



Fall 2017 — Making Connections

Seismic Design of Shape Memory Alloy Reinforced Concrete Bridge Pier

Dr. AHM Muntasir Billah, P.Eng.

Bridge Engineer, Parsons

Dr. M. Shahria Alam, P.Eng.

The University of British Columbia



Outline

- Current seismic design philosophy
- Performance based seismic design (PBSD)
- PBSD for new materials
- PBSD Example on SMA-RC Pier
- Conclusion

Current Seismic Design Philosophy

Collapse Prevention



“Failure”

Current Seismic Design Philosophy



“Failure”

Current Seismic Design Philosophy



“Success -- ?”

Current Seismic Design Philosophy

- ❑ May result in bridge closures
 - Excessive column damage
 - Excessive lateral deflection
 - Limited access; may or may not allow even emergency response vehicles
- ❑ Extensive Repairs
 - Patching of spalled concrete
 - Shoring of spans
 - Replacement
 - Disrupts traffic
 - Major economic loss

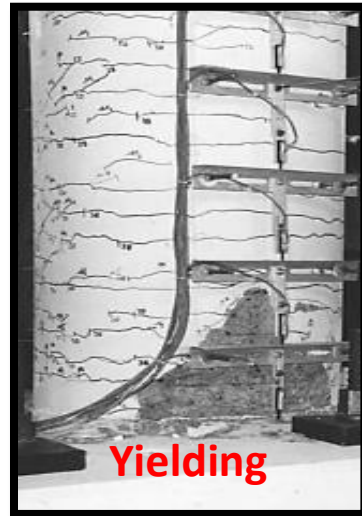
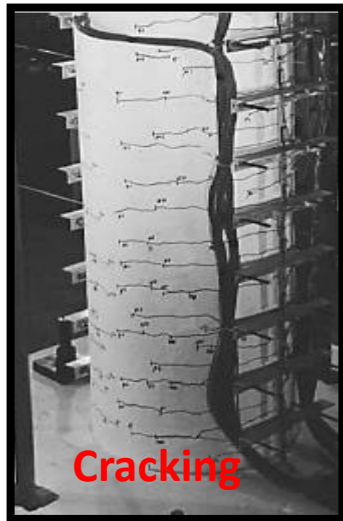


Improved Seismic Design

- Minimize residual drift
- Minimize repair need
- Keep bridges operational
- Reduce damage to plastic hinges
- Keep an energy dissipating system

Performance Based Design.....

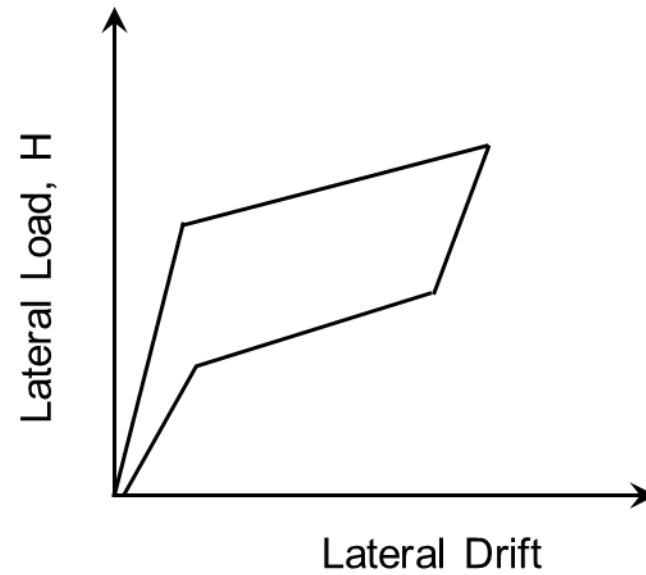
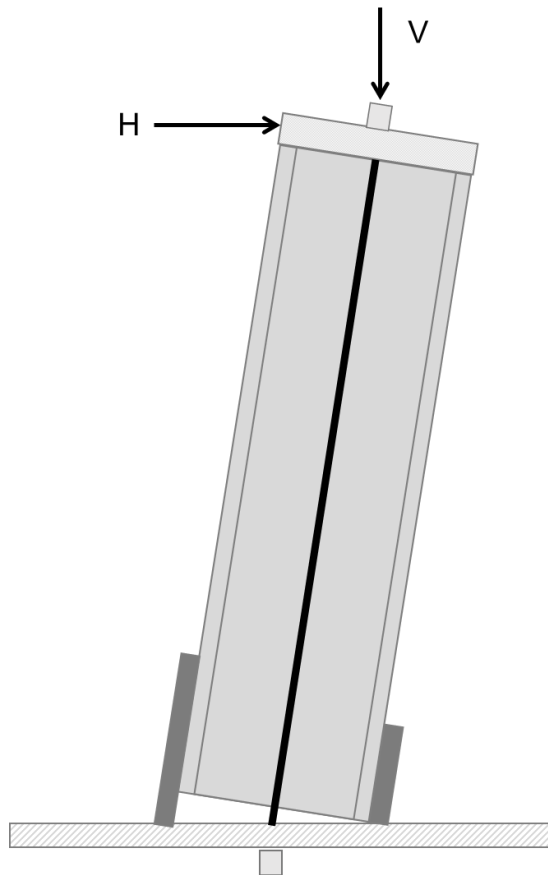
Performance Based Seismic Design



Hose et al. 2000

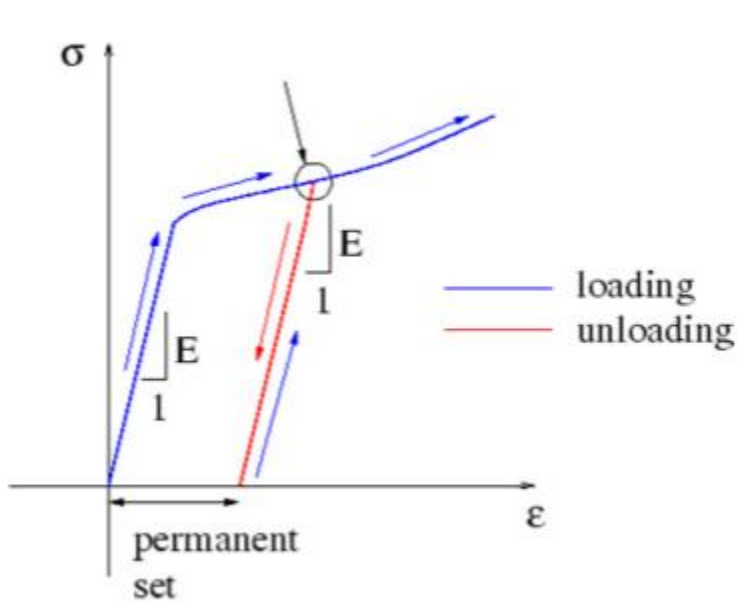
**Is it enough to protect our investments?
If not, what can we do?**

Rocking bridge pier

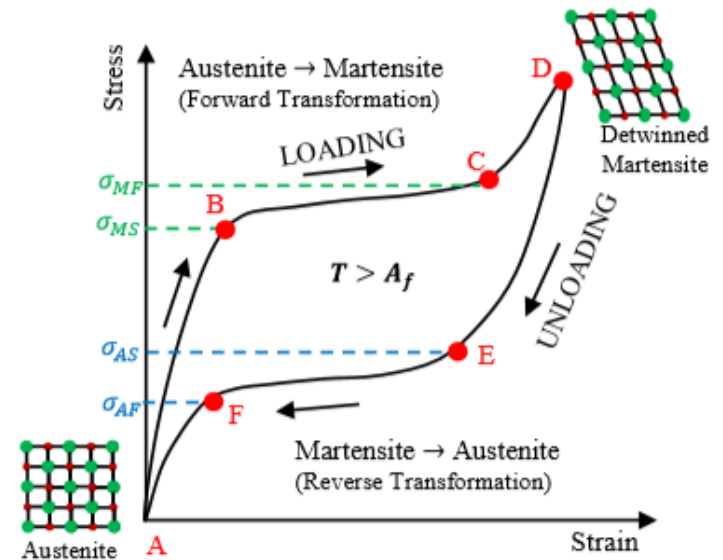


Innovative Materials

Superelastic Shape Memory Alloy (SMA)



Steel

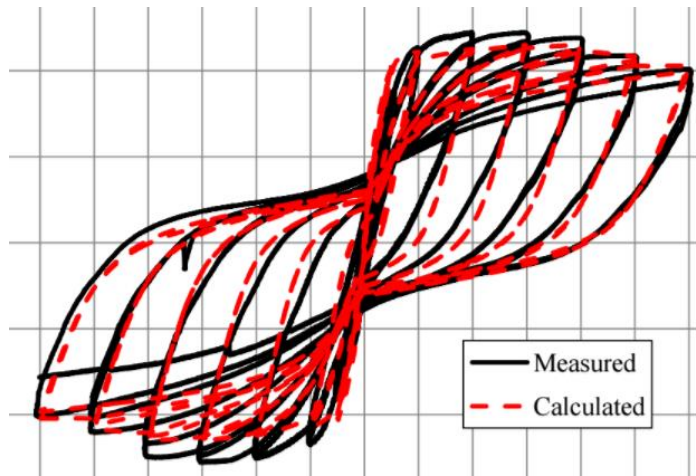


SMA

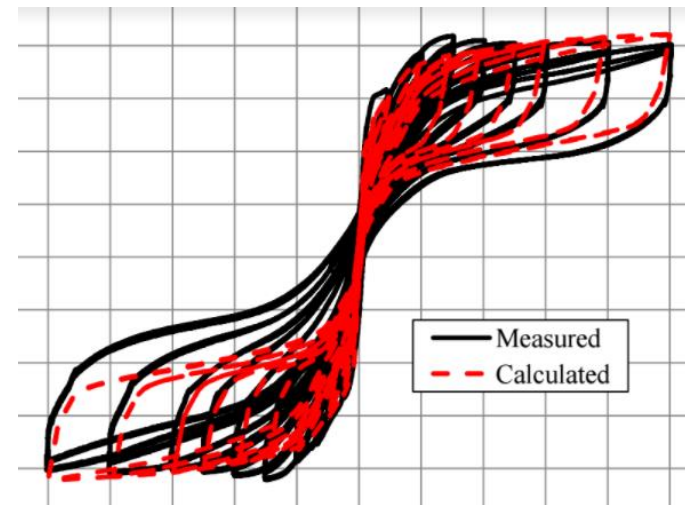
Innovative Materials

Reinforced Concrete Columns

➤ Reduced residual deformation

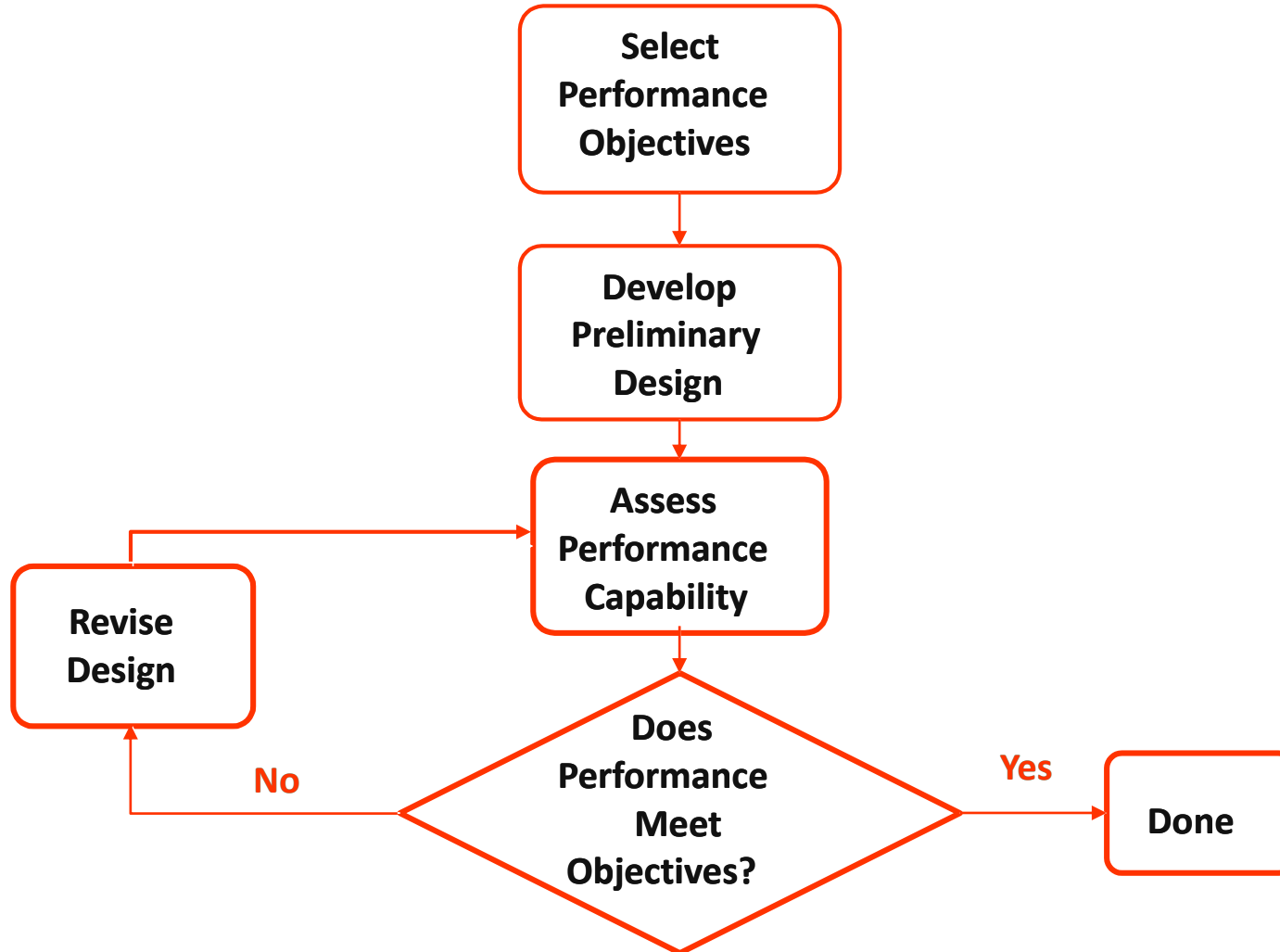


Steel RC Column

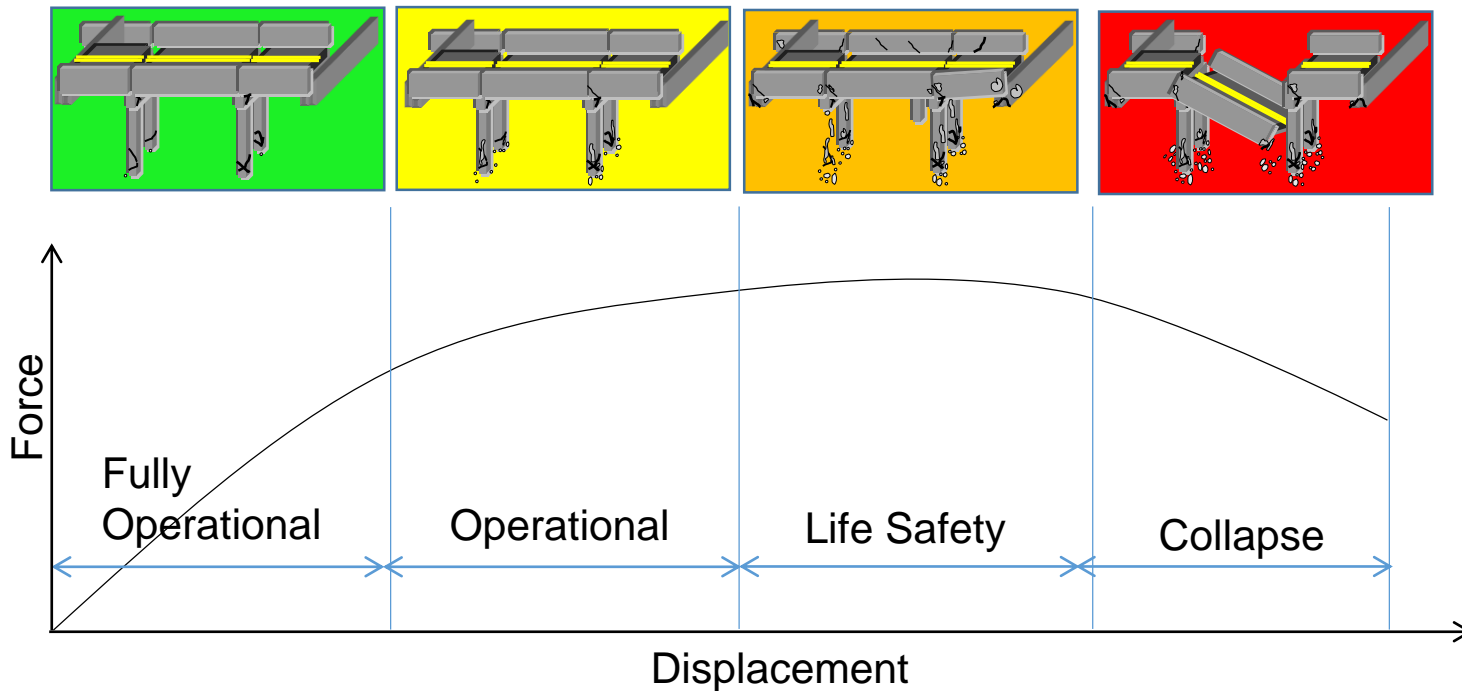


SMA RC Column

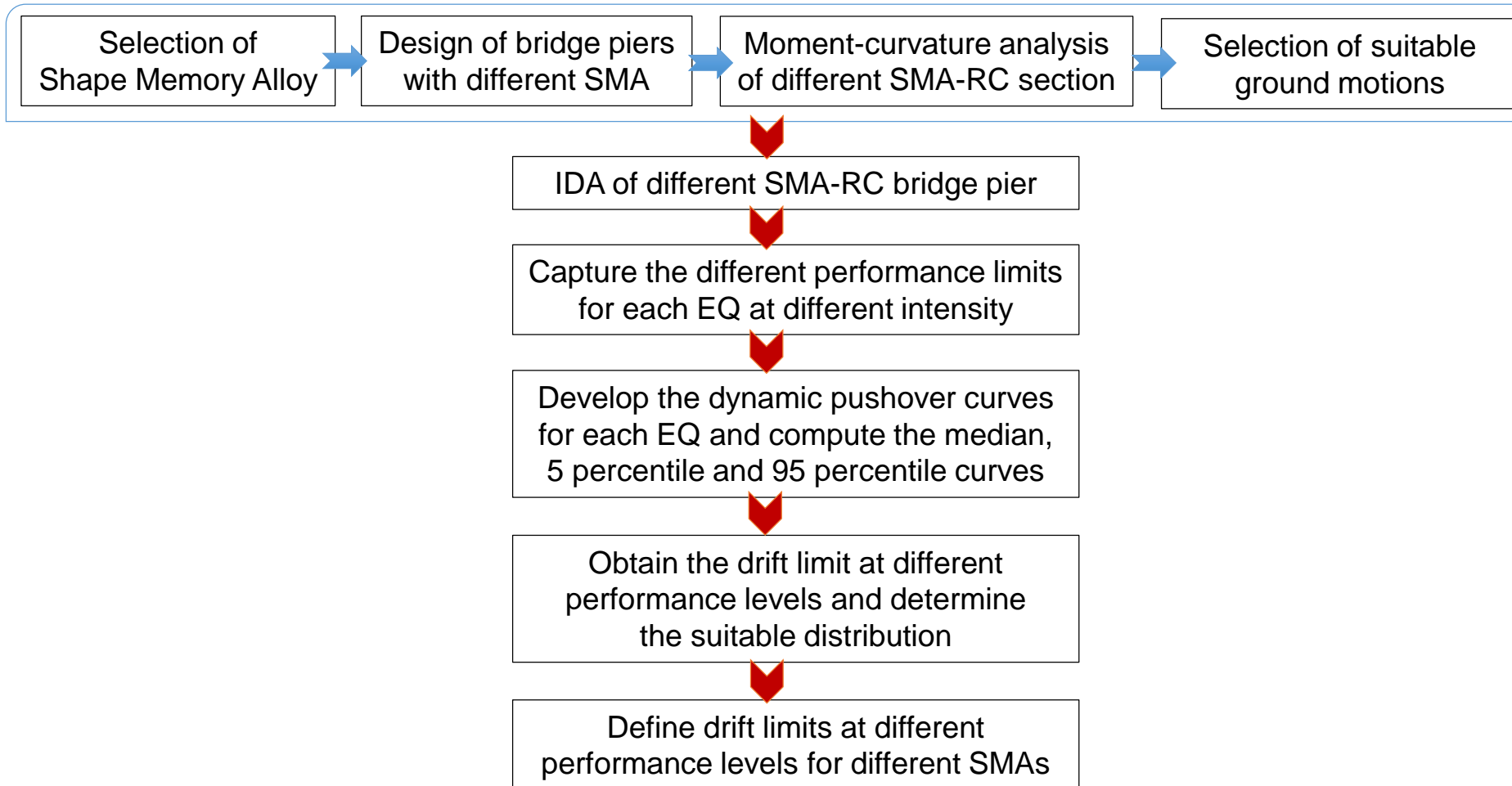
Performance Based Design of SMA-RC Pier



Performance-based Damage States



Damage State Development

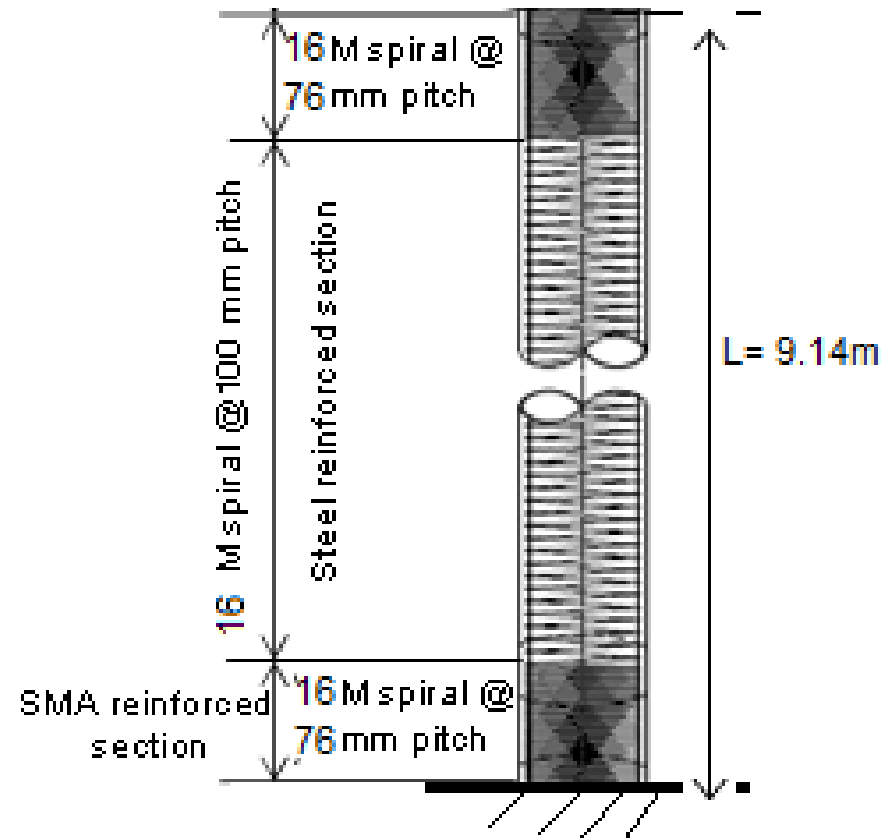
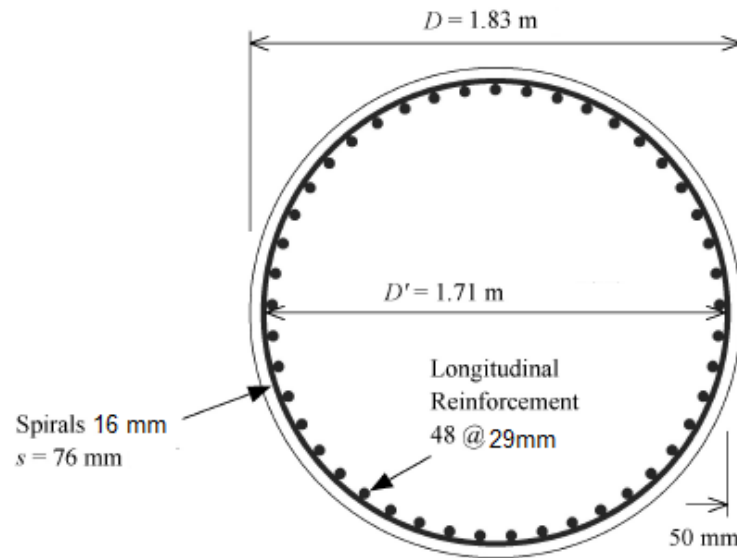


Properties of Different SMAs

	Alloy	ϵ_s (%)	E (GPa)	f_y (MPa)	f_{p1} (MPa)	f_{T1} (MPa)	f_{T2} (MPa)	Ref
SMA-1	NiTi ₄₅	6	62.5	401.0	510	370	130	Alam et al. 2008
SMA-2	NiTi ₄₅	8	68	435.0	535.0	335	170	Ghassemieh et al. 2012
SMA-3	FeNCATB	13.5	46.9	750	1200	300	200	Tanaka et al. 2010
SMA-4	CuAlMn	9	28	210.0	275.0	200	150	Shrestha et al. 2013
SMA-5	FeMnAlNi	6.13	98.4	320.00	442.5	210.8	122	Omori et al. 2011

f_y (austenite to martensite starting stress); f_{p1} (austenite to martensite finishing stress); f_{T1} (martensite to austenite starting stress); f_{T2} (martensite to austenite finishing stress) , ϵ_s (superelastic plateau strain length); and E (modulus of elasticity).

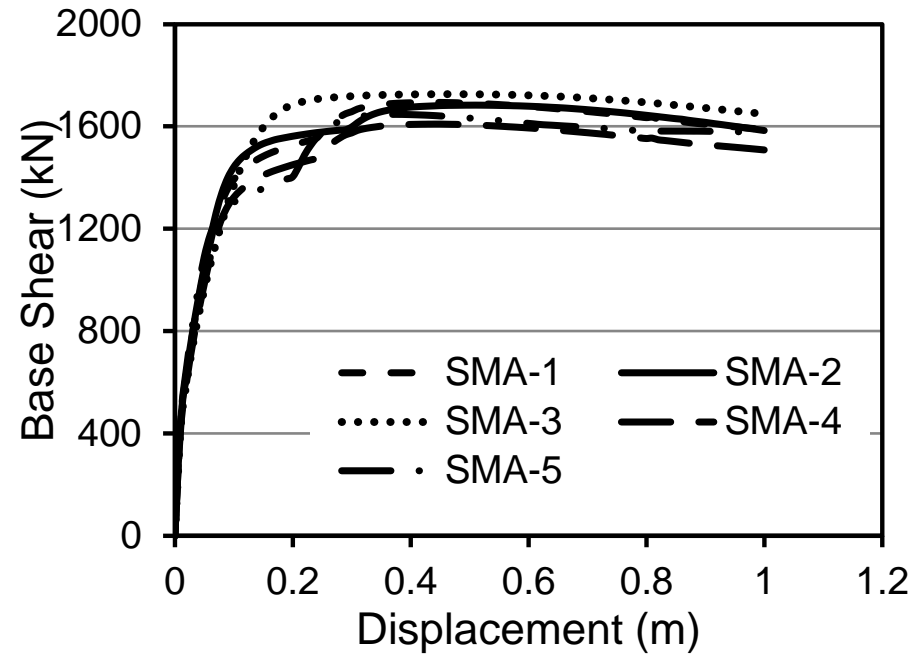
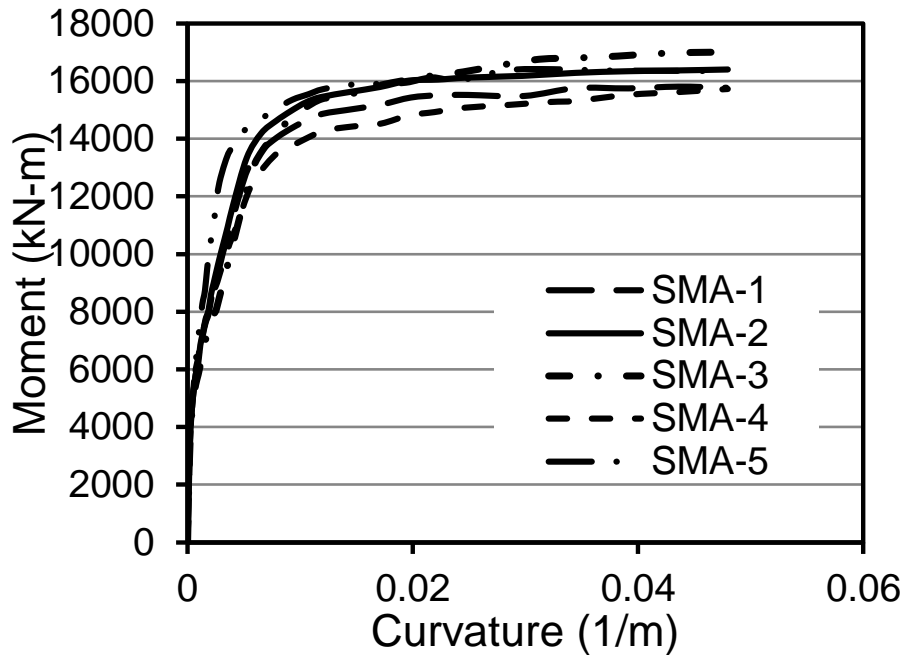
Design and Geometry of Bridge Piers



Bridge Pier Configuration

Pier	Longitudinal Rebar	ρ_l (%)	Spiral	ρ_s (%)
SMA-RC-1	48-28M	1.12	15M @76 mm	0.70
SMA-RC-2	48-28M	1.12	15M @76mm	0.70
SMA-RC-3	48-20M	1.20	15M @76 mm	0.70
SMA-RC-4	48-35M	1.75	15M @76 mm	0.70
SMA-RC-5	48-32M	1.46	15M @76mm	0.70

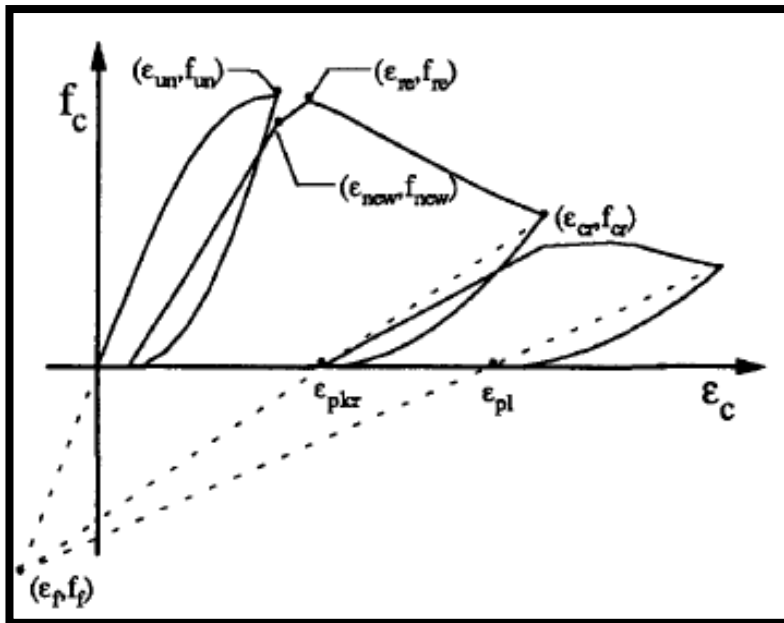
Capacity Curves



Finite Element Modeling

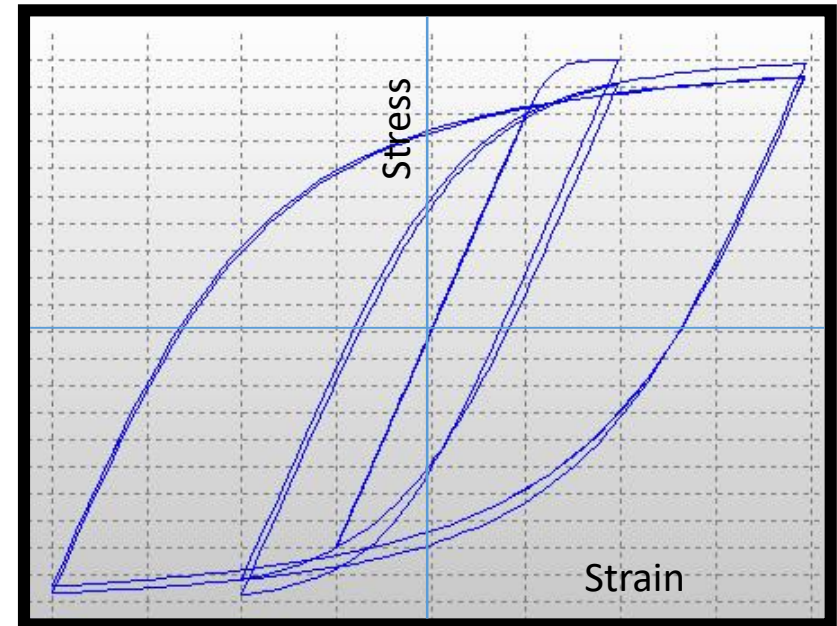
Concrete Model

Mander et al. [1988] & Martinez-Rueda and Elnashai [1997]



Steel Model

Menegotto and Pinto, 1973



Validation with Experimental Result

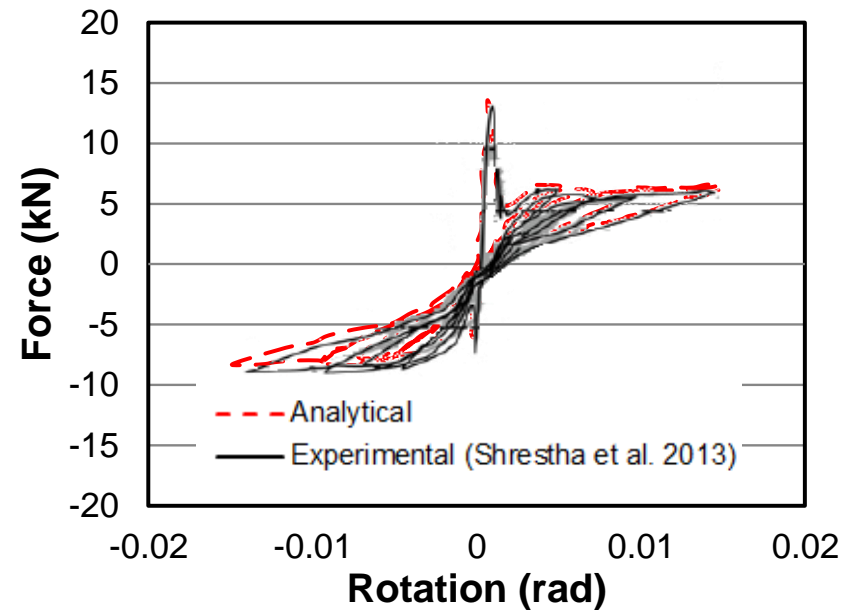
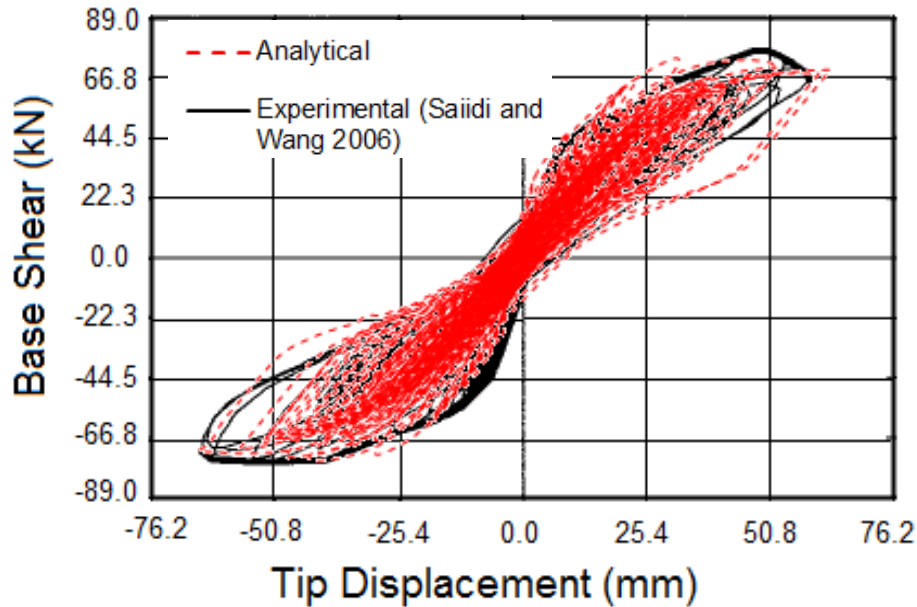
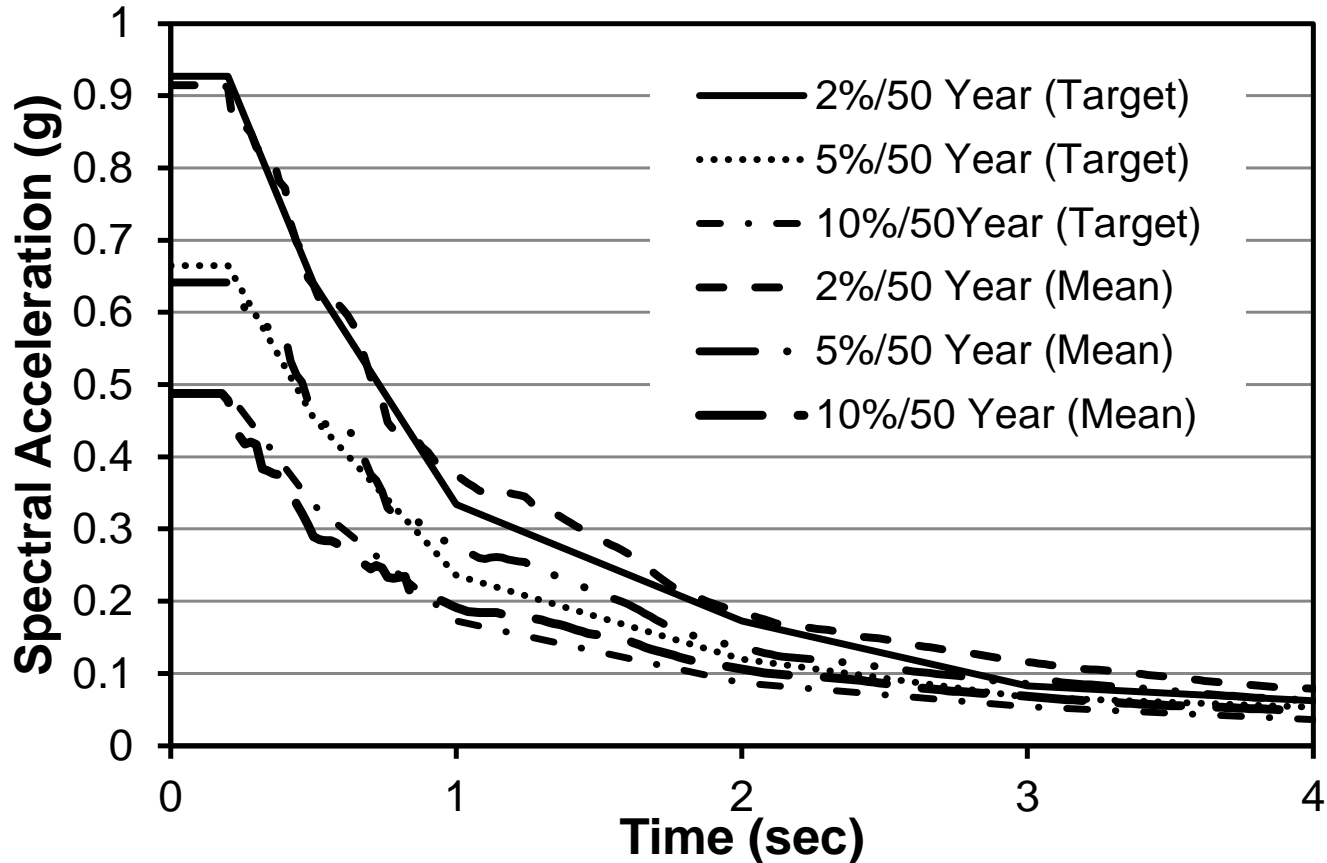


Fig. Comparison of experimental and numerical results (a) SMA-RC (SMA-1) bridge pier (Saiidi and Wang 2006). (b) SMA-RC (SMA-4) beam (Shrestha et al. 2013).

Different Hazard Levels



Proposed Damage State Framework

Damage Parameter	Damage State	Functional Level	Description
Cracking	DS-1	Immediate	Onset of hairline cracks
Yielding	DS-2	Limited	Theoretical first yield of longitudinal rebar
Spalling	DS-3	Service disruption	Onset of concrete spalling
Core Crushing	DS-4	Life safety	Crushing of core concrete

Maximum Drift Damage States

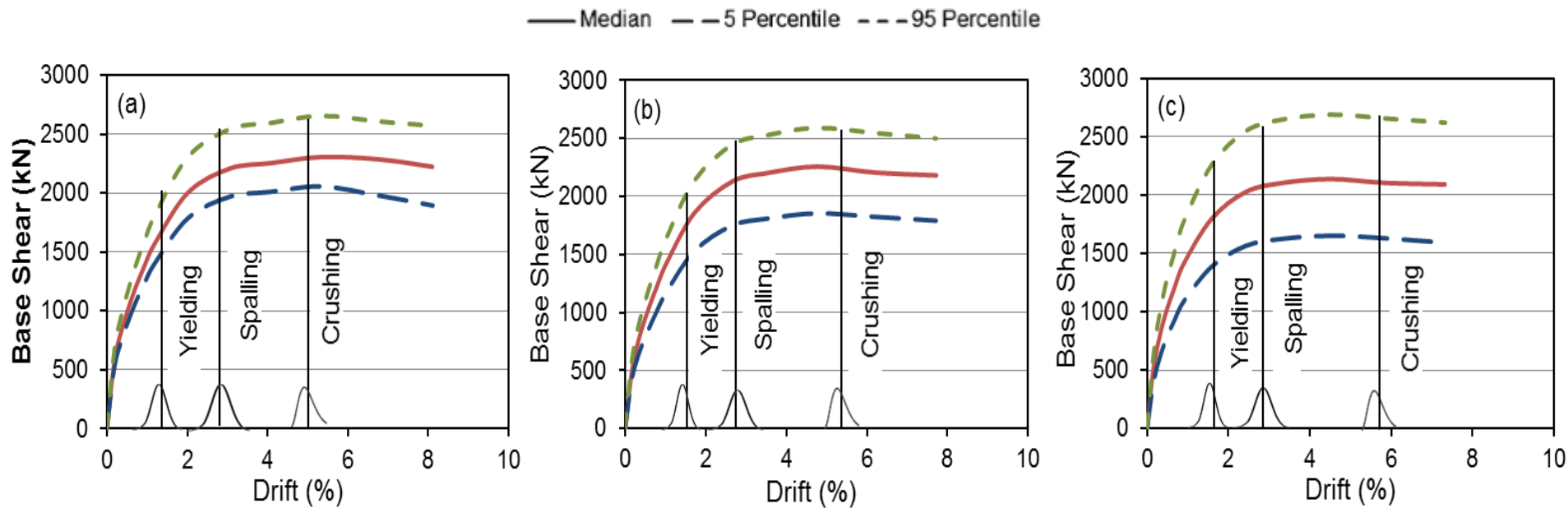


Figure . Dynamic pushover response and different damage states with distribution for SMA-RC-1 for (a) 2% in 50 years (b) 5% in 50 years and (c) 10% in 50 years probability of exceedance

Damage States of SMA-RC Bridge Pier

Damage Parameter	Damage State	SMA-1			SMA-2			SMA-3			SMA-4			SMA-5			Distribution	
		Drift (%)			Drift (%)			Drift (%)			Drift (%)			Drift (%)				
		Probability of Exceedance																
2%	5%	10%	2%	5%	10%	2%	5%	10%	2%	5%	10%	2%	5%	10%	2%	5%	10%	
50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	
Cracking	DS-1	0.28	0.28	0.28	0.30	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	Uniform
Yielding	DS-2	1.68	1.76	1.86	1.66	1.72	1.80	2.28	2.42	2.58	1.74	1.83	1.95	1.10	1.16	1.21	Lognormal	
Spalling	DS-3	2.66	2.79	2.88	2.69	2.77	2.87	1.64	1.72	1.80	2.52	2.61	2.68	1.97	2.02	2.10	Normal	
Crushing	DS-4	5.05	5.68	5.94	5.51	5.91	6.05	7.65	7.81	7.94	5.56	5.63	5.72	4.73	4.79	4.84	Gamma	



Maximum Drift Damage States

Damage Parameter	Damage State	Functional Level	Maximum Drift (%)		
			Probability of Exceedance		
			10% in 50	5% in 50	2 % in 50
Cracking	DS-1	Fully Operational	0.28	0.28	0.28
Yielding	DS-2	Operational	1.86	1.76	1.68
Spalling	DS-3	Life safety	2.88	2.79	2.66
Crushing	DS-4	Collapse Prevention	5.94	5.68	5.05

Residual Drift Damage States

Damage State	Functional Level	Description
Slight (DS=1)	Fully Operational	No structural realignment is necessary
Moderate (DS=2)	Operational	Minor structural repairing is necessary
Extensive (DS=3)	Life safety	Major structural realignment is required
Collapse (DS=4)	Collapse	Structure in danger of collapse from earthquake aftershocks

Residual Drift Damage States

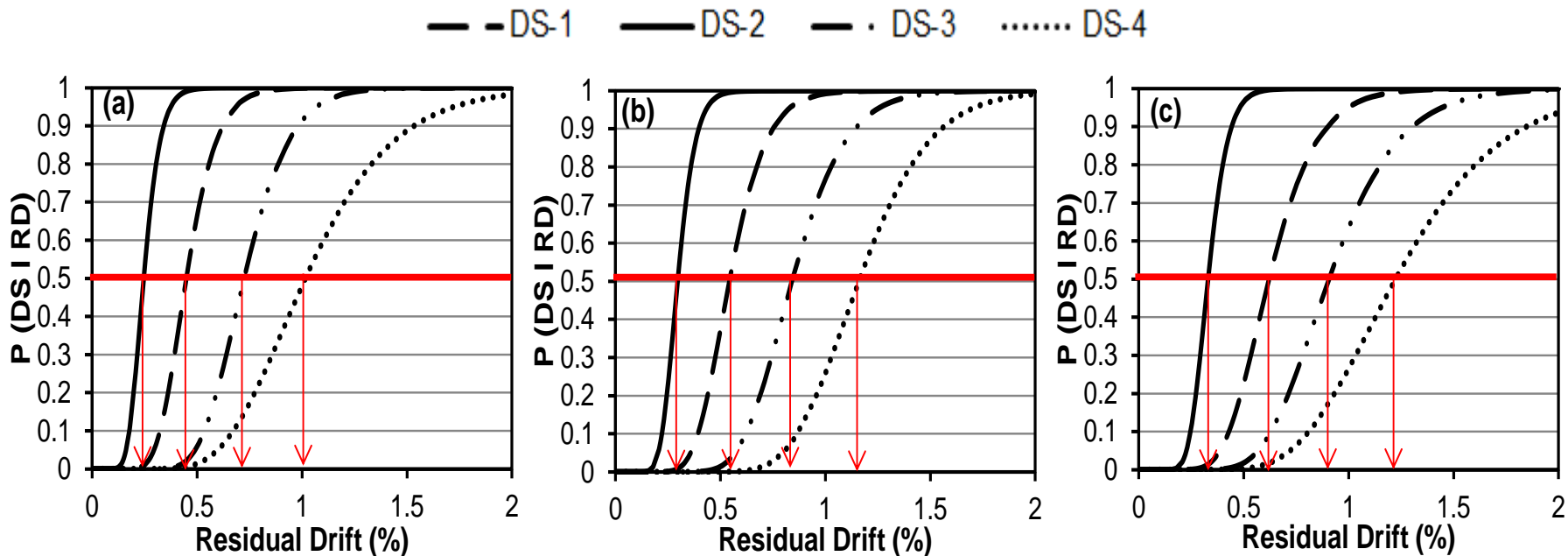


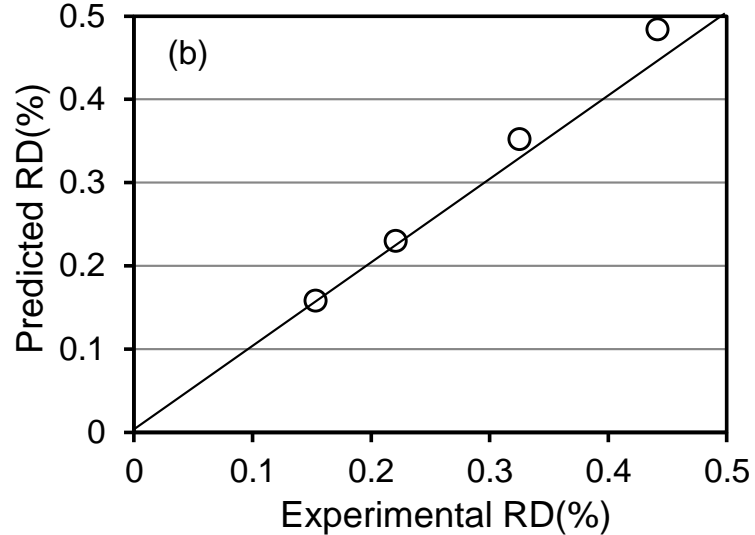
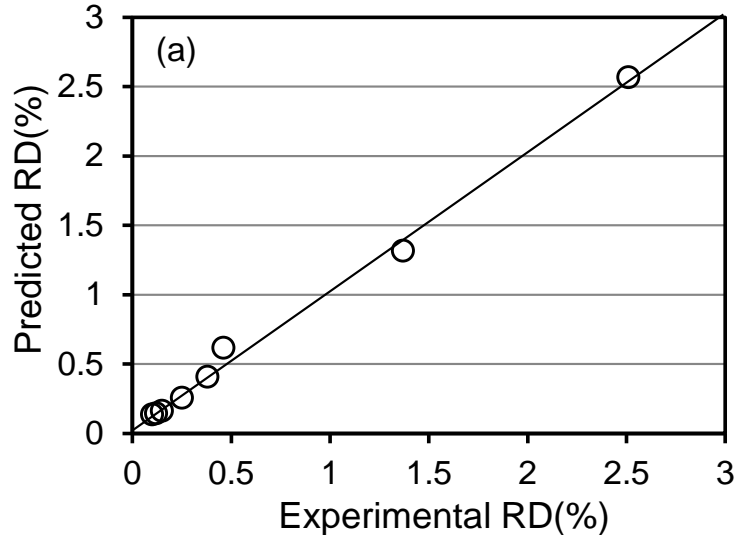
Figure. Fragility curves in terms of residual drift at (a) 10% in 50 years (b) 5% in 50 years and (c) 2% in 50 years probability of exceedance

Residual Drift Damage States

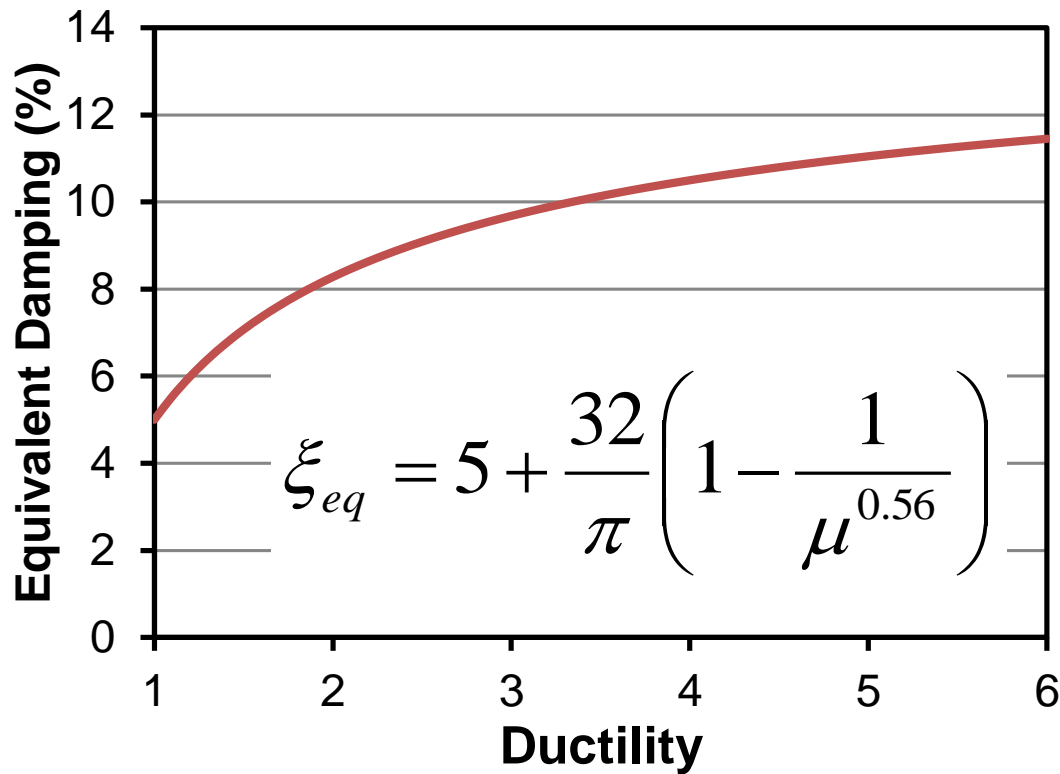
Damage State	Functional Level	Description	Residual Drift, R_{Δ} (%)		
			Probability of Exceedance		
			10% in 50	5% in 50	2 % in 50
Slight (DS=1)	Fully Operational	No structural realignment is necessary	0.24	0.28	0.33
Moderate (DS=2)	Operational	Minor structural repairing is necessary	0.48	0.55	0.62
Extensive (DS=3)	Life safety	Major structural realignment is required	0.73	0.82	0.87
Collapse (DS=4)	Collapse	Structure in danger of collapse from earthquake aftershocks	1.04	1.16	1.22

Prediction of Residual Drift

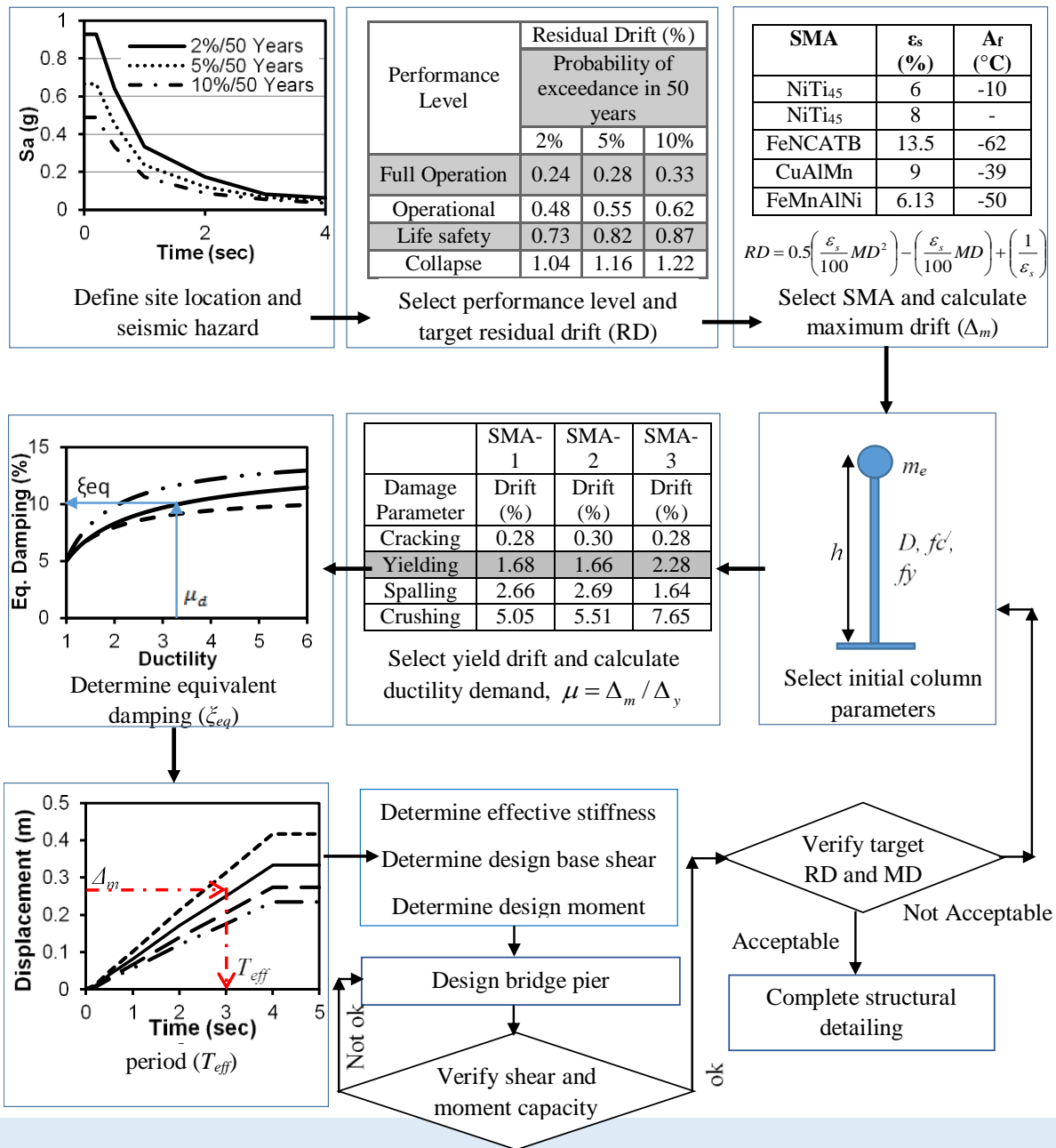
$$RD = 0.5 \left(\frac{\varepsilon_s}{100} MD^2 \right) - \left(\frac{\varepsilon_s}{100} MD \right) + \left(\frac{1}{\varepsilon_s} \right)$$



μ - ξ Relationship of SMA-RC Pier



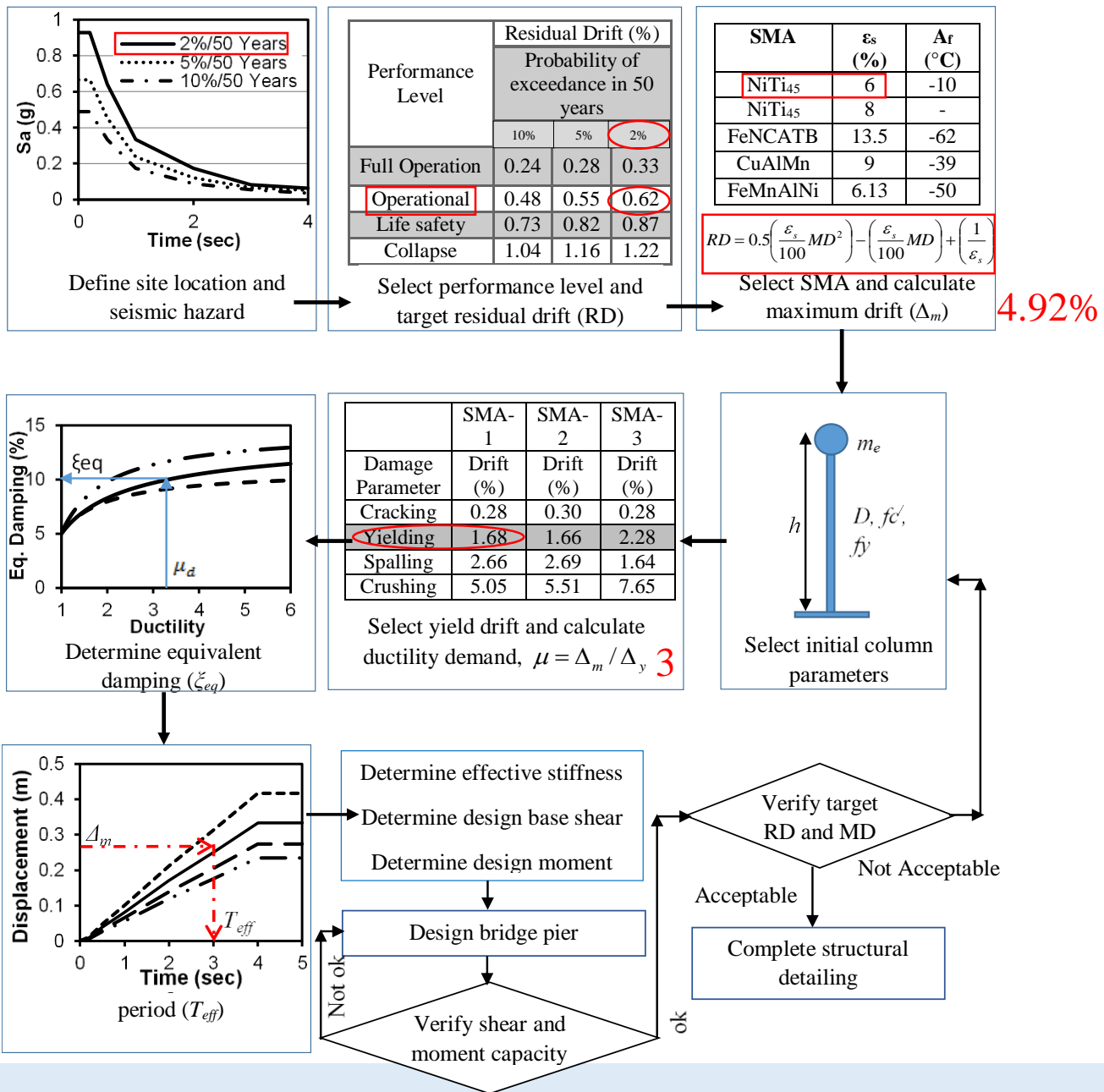
PBSD of SMA-RC Pier





Design of SMA-RC Pier

- Location: Vancouver (Soil Class-C)
- Life Line Bridge
- EQ Return Period: 2475 Yr
- Functional Level: Operational
- Damage Level: Moderate
- Target RD = 0.6%



Design of SMA-RC Pier

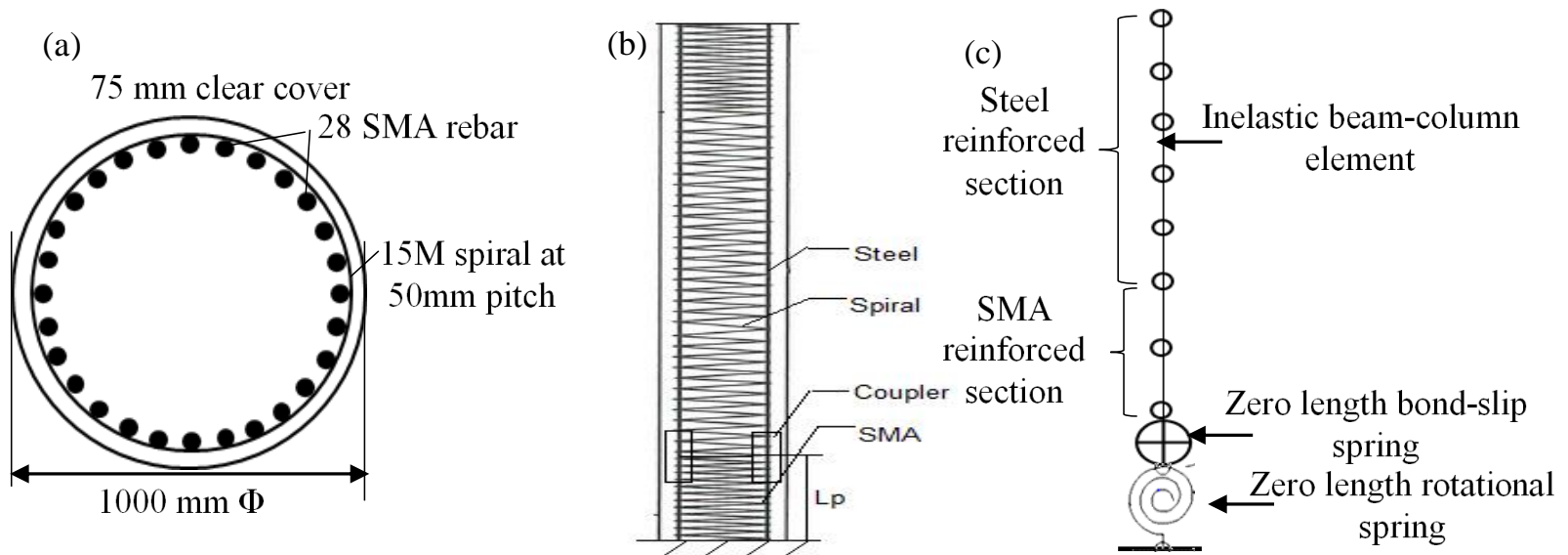
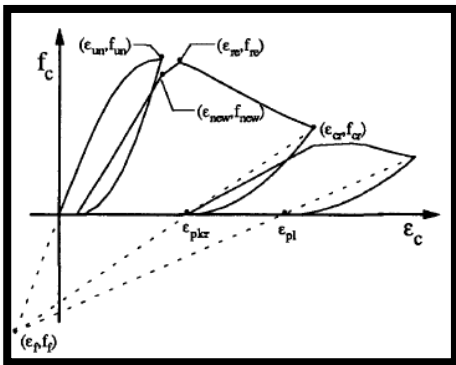


Figure. (a) Cross section, (b) elevation and (c) finite element model of SMA-RC bridge pier

Finite Element Modeling

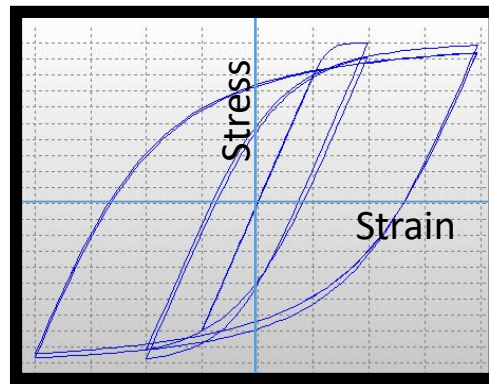
Concrete Model

Mander et al. [1988] &
Martinez-Rueda and
Elnashai [1997]



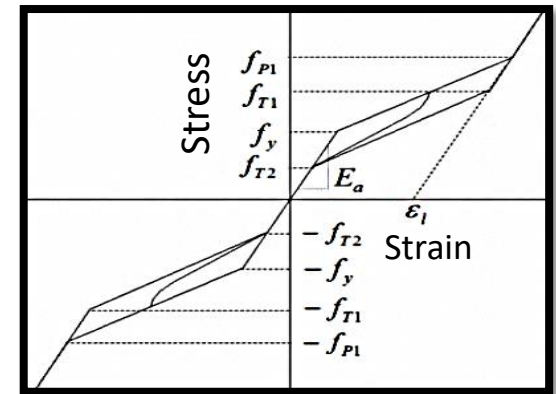
Steel Model

Menegotto and Pinto, 1973



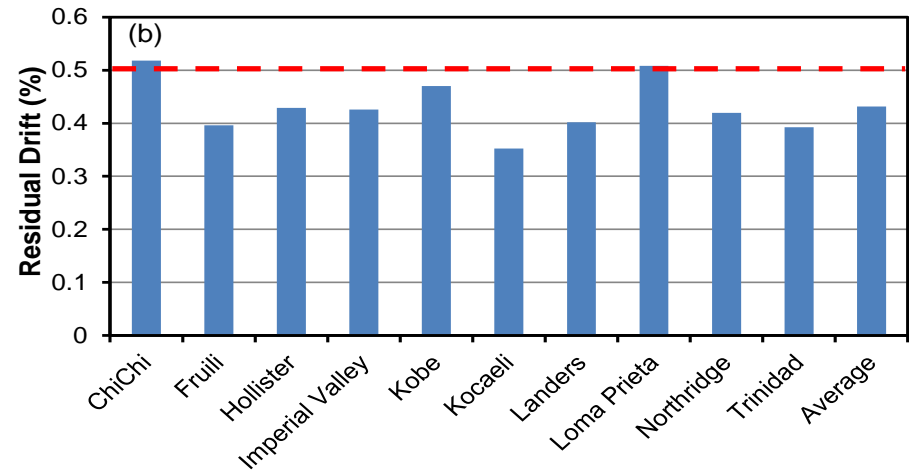
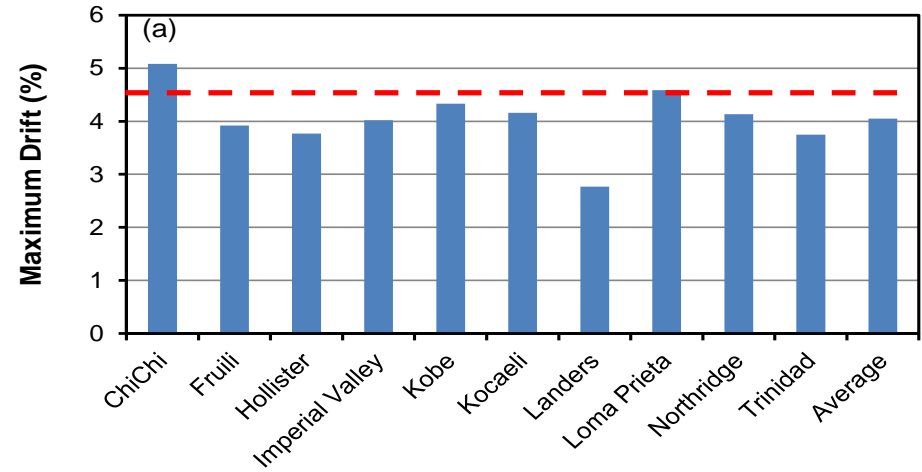
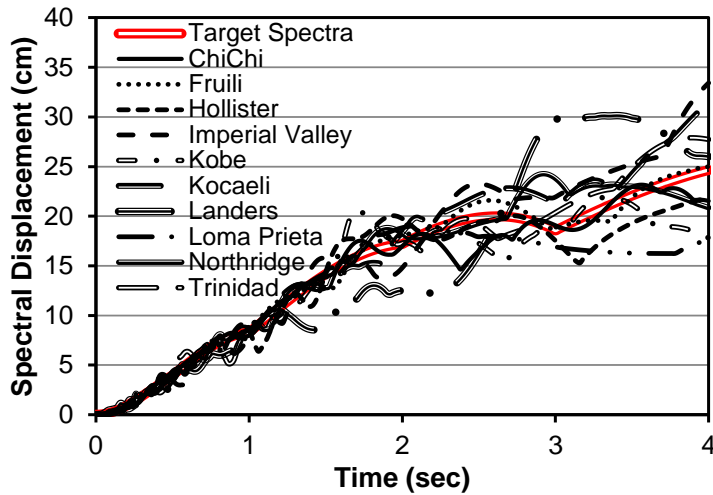
SMA Model

Auricchio and Sacco [1997]



SeismoStruct

Performance Evaluation



Conclusions

- A new residual drift-based design method
- A comprehensive approach for PBSD of SMA-RC bridge piers
- Meets performance expectations
- Lower residual drift
- Less maintenance cost

Acknowledgement

Natural Sciences and Engineering Research Council of
Canada (NSERC)

- Discovery Grant
- Industrial Postgraduate Studies

Bourcet Engineering, Vernon, BC

University of British Columbia (UBC)

- University Graduate Fellowship (UGF)



a place of mind
THE UNIVERSITY OF BRITISH COLUMBIA





Fall 2017 — Making Connections

Thanks for your attention



Questions/Comments

muntasir.billah@parsons.com

shahria.alam@ubc.ca



Source: http://www.wsdot.wa.gov/publications/fulltext/Bridge/Shape_Memory.pdf