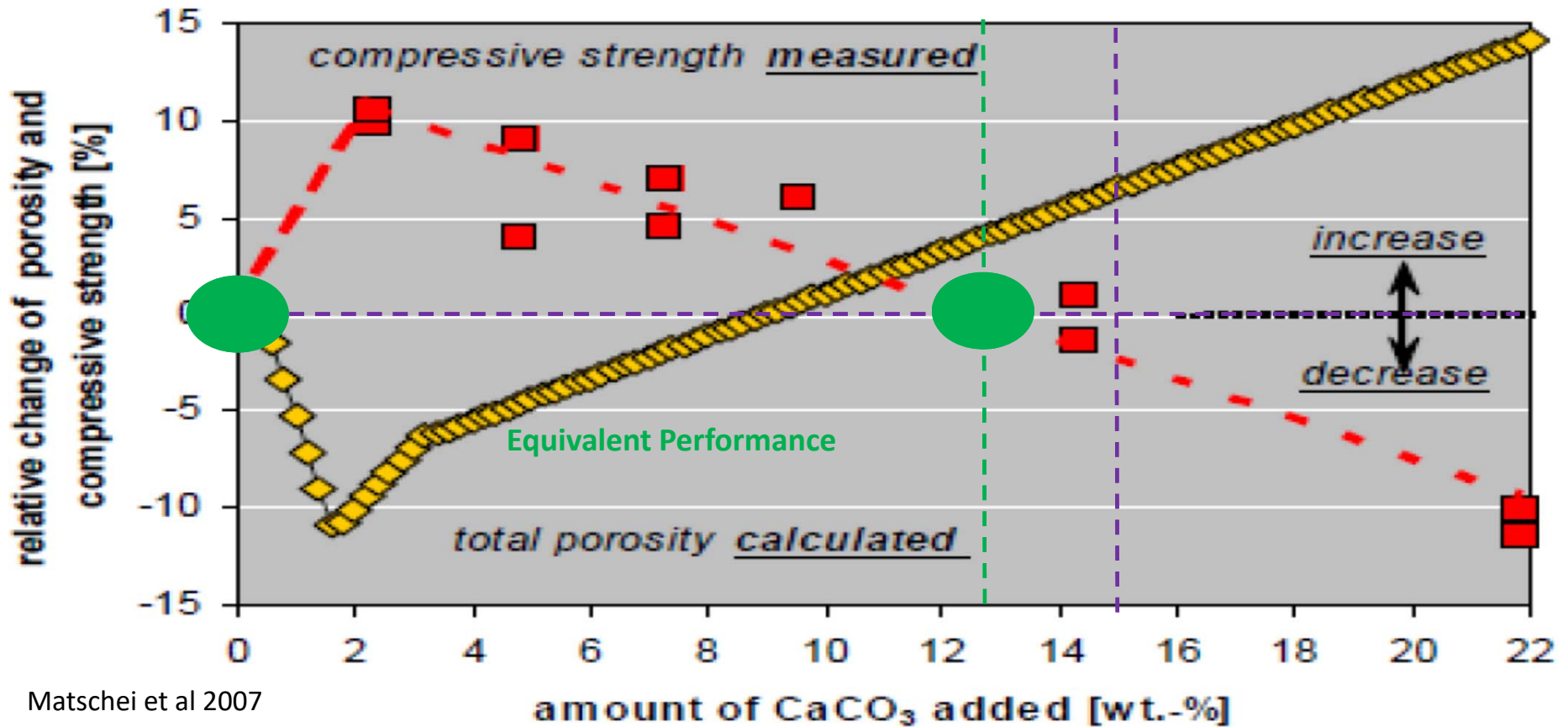


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- Blaine fineness typically increased to compensate for lower clinker content (8 to 10 m<sup>2</sup>/kg per % of LS added)
- generally 80 to 100 m<sup>2</sup>/kg to go from OPC (2%) to PLC (12%)
- Intergrind limestone is very fine since limestone is softer than clinker, the clinker may be slightly finer



# PLC Performance Studies



Matschei et al 2007

# Field Trials – Barrier Walls (Hooton 2009)



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- Minor scaling where water collects
- GU, GUL, GU, and GUL Slag
- Also used in paving operations

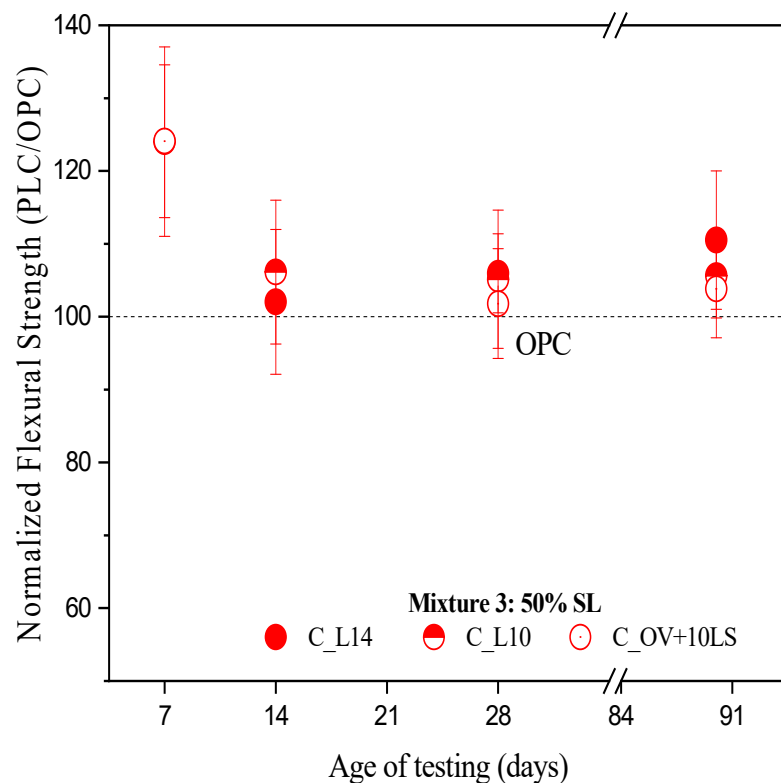


23 m<sup>3</sup> of each mix placed, 30 MPa, 60-100 mm (2.5-4 in.) slump

Nov. 2009 Barrier Wall

2009 Barrier Wall	PC +25% SLAG	PLC + 25% SLAG
Shrinkage (28d)	<b>0.038%</b>	<b>0.038%</b>
Strength (MPa)		
1	<b>9.5</b>	<b>10.3</b>
3	<b>19.3</b>	<b>19.4</b>
7	<b>25.6</b>	<b>26.8</b>
28	<b>36.9</b>	<b>37.9</b>
56	<b>38.9</b>	<b>38.0</b>
91	<b>40.7</b>	<b>40.2</b>
Freeze/Thaw Durability	<b>94%</b>	<b>94%</b>
MTO LS-412 Scaling	<b>0.24 kg/m<sup>2</sup></b>	<b>0.24 kg/m<sup>2</sup></b>
RCP (Coulombs)		
28 days	<b>2070</b>	<b>1490</b>
56 days	<b>1930</b>	<b>1340</b>

# Interesting Observation

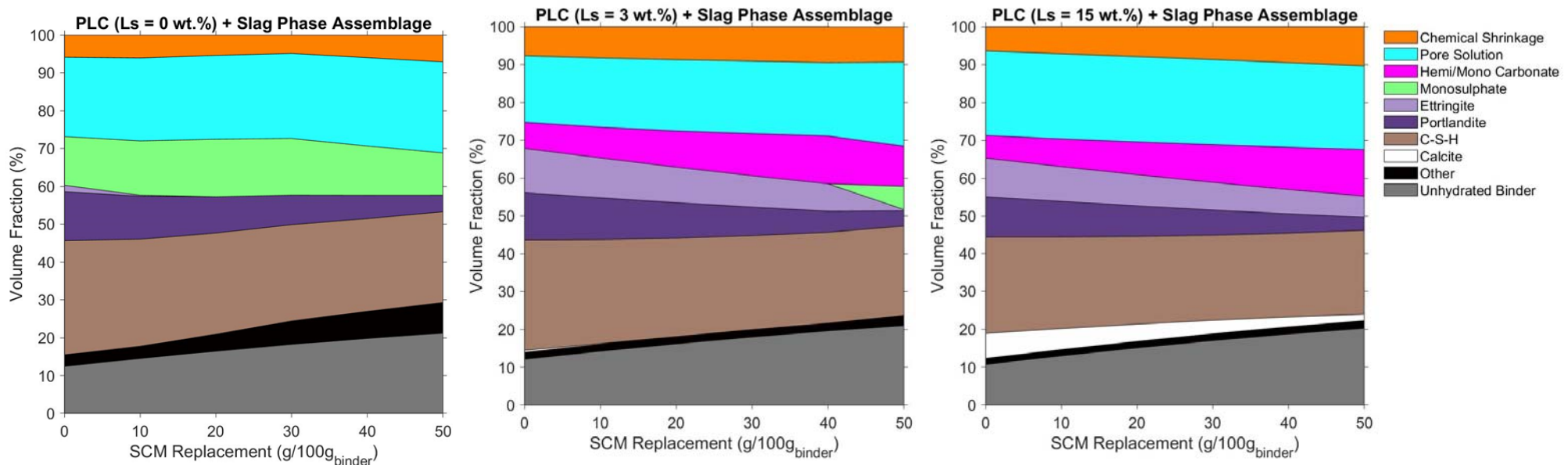


- When slag is used with PLC the early strength (and overall strength) tend to increase
- This is due to a synergistic effect of the limestone with slag

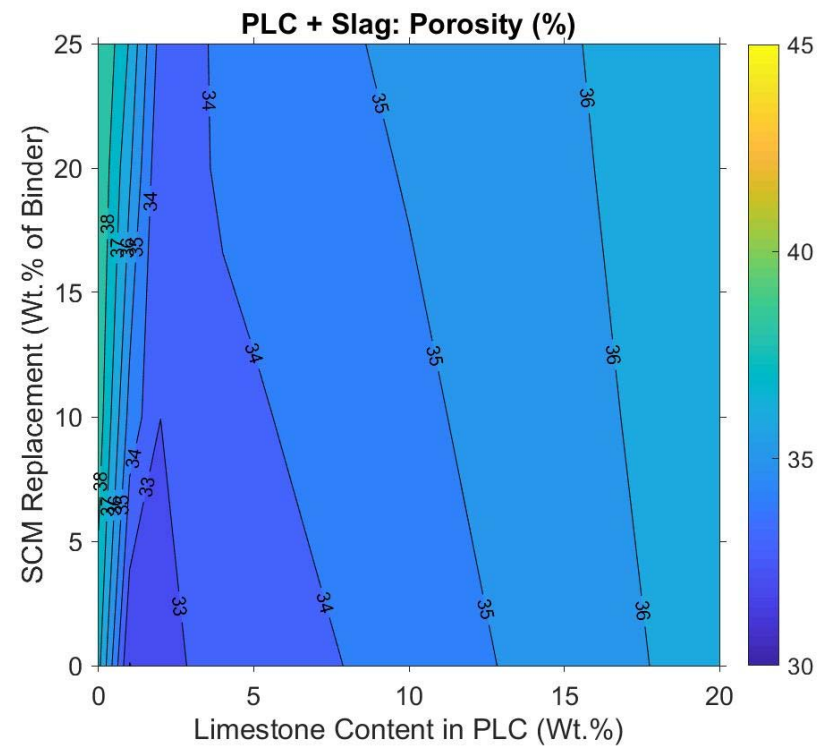
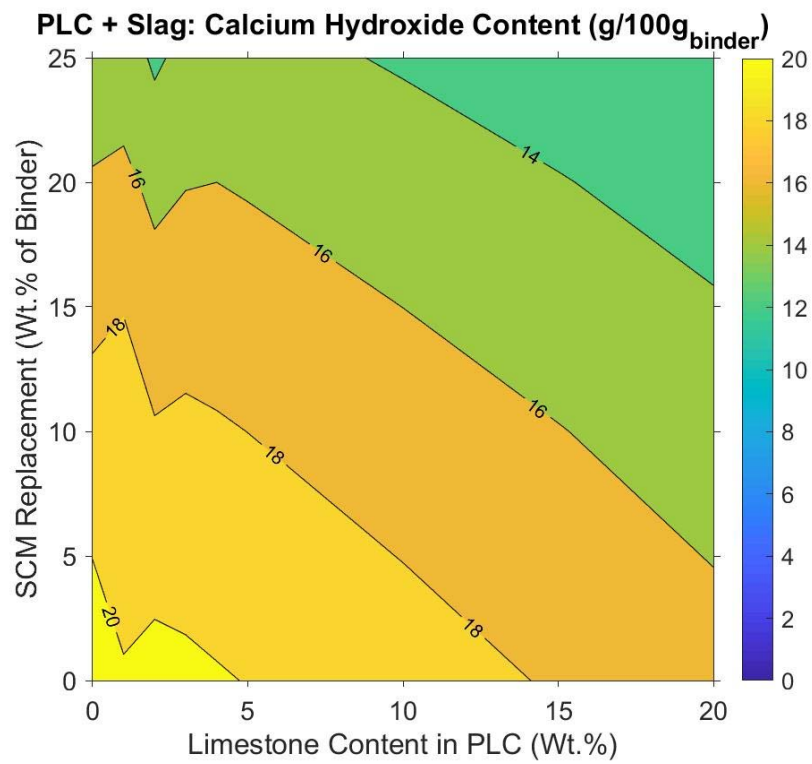
# Thermodynamic Model



- As limestone is increased, the chemical shrinkage increases and the monosulfate converts to ettringite and hemi/mono carbonate

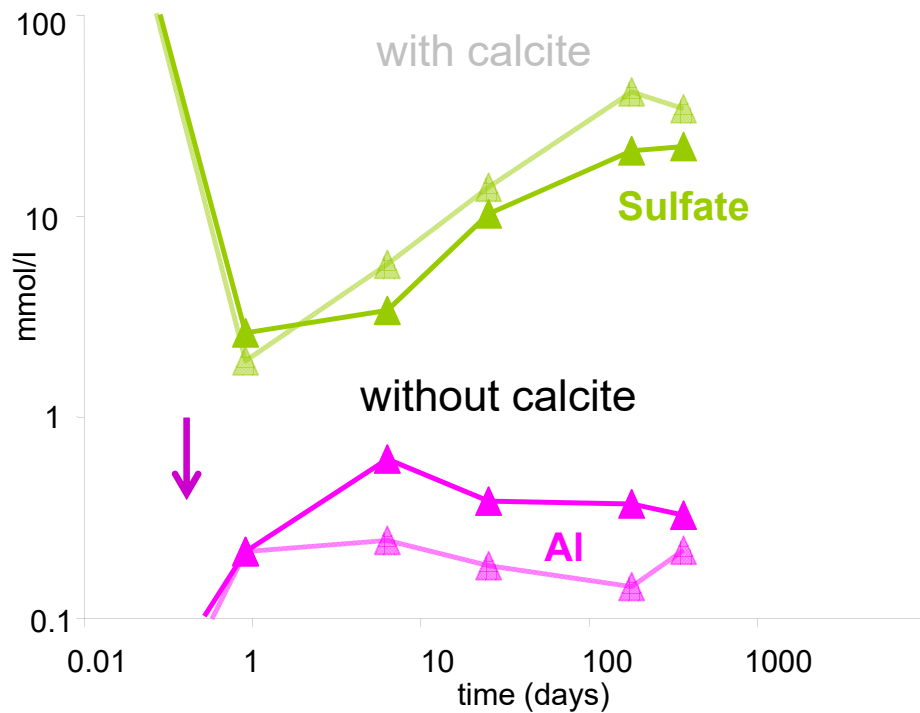


# PLC + Slag



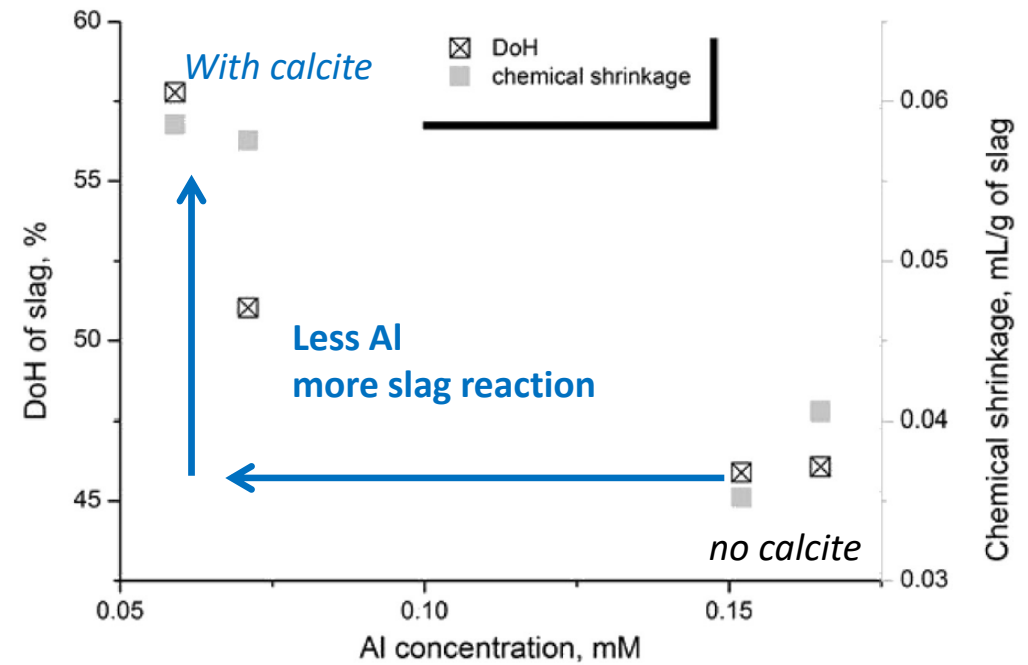


# Effect of limestone on pore solution (From Lothenbach)



Lothenbach et al. 2008, CCR 38

**Days to years:**  
**Limestone lowers aluminium concentrations**  
**Faster slag reaction**



Adu-Amankwah et al. 2017, CCR 100

# Conclusions



- Salt damage occurs at joints in pavements due to calcium oxychloride formation
- Slag reduces the potential for damage to occur – Dilution and reduction in CH
- New reactivity test (the pozzolanic test needs interpretation for non pozzolans)
- LTDSC Test is very useful
- Thermodynamic modeling is very useful
- Limestone and slag are a great combination

# Concrete at Early Ages: Relating Science and Construction Operations



# Construction Operations



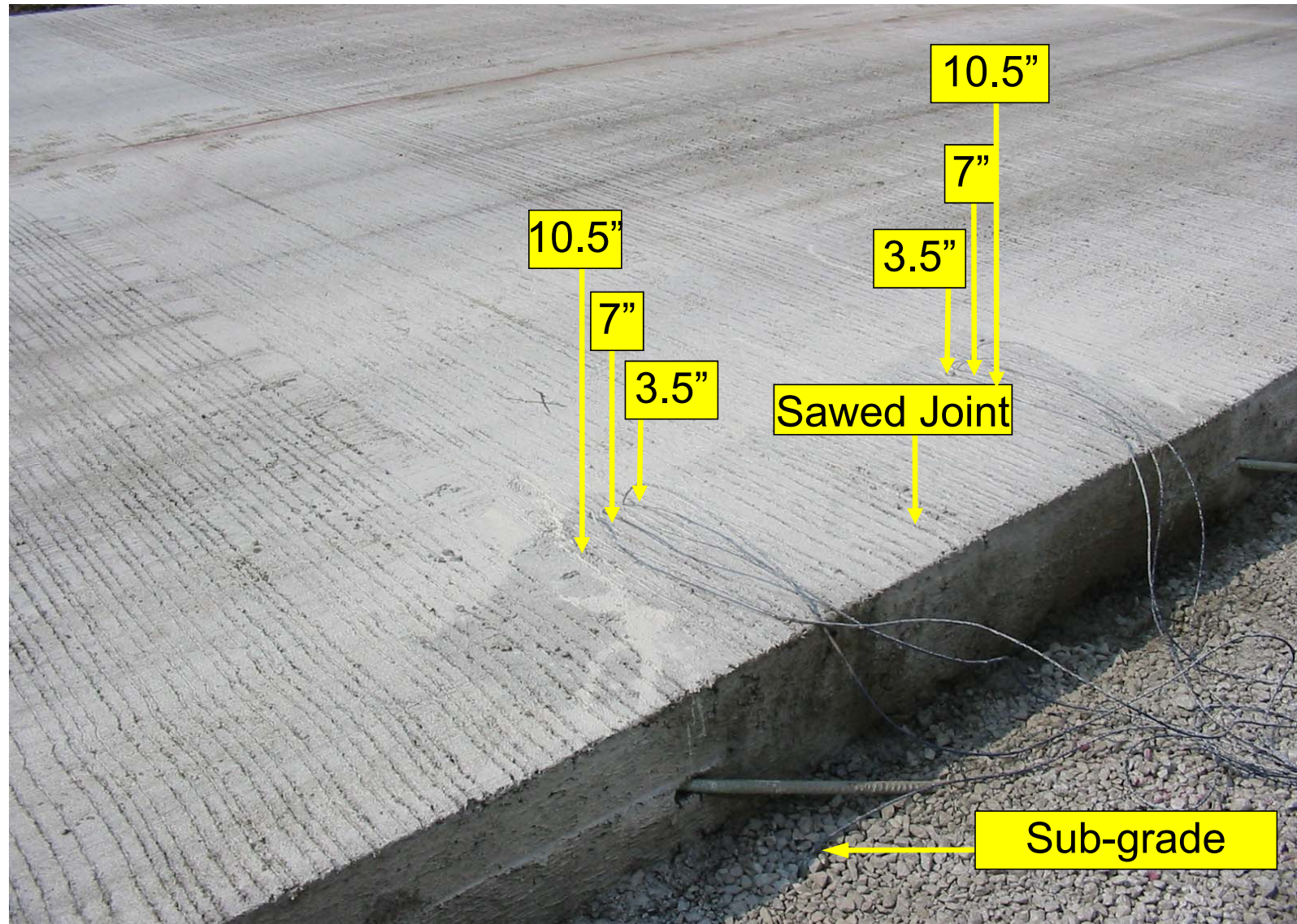
Oregon State University  
College of Engineering

- procedure for determining the appropriate **saw-cutting time window** constructed under the range of environmental conditions
- appropriate **depth of the saw-cut** that minimize the risk of damage (micro-cracking) and random crack development, and
- Developed **tools and training materials**



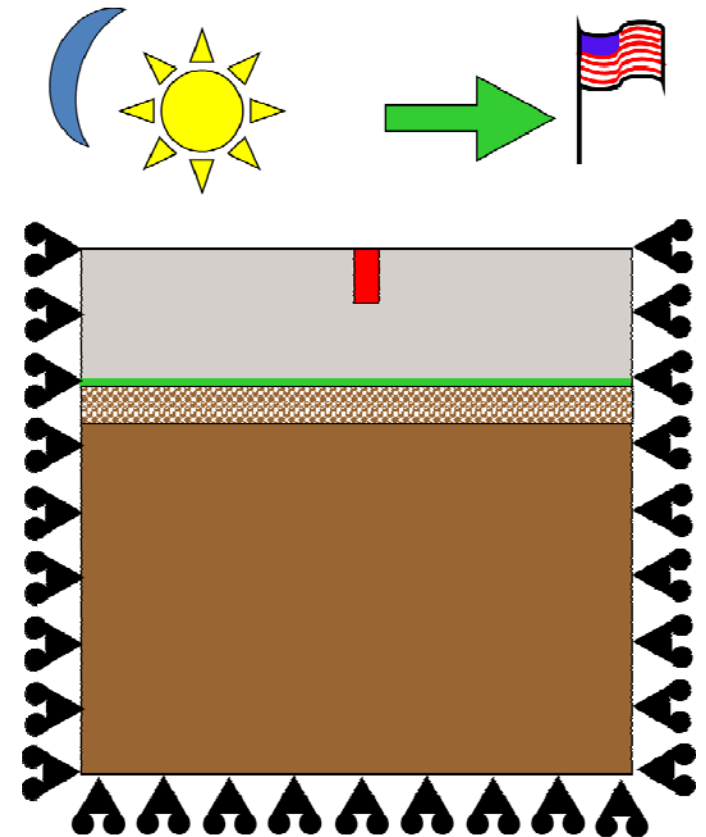
# Field Work

- 5 site visits (4 locations)
- Wide range of envir. (81°F -24°)
- Night pave
- 3 different mix design
- 10", 12", 14" and 15" pavement



# Modeling Approach

- Model developed to simulate stress and strain development in concrete pavements (slabs, decks) at early ages
- Model considers material properties, environmental exposure, and can introduce the sawcut



**The concrete mixture we are simulating is close to the mixture used by Berns Const.**

**w/cm = 0.42**

**air = 6.5%**

**Initial temp = 20°C**

**\* can be varied**

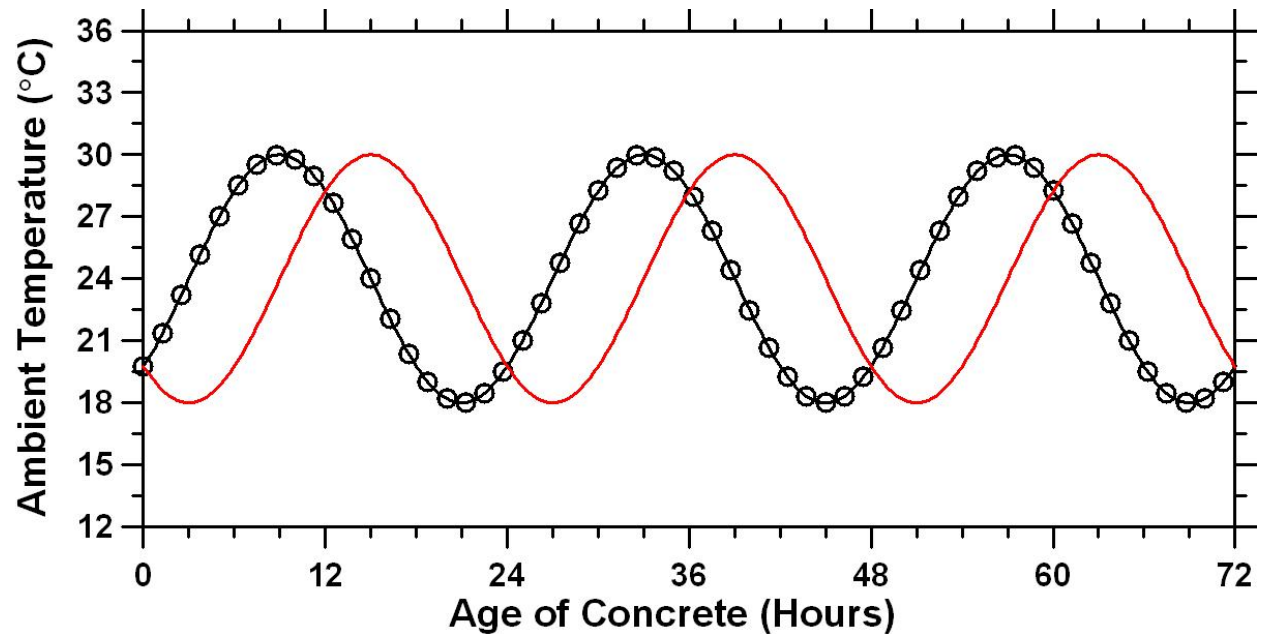


# Ambient Temperature



Oregon State University  
College of Engineering

- Choice of constant, periodical and linear ambient temperature functions
- This temperature function can be shifted to the right or to the left to consider paving operation at **different times of the day**



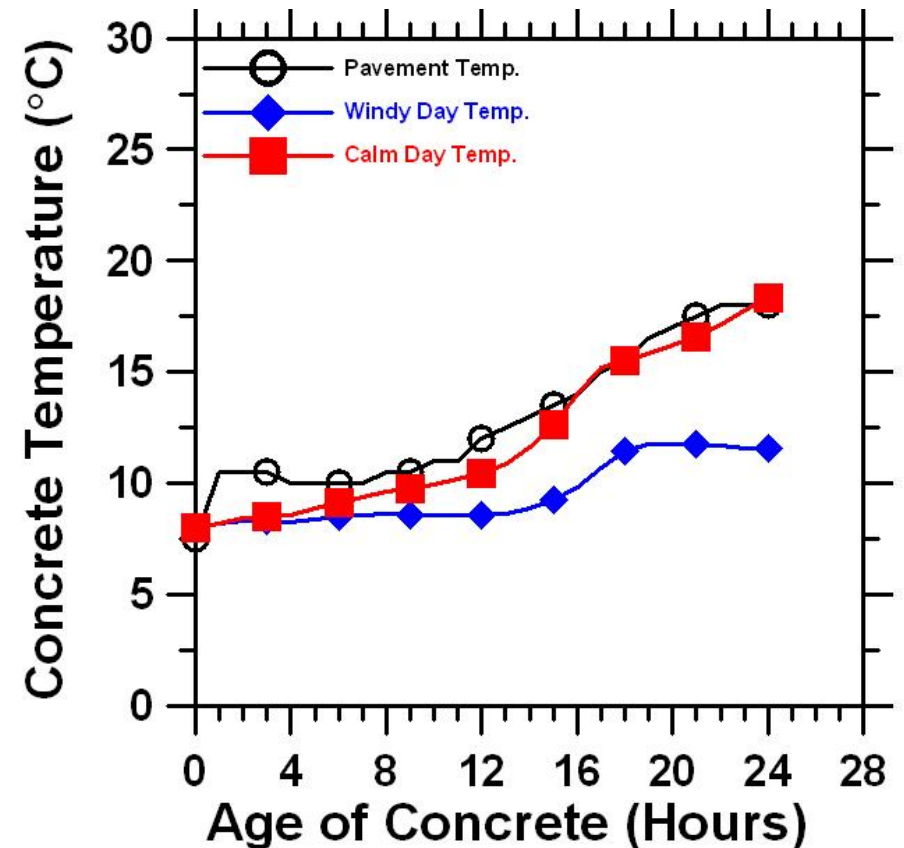
Temperature fluctuates  
between 18 °C and 30°C in  
a 24 hours time period



# Influence of the Wind

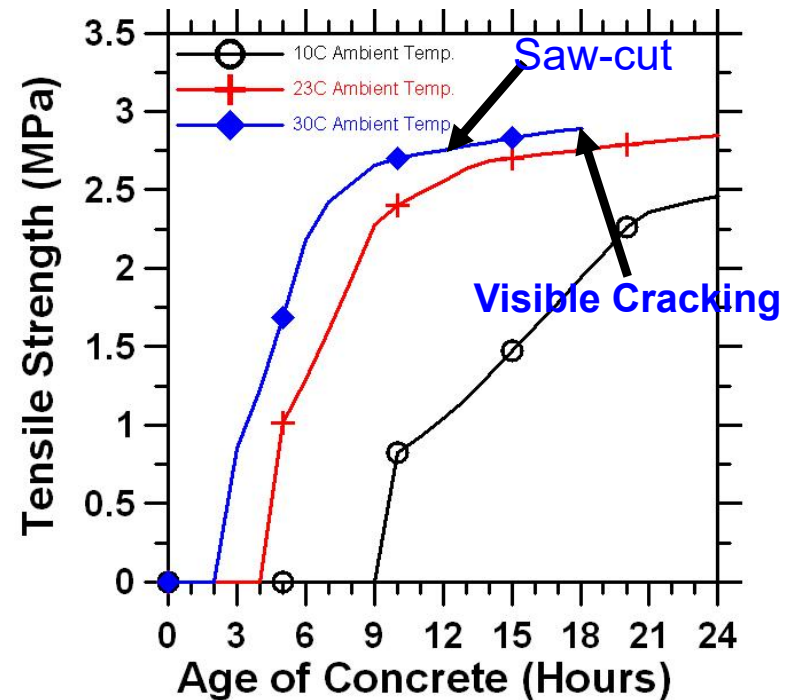


- Analysis shows that the higher the wind velocity, the higher the rate of heat dissipation, the lower the concrete temperature.
- The results compare well with field measurements.



# Influence of Ambient Temp. on Property Dev.

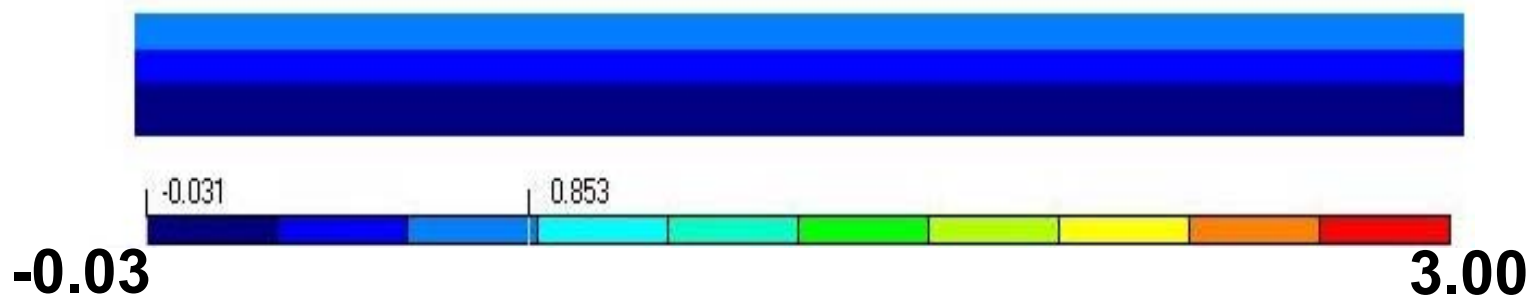
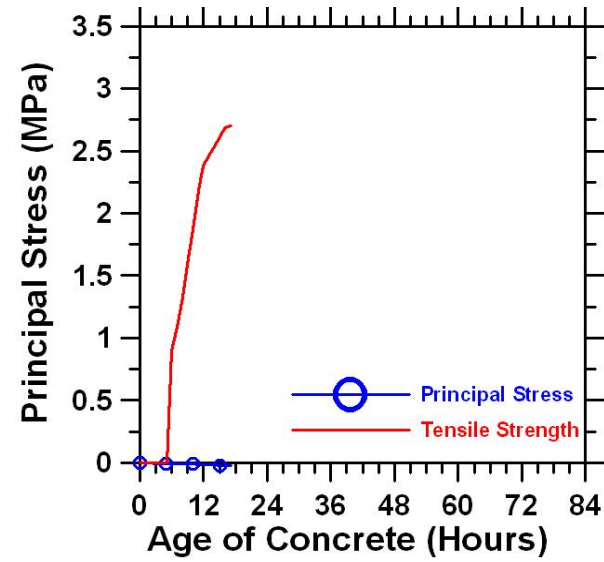
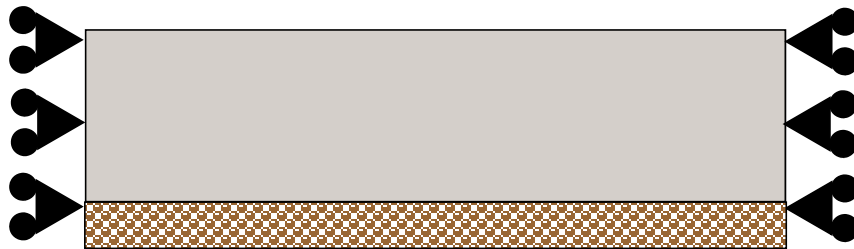
- 3 simulations performed with constant 10°C, 23°C, 30°C ambient temperatures
- As an example, tensile strength was measured at the tip of the notch
- Analysis reveals that the higher the ambient temperature, the higher the rate of concrete property development.





# What Happens When There Is No Saw-cut ?! Case I

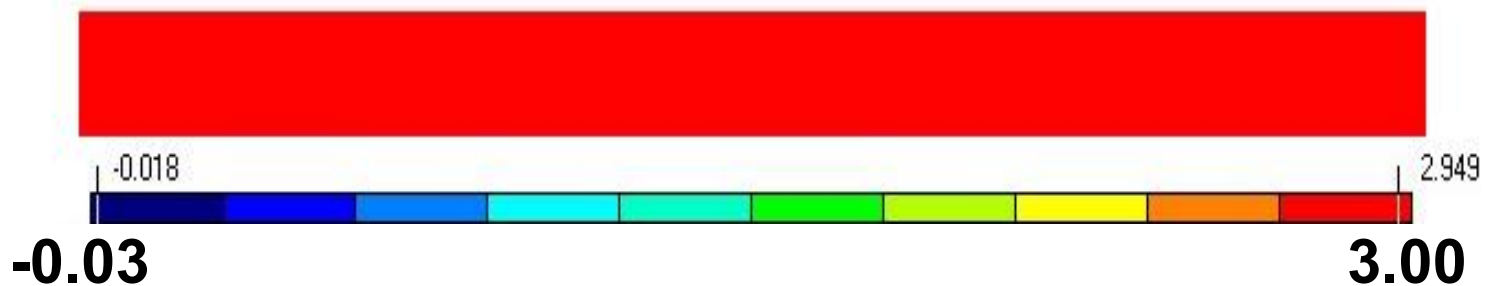
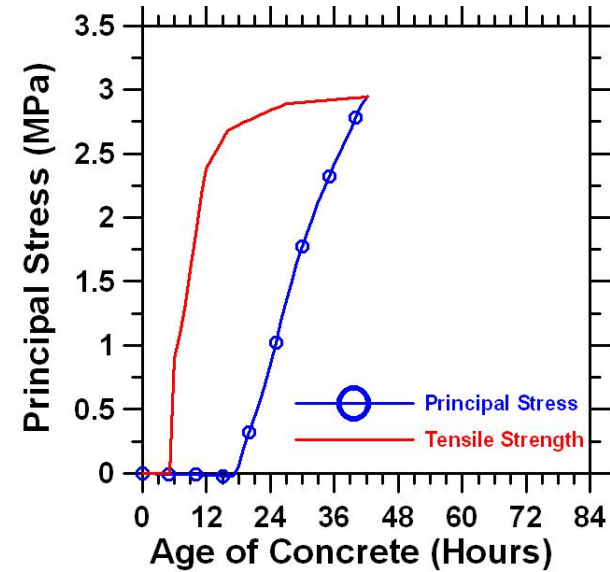
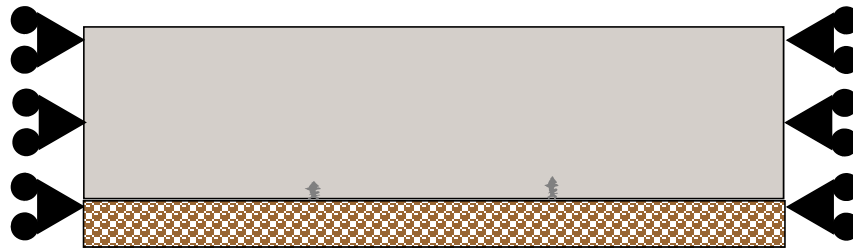
Step 1, 0–17 hours





# What Happens When There Is No Saw-cut ?! Case I

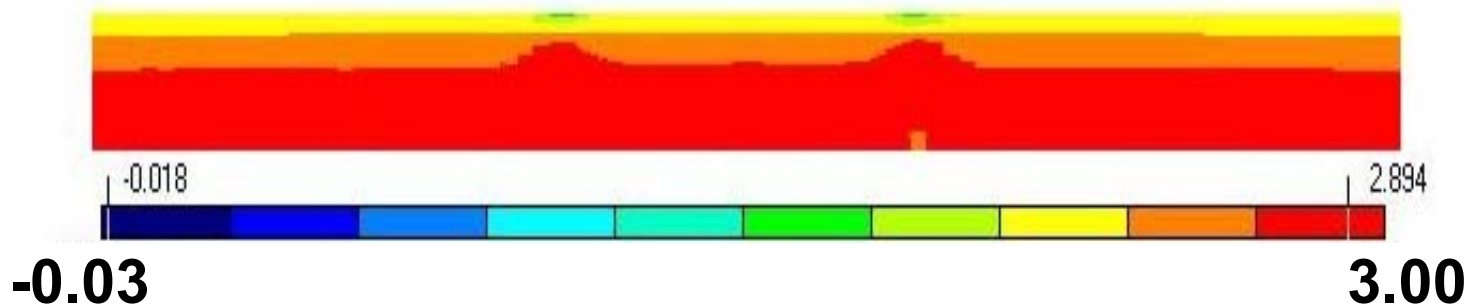
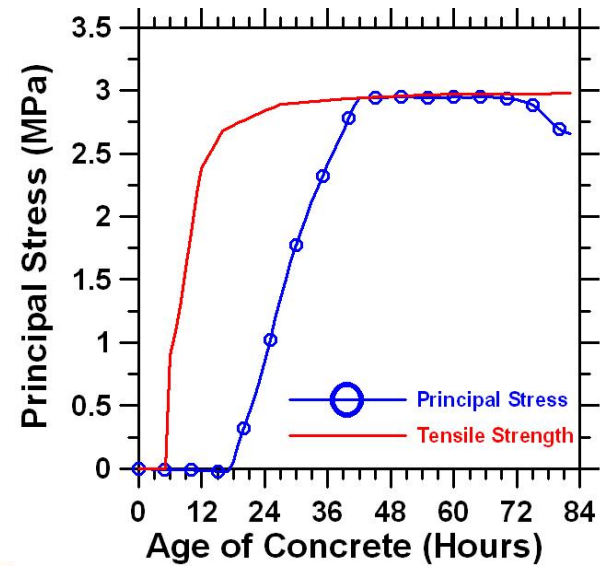
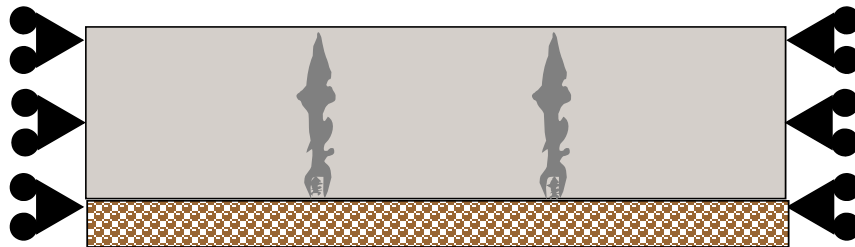
Step 2, 18-42 hours





# What Happens When There Is No Saw-cut ?! Case I

Step 3, 43-82 hours

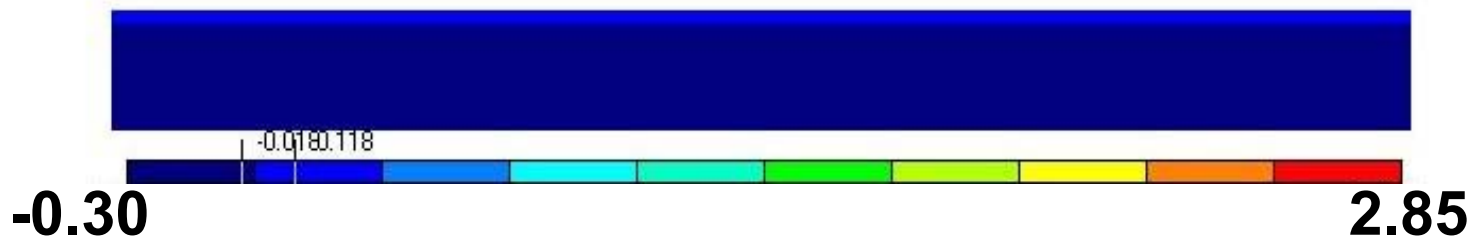
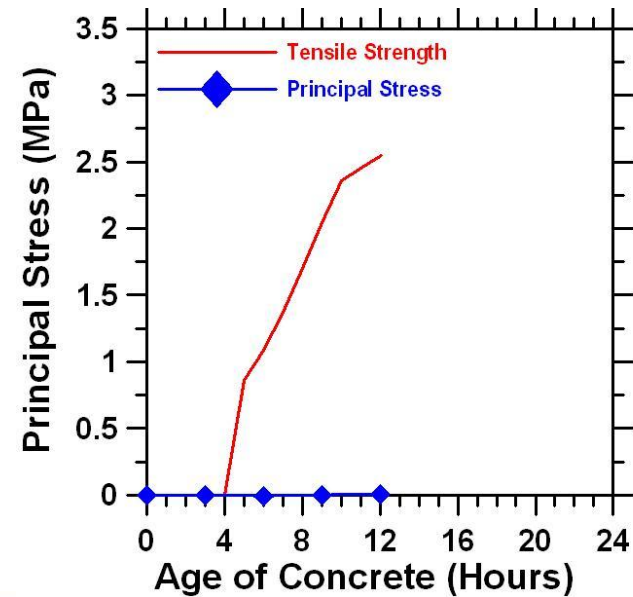
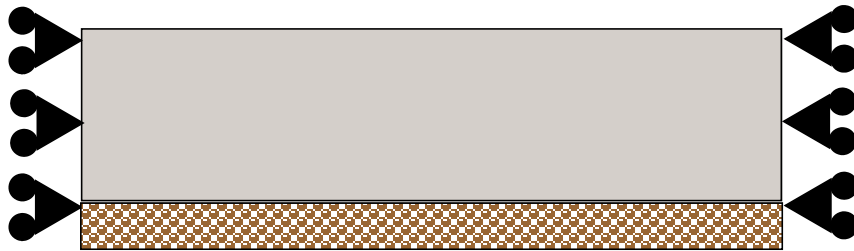




# $a_0 = D/3$ Notch Exerted at 12 Hours

## Case II

Step 1, 0–12 hours

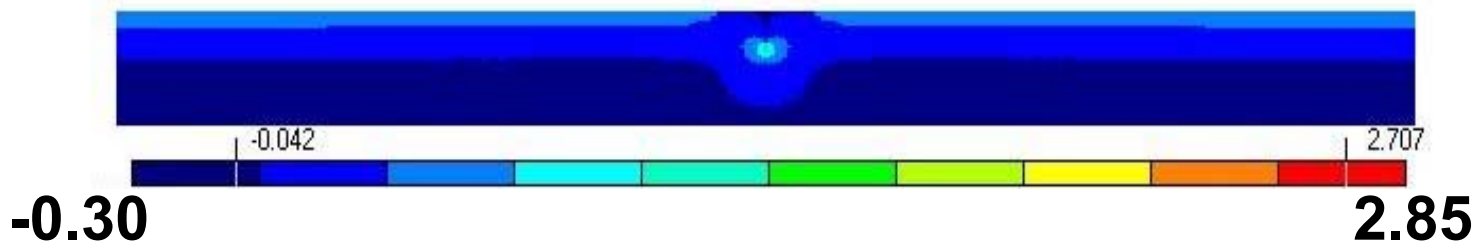
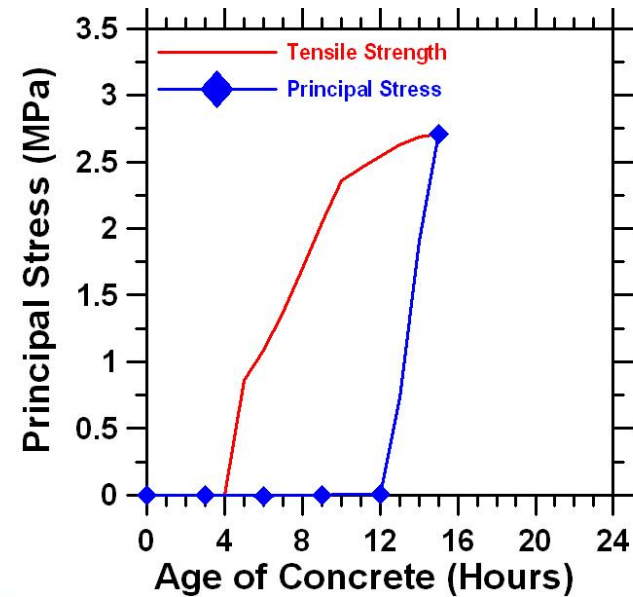
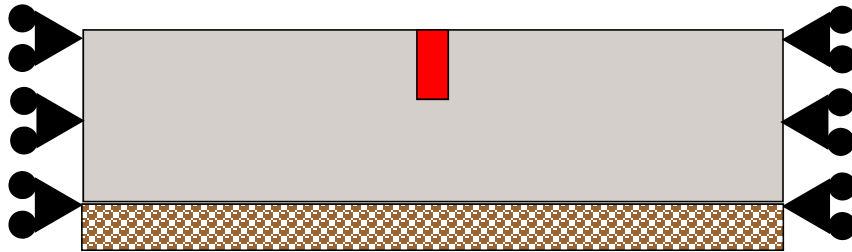




# $a_0 = D/3$ Notch Exerted at 12 Hours

## Case II

Step 2, 13-15 hours

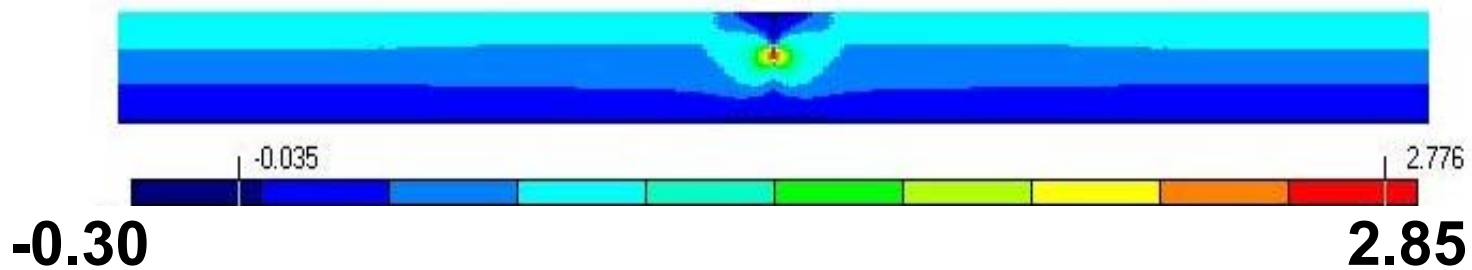
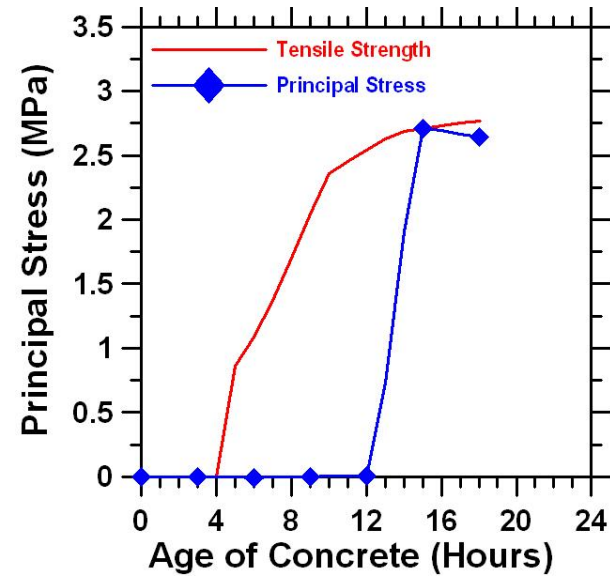
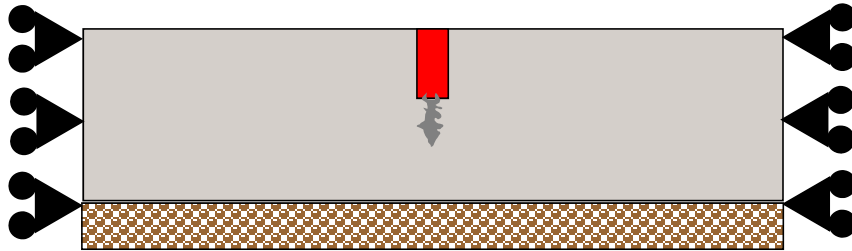




# $a_0 = D/3$ Notch Exerted at 12 Hours

## Case II

Step 3, 16-18 hours



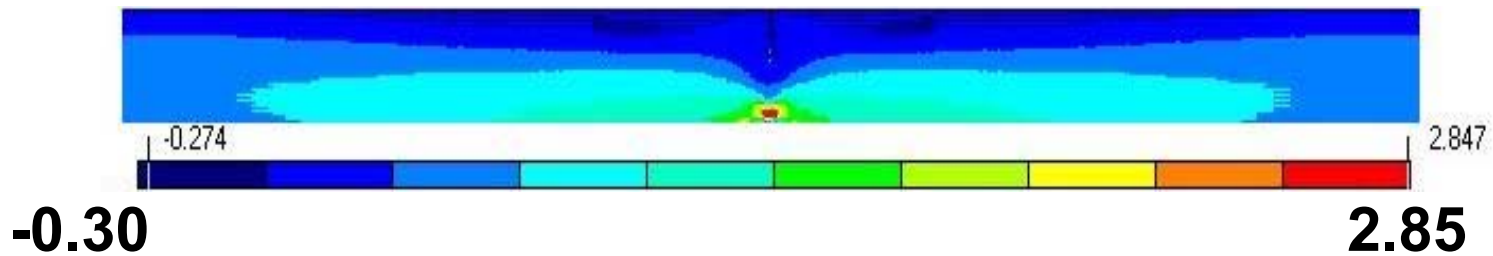
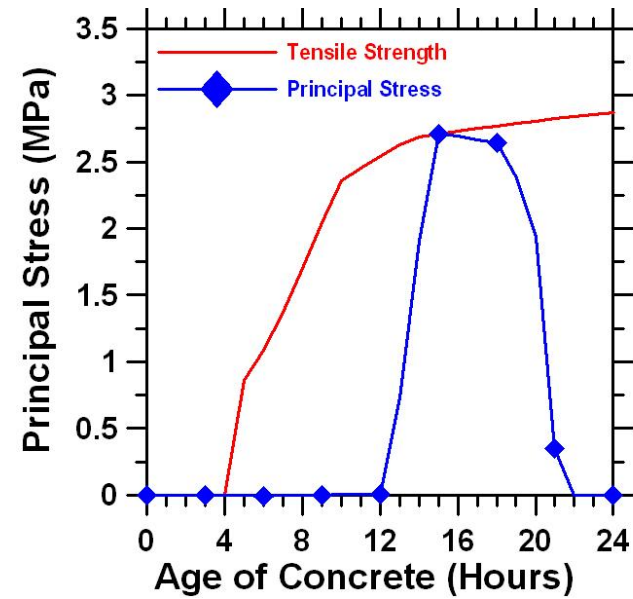
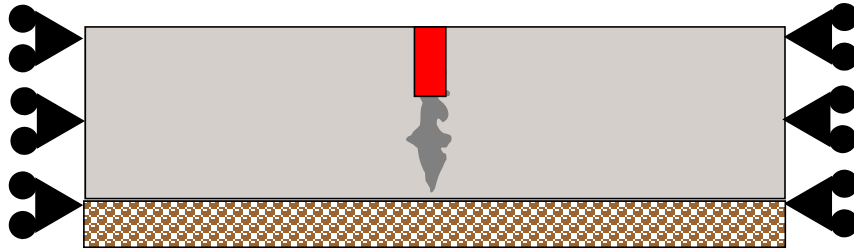




# $a_0 = D/3$ Notch Exerted at 12 Hours

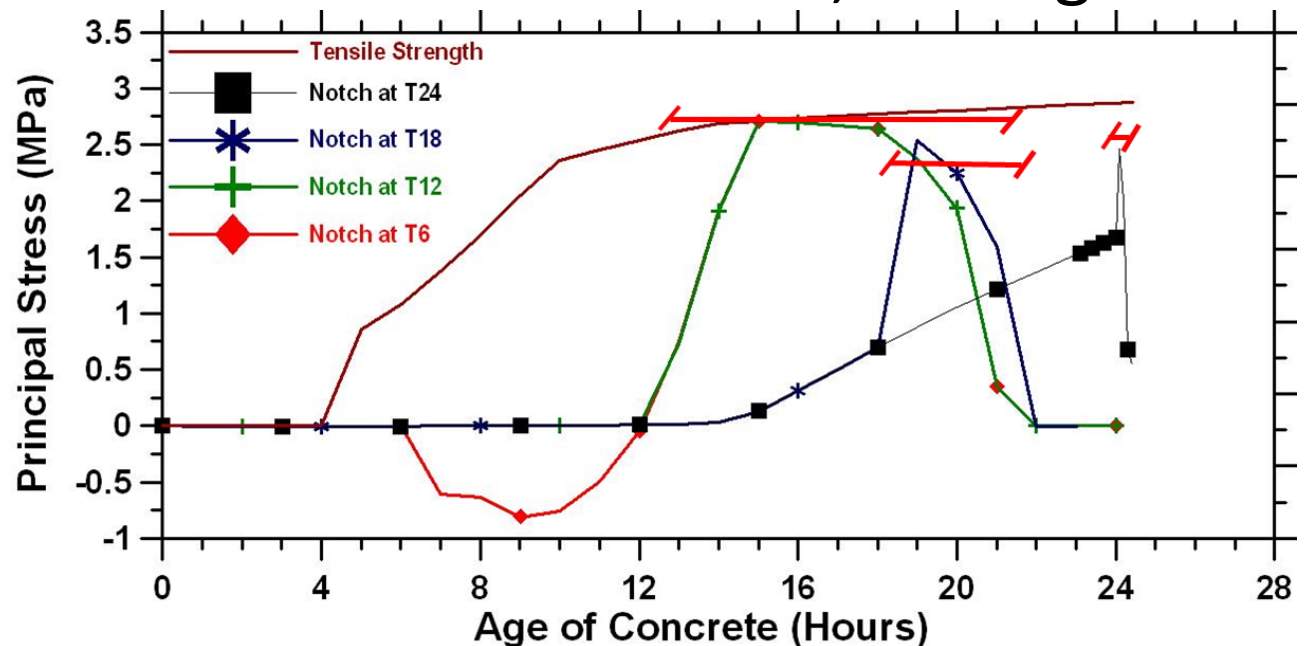
## Case II

Step 4, 19-24 hours



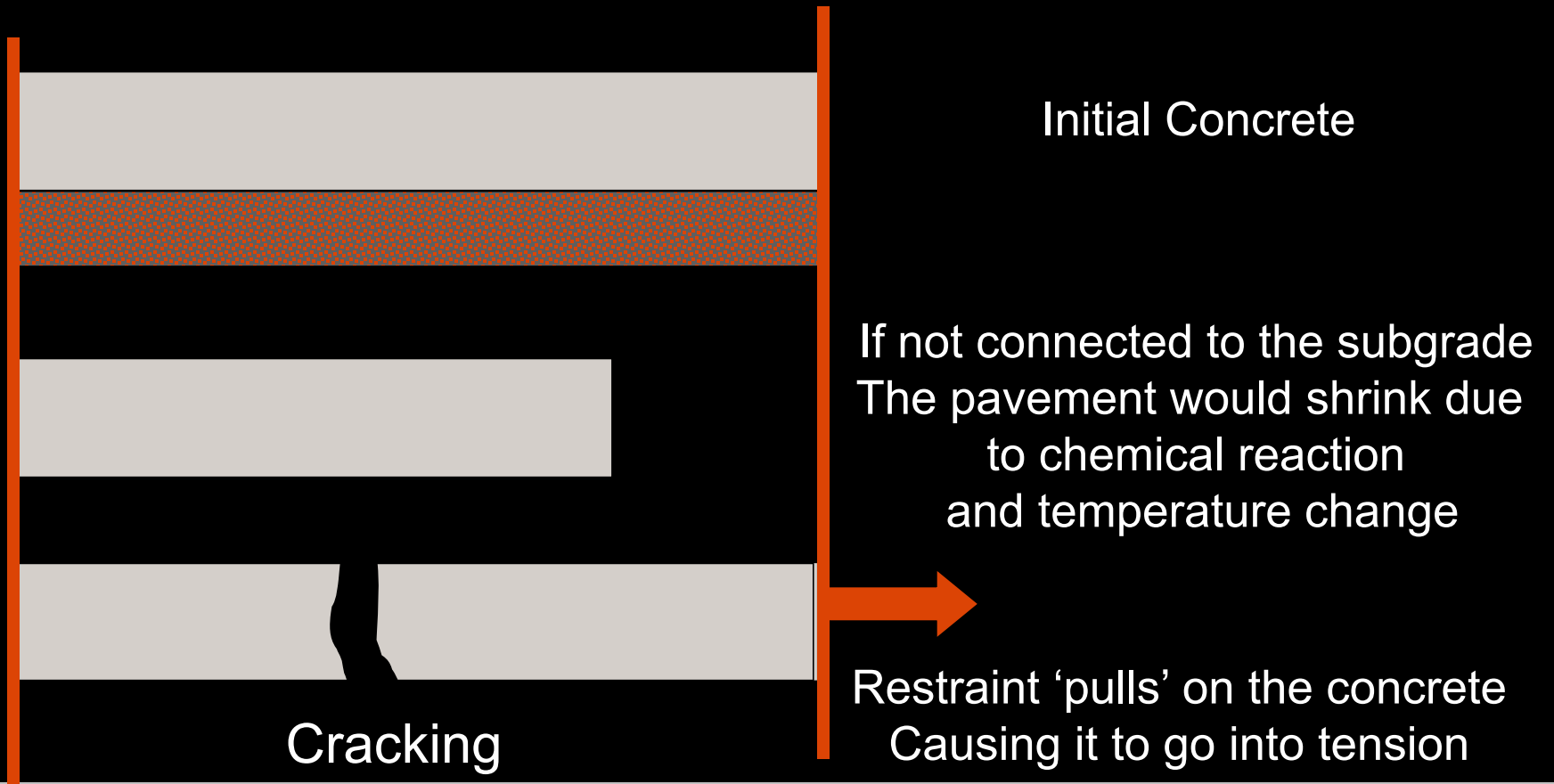
# Summary of Different Saw-cutting Time

- As shown in the graph, the later the notch is introduced, the more brittle the concrete, the higher internal stresses, the higher the potential for random cracking



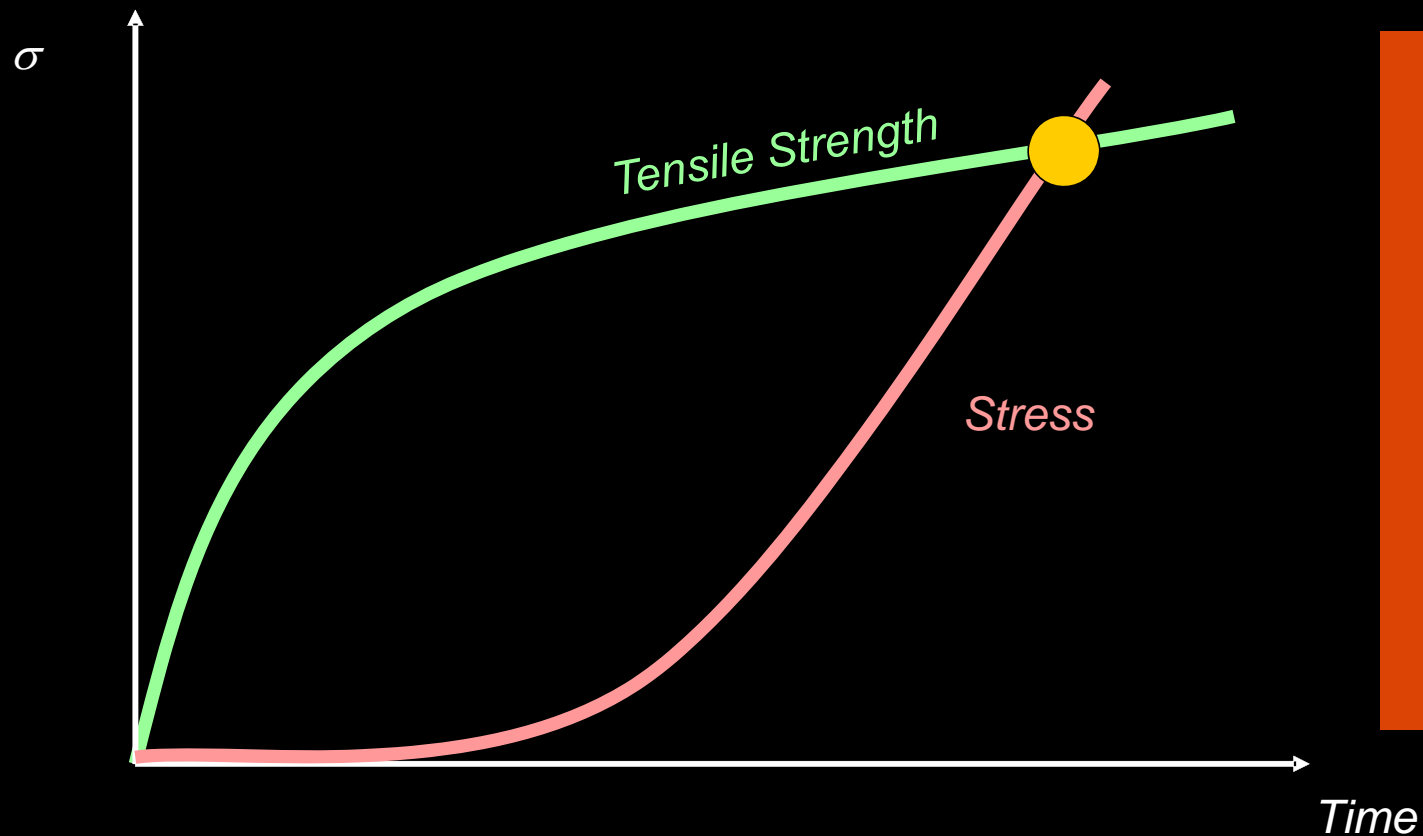


# Restrained Slab at Early Ages





# Comparing Stress and Strength

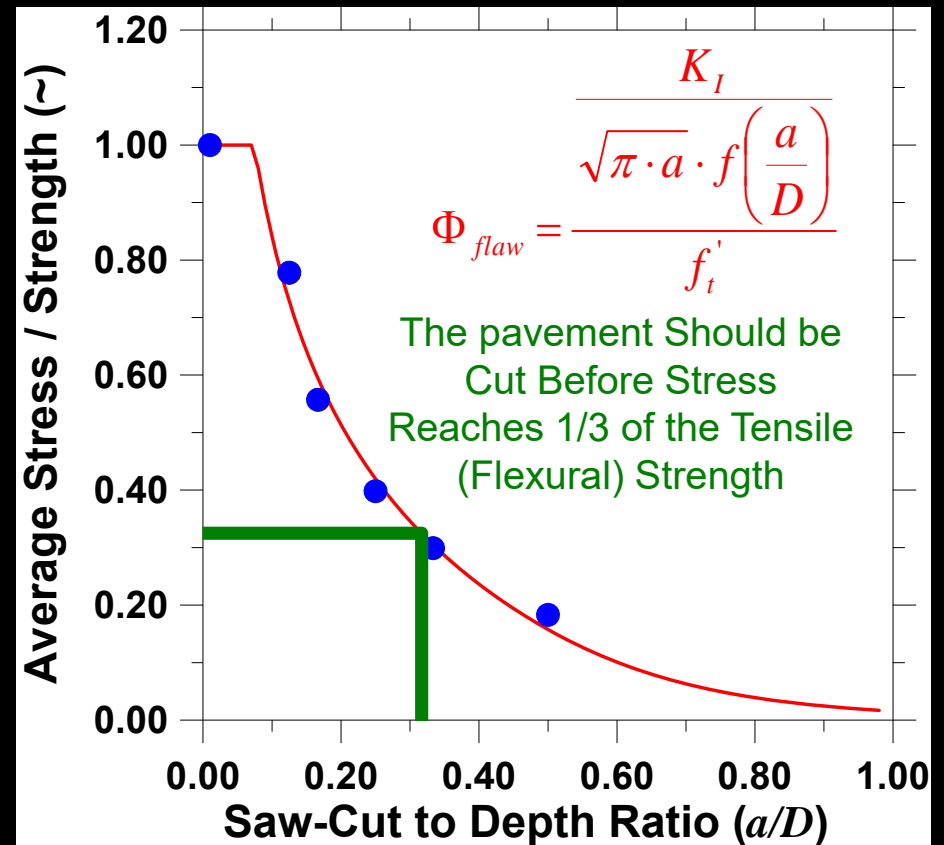


**Valid for an  
Unnotched  
Specimen Only  
A Strength  
Reduction  
Factor is  
Needed for Cut  
Slabs**



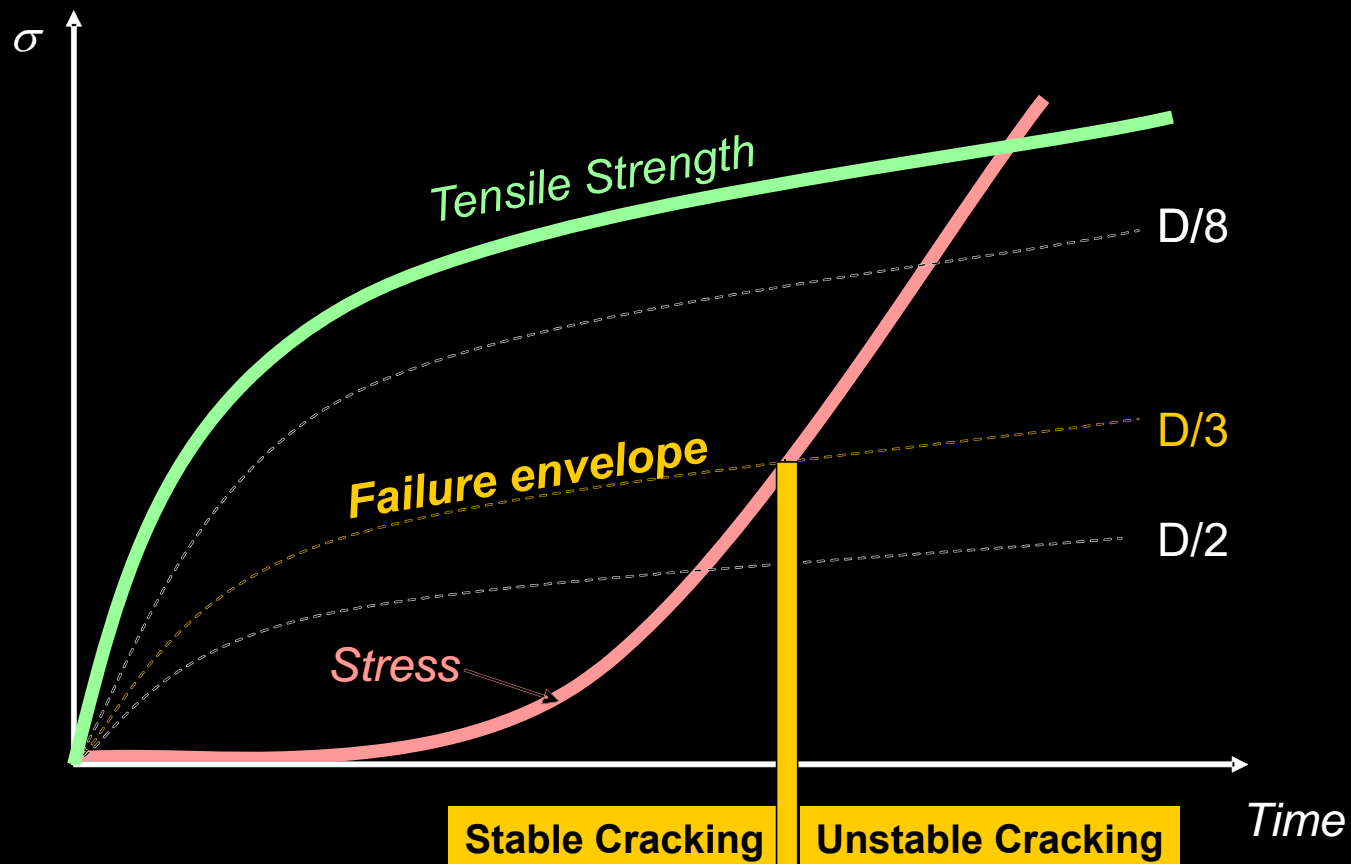
# Saw-Cut Depth and A Strength Reduction Factor

- Average stress/strength ratio for different saw-cut depths
- It can be used effectively to select appropriate depth of saw-cut





# Comparing Stress and Strength When a Cut Exists

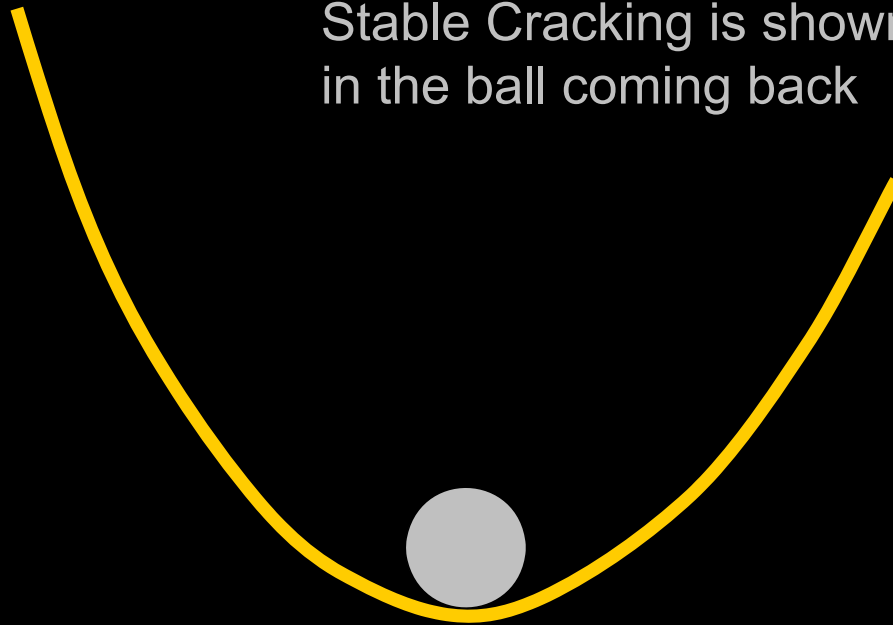




# Stable vs. Unstable Cracking

Sawcutting Changes the 'Energy in a Pavement'  
It is like moving the ball in this dish

Stable Cracking is shown where movement results  
in the ball coming back

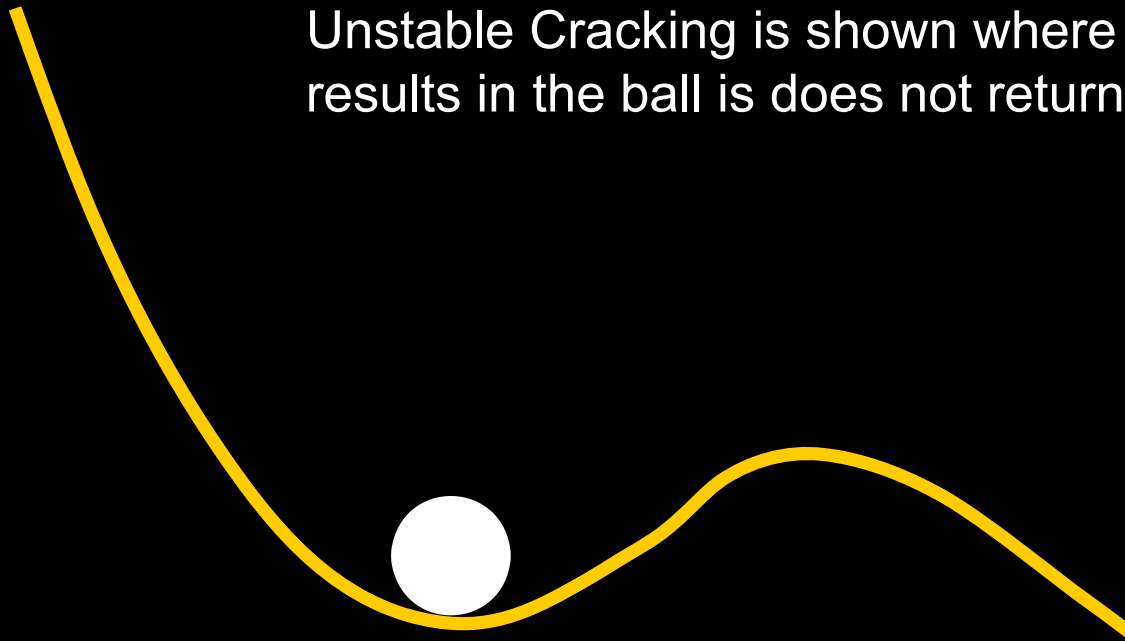




# Stable vs. Unstable Cracking

Sawcutting Changes the 'Energy in a Pavement'  
It is like moving the ball in this dish

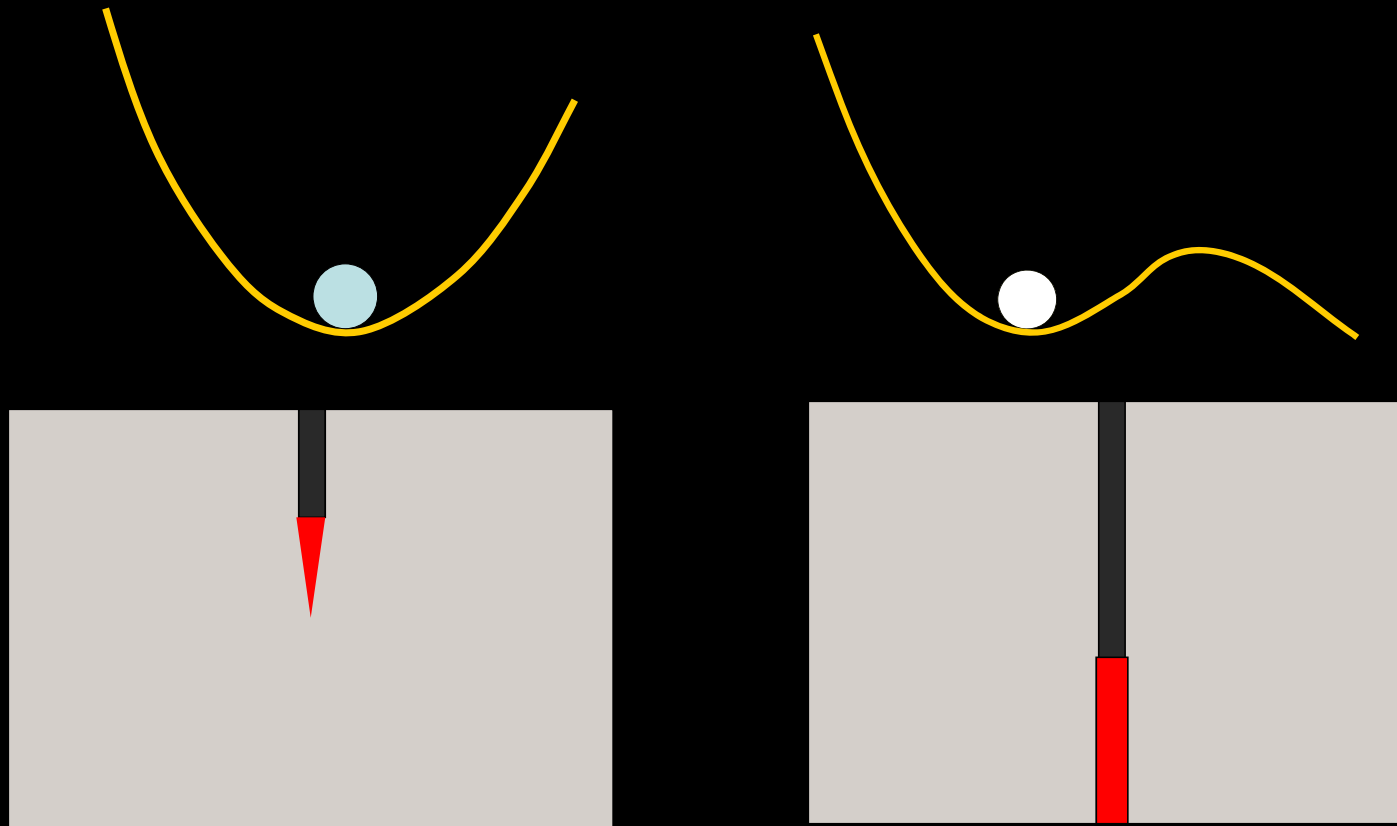
Unstable Cracking is shown where movement results in the ball is does not return to a stable spot





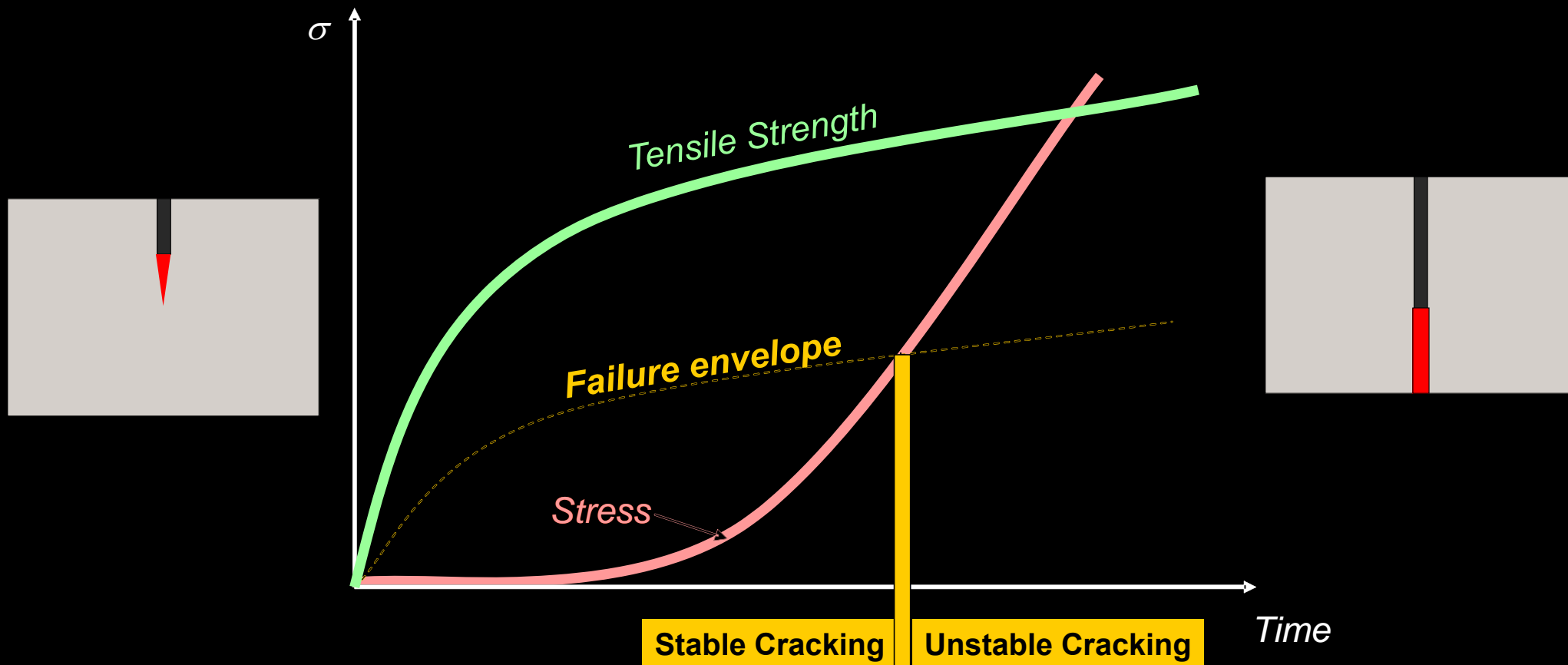


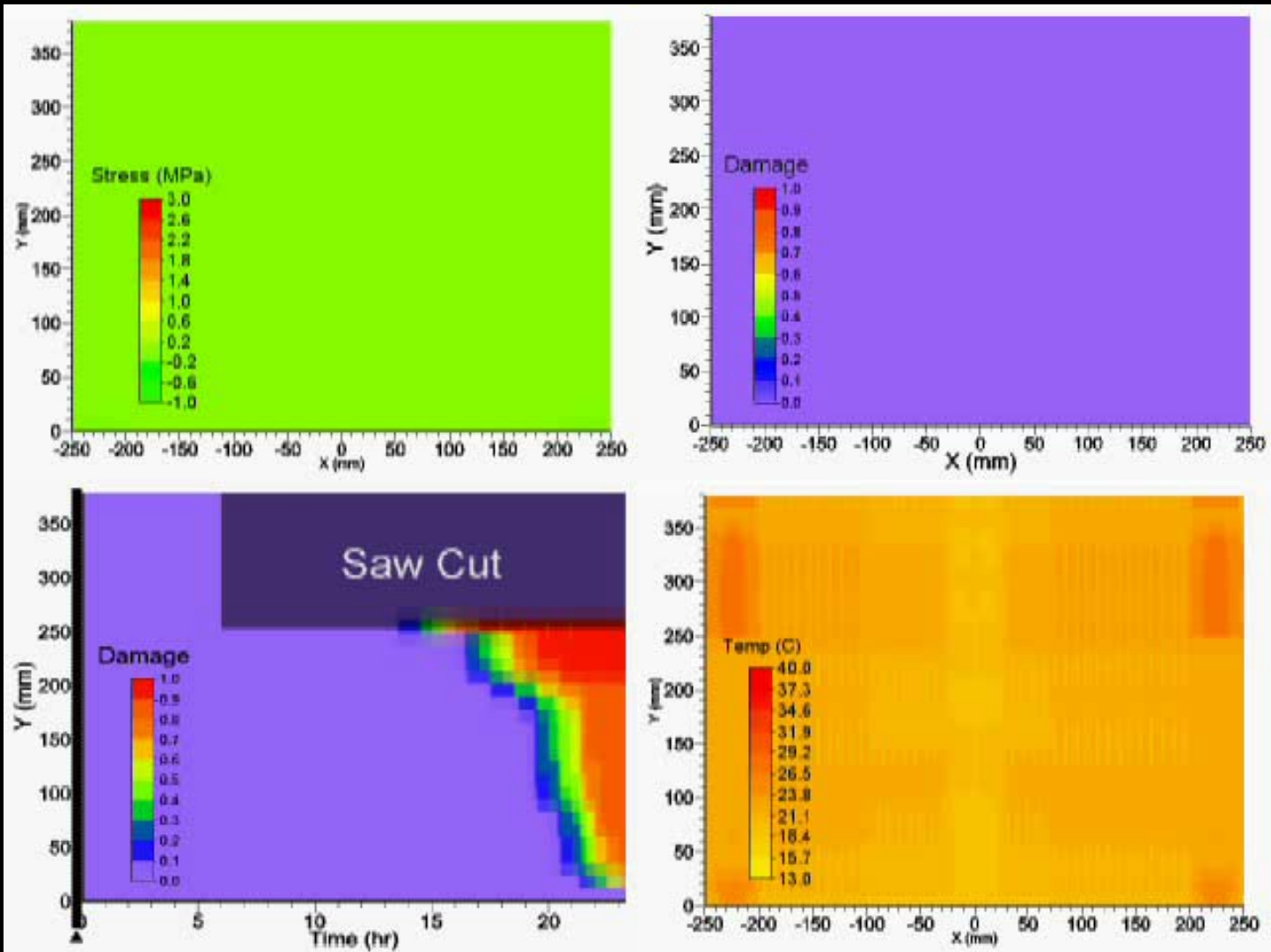
# Stable vs. Unstable Cracking





# Comparing Stress and Strength When a Cut Exists





# Conclusions



- Used a computer to simulate early age concrete
- Examined the influence of the environment and construction operations
- Case I – No Saw-Cutting
- Case II – Saw-Cutting
- Cutting at Later Ages is Less Stable
- Developed A Strength Reduction Factor
- If Late in Cutting, Cut Shallow then Make Larger